

**TRANSISTOR AUDIO AND RADIO CIRCUITS**

**Mollard**

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# **TRANSISTOR AUDIO AND RADIO CIRCUITS**

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## FOREWORD

'Transistor Audio and Radio Circuits' is intended as a manual of established and practical circuits for use by receiver and equipment manufacturers, radio and audio service engineers, university and college students, and do-it-yourself home constructors and hi-fi enthusiasts. A wide range of circuits is presented, extending from portable radio receivers to f.m. tuners and audio amplifiers capable of the highest standards of reception and reproduction.

The circuits presented can often be used in a variety of combinations to give a wide range of equipment. For example, various pairings are possible of the h.f. and a.f. stages designed for radiograms and portable radios. And again, in the hi-fi realm, either of the f.m. tuners can be used with either of the audio amplifiers and each resulting line-up can be used with or without a stereo reception facility, and can be combined with disc and tape input sources.

Details of the practical circuits are complete, but because of the wide range of possible combinations of circuits, no attempt has been made to present precise layout and constructional information. Some general guidance is given for hi-fi amplifiers, and a chapter is devoted to some simple test equipment and its use in effectively commissioning and maintaining audio circuits. But because of the need for rather complex equipment for aligning r.f. and i.f. circuits, similar information has not been given for such stages: it is envisaged that it will be those who have access to specialised knowledge and equipment—amateur enthusiasts, beginners under expert tutelage, or professionals—who attempt to build these h.f. circuits.

'Transistor Audio and Radio Circuits' is the latest of a number of Mullard books aimed at those whose interest lies in the audio and radio fields. It reflects the advances in electronic science since the earlier books were published, both in terms of devices and circuit techniques.

## AVAILABILITY OF COMPONENTS

All the Mullard devices mentioned in this book can be obtained through the usual trade channels. Other components, including meters and transformers, not marketed by Mullard are also readily obtainable; suitable components are manufactured by:—

### *Transformers*

Colne Electric Limited, Rickmansworth, Herts.  
Drake Transformers Limited, Billericay, Essex.  
Gardners Transformers Limited, Christchurch, Hants.  
Parmeko Limited, Aylestone Park, Leicester.

### *Meters*

Sifam Electrical Instrument Company Limited, Woodland Road, Torquay, Devon.  
Taylor Electrical Instruments Limited, Montrose Avenue, Slough, Bucks.

Printed-wiring boards for some of the audio circuits described in this book may be obtained from Bribond Printed Circuits Limited, Terminus Road, Chichester, Sussex.

## DATA ON MULLARD DEVICES

Abridged data on most of the Mullard devices mentioned in this book are given in the current edition of the Mullard 'Pocket' Data Book (U.K. edition).

Data on the few devices not included in the 'Pocket' Data Book can be obtained free of charge from Central Technical Services, Mullard Limited.

Complete data on all current Mullard devices are given in the Mullard Technical Handbook. Details of the Handbook can be obtained from Central Technical Services, Mullard Limited.

The circuits in this book are proven designs and it must be stressed that Mullard cannot undertake to answer queries arising from the information presented.

# CONTENTS

	Page
<b>CHAPTER 1 SILICON AND GERMANIUM TRANSISTORS ..</b>	<b>1</b>
<b>CHAPTER 2 BASIC H.F. CIRCUITS .. ..</b>	<b>11</b>
<b>CHAPTER 3 BASIC A.F. CIRCUITS .. ..</b>	<b>23</b>
<b>CHAPTER 4 RADIOGRAMS, RECORD PLAYERS AND PORTABLE RADIOS .. ..</b>	<b>33</b>
A.F. stages: 1W audio amplifier; 3W audio amplifier; 10W audio amplifier; pre-amplifier for use with 3W and 10W amplifiers; 3W record-player amplifier. I.F. and r.f. stages; a.m. receiver; a.m./f.m. receiver.	
<b>CHAPTER 5 TAPE RECORDERS .. ..</b>	<b>69</b>
4W tape recorder; tape pre-amplifier; modifications for stereo operation; automatic gain control.	
<b>CHAPTER 6 CAR RADIOS .. ..</b>	<b>89</b>
A.F. stages: 5W class A audio amplifier; 6W class B audio amplifier. I.F. and r.f. stages.	
<b>CHAPTER 7 HIGH-QUALITY AUDIO EQUIPMENT .. ..</b>	<b>101</b>
10W audio amplifier; 25W audio amplifier; pre-amplifier for use with 10W and 25W amplifiers; auxiliary amplifiers; auxiliary control circuits and filters; layout of high-quality equipment.	
<b>CHAPTER 8 HIGH-QUALITY F.M. TUNERS .. ..</b>	<b>145</b>
F.M. tuner using bipolar transistor; f.m. tuner using field-effect transistor; stereo decoder.	
<b>CHAPTER 9 TEST EQUIPMENT .. ..</b>	<b>173</b>
<b>Appendix 1 BIASING ARRANGEMENTS FOR H.F. CIRCUITS .. ..</b>	<b>185</b>
<b>Appendix 2 BBC TEST-TONE TRANSMISSIONS .. ..</b>	<b>191</b>
<b>Appendix 3 CHARTS AND NOMOGRAMS .. ..</b>	<b>193</b>



## CHAPTER 1

# SILICON AND GERMANIUM TRANSISTORS

Most transistors are made from either silicon or germanium. The early transistors were made from germanium because silicon presented many manufacturing problems, but these problems have been largely overcome by the development of the planar process. Silicon and germanium transistors are now produced concurrently, and there are applications for which each is the more suitable.

Certain characteristics of germanium semiconductor material limit the operating junction temperature of germanium transistors to below  $100^{\circ}\text{C}$ , while silicon devices can operate at temperatures in excess of  $150^{\circ}\text{C}$ . However, germanium transistors still have the advantage of a low value of forward base-emitter voltage and bottoming voltage and, since these two represent voltage losses in the circuit, germanium devices are particularly suitable for the lower-voltage type of a.f. output stage. Another advantage of germanium transistors is that they are easily matched in complementary (p-n-p/n-p-n) pairs, thus facilitating their use in complementary-pair push-pull output stages.

Because silicon has an extremely high intrinsic resistivity the leakage currents of silicon transistors are far smaller than those of germanium transistors. This advantage, together with the higher permissible junction temperature mentioned above, and the high voltage ratings available with silicon transistors, makes them ideal for a wide variety of audio applications, especially at high output powers where high voltages are necessary. Silicon planar transistors can be manufactured with high switching speeds, making these devices suitable for use at high frequencies, for example in the r.f. stages of radio receivers.

### TRANSISTOR MANUFACTURE

The manufacturing processes of germanium and silicon transistors both start with the production of a crystal of the doped semiconductor material. The crystal is then cut into thin slices and it is from this point on that the manufacturing processes differ.

## Germanium Transistors

Germanium transistors can be made by either of two methods—the alloy-junction method or the alloy-diffusion method. In the manufacture of a p-n-p transistor by the alloy-junction method, an emitter pellet of p-type material is fused to one side of the n-type slice and a collector pellet of p-type material is fused to the other side. In the alloy-diffusion method, a p-n-p transistor is made by depositing a layer of n-type material on one surface of the p-type slice and placing two pellets close together on the n-type layer. One of the pellets, which eventually forms the base connection of the transistor, contains n-type additives only, and the other pellet, which will form the emitter, contains p-type and n-type additives. The assembly is heated and the additives diffuse into the p-type germanium beyond the prediffusion layer. In this way a transistor is made in which the collector is formed by the original slice, and all diffusion has been effected on one side. The processes used in the manufacture of germanium transistors are now well known and will not be elaborated upon in the present book. The manufacture of a germanium alloy-junction transistor is summarised in Fig. 1.

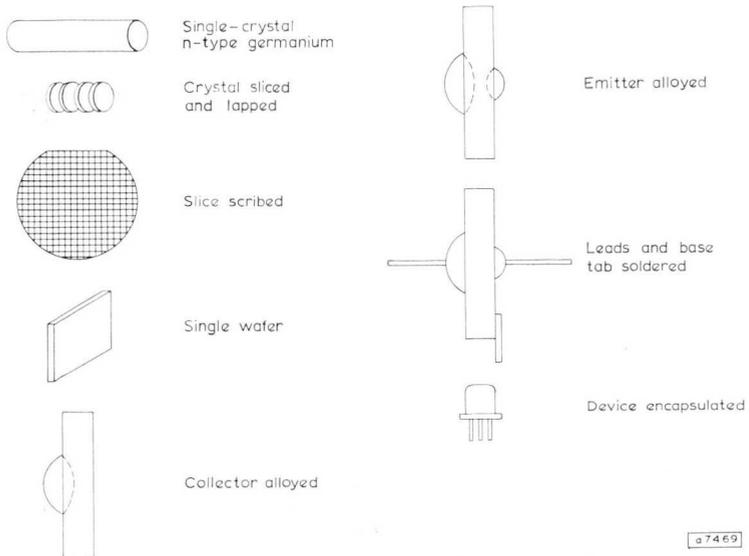


Fig. 1—Stages in the manufacture of germanium alloy-junction transistors

## Silicon Transistors

A process now widely used in the manufacture of silicon transistors is the planar process illustrated in Fig. 2. A slice of n-type silicon is cleaned under very stringent conditions and is then heated in oxygen so that a layer of silicon oxide is formed all over it. The oxidised slice is attached to the middle of a high-speed spinner, and a drop of photosensitive etchant-resistant material, or photoresist, is placed on it. When the spinner revolves, the photoresist spreads out in a thin, even coating. Some transistors, such as power transistors, need a thicker layer than others; in high-frequency transistors where well-defined edges are needed, a thin layer of photoresist is used. Hence, the spinning speed for power transistors is less than that for high-frequency transistors.

### *Base and Emitter Diffusion*

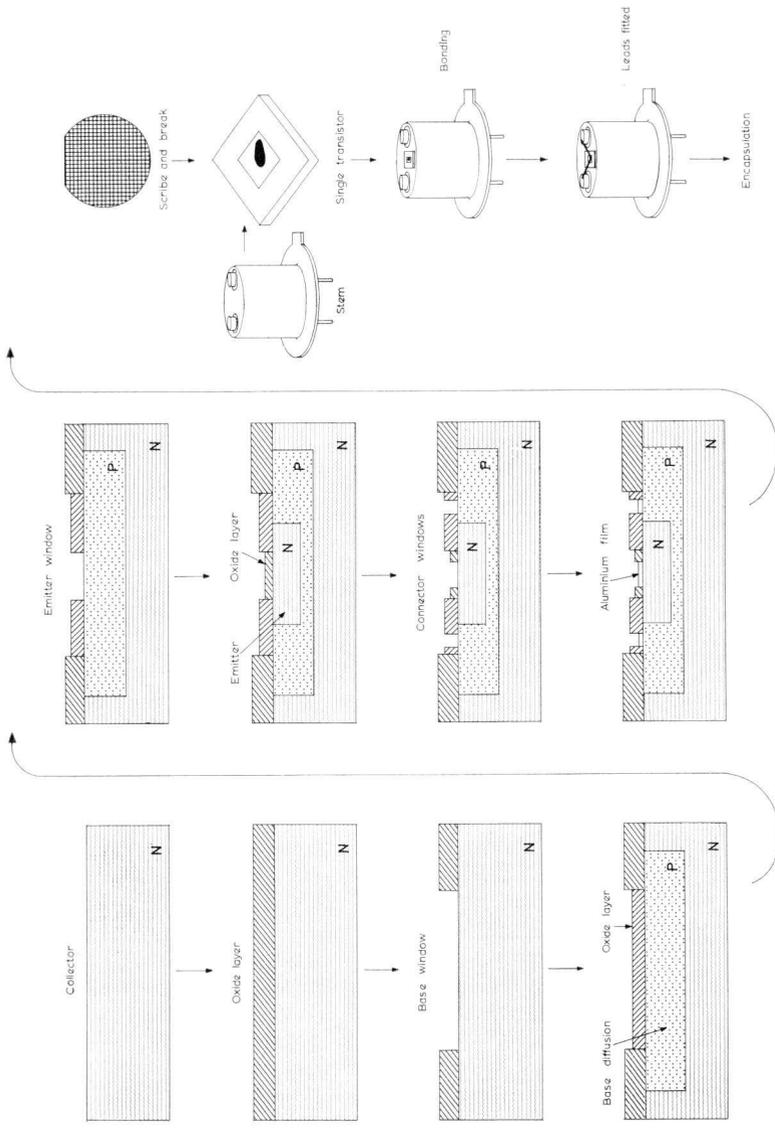
When the slice has been coated with the photoresist, it is covered with the base mask and exposed to ultraviolet light. The base mask is a photographic negative which carries a pattern formed by the proposed positions of the bases of the transistors that will be made from the slice.

The parts of the photoresist exposed to ultraviolet light change to a hard material which cannot easily be washed off, while the unexposed parts are easily removed. Therefore, after washing, there are many small windows in the photoresist, through which the silicon oxide is exposed. These windows are in the positions of the transistor bases.

The remaining photoresist is further hardened by baking the slice, which is then treated with acid to etch away the oxide exposed through the windows and reveal the silicon. The rest of the photoresist is then removed and the slice is ready for base diffusion.

When all the photoresist has been removed, the slice is again cleaned and placed in an oven with a little of the required p-type doping additive (usually boron). The additive evaporates and some of it settles in the windows. The slice is then transferred to a hotter oven filled with oxygen. In this oven, the additive is driven into the silicon to the required depth. At the same time, another oxide layer is formed all over the slice, including the windows. The base of each transistor in the slice has now been formed.

The slice is again covered with the photoresist and another pattern of windows produced as described above. This time, however, a different negative—the emitter mask—is used, and the windows are in the positions of the transistor emitters. The cleaning, diffusion and oxidation processes are repeated to form the transistor emitters. The doping additive used in this diffusion process, however, is not boron but phosphorus—an n-type substance.



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Fig. 2—Stages in the manufacture of silicon planar transistors

### *Lead Connections*

By means of the photoresist and a third negative, windows are produced over the base and emitter areas. The slice is placed in a vacuum and a fine layer of aluminium deposited all over it. The slice is removed from the vacuum and, by means of a fourth mask and another etching process, the aluminium is removed from all areas except where it is needed to provide contacts to the bases and emitters. The remaining aluminium is lightly alloyed to the bases and emitters to form non-rectifying contacts. At a later stage, fine gold or aluminium wires will connect the aluminium layer to the transistor leads or pins.

The oxide layer is now removed from the collector side of the slice, and the thickness of the slice is reduced by etching to lower the thermal resistance and improve the knee characteristic of the transistors.

The slice now contains between 200 and 6000 transistors, depending on the type of transistor, to which no leads have been attached. Each transistor is tested for breakdown voltage and small-signal current gain by means of a special probing machine connected to a test set. A photograph of this machine is given in Fig. 3. Transistors which fail any of these tests are marked and rejected at a later stage in manufacture.

After these tests, the slice is scribed with a diamond and broken into dice, each containing one transistor. At this stage, the marked transistors are rejected.

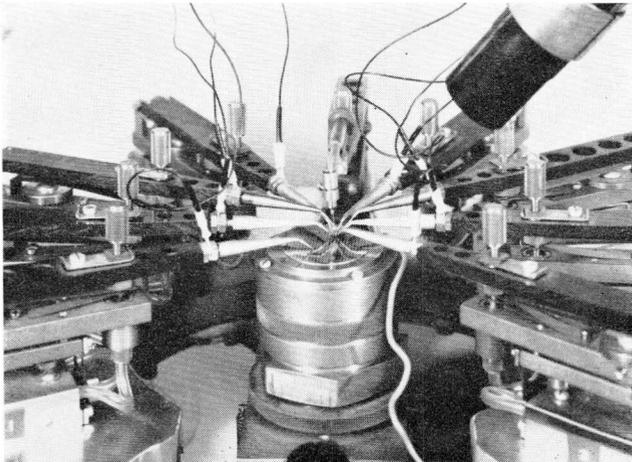


Fig. 3—Probing machine checking breakdown voltage and current gain of transistors

Each good transistor is soldered or bonded, collector side down, on the gold-plated stem or header. This operation is performed automatically on a dice bonder which fixes the transistor to the header by a silicon-gold eutectic.

The wires connecting the base and emitter to their leadout wires are usually of gold or aluminium, and are attached to the aluminium film on the transistor by means of a suitable bonder. When the leads have been attached, the transistors are encapsulated.

#### *Lockfit Encapsulation*

The familiar metal-can encapsulation requires no further description. However, a more modern encapsulation is epoxy resin, which is used on the range of Lockfit transistors. The coating of epoxy material provides the semiconductor wafer with complete environmental protection, and the junction-to-ambient thermal conductivity of the material is superior to that obtained with most metal encapsulations. The transistor leads take the form of flat pins which are designed to snap into printed-wiring board as shown in Fig. 4.

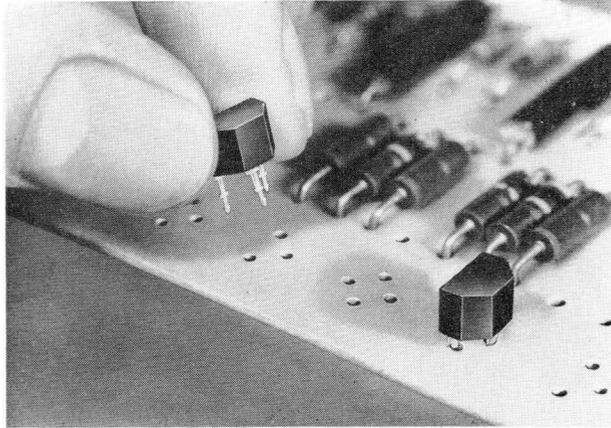


Fig. 4—Insertion of Lockfit transistors in printed-wiring board

The encapsulated transistors are subjected to a temperature cycling test, a drop test and a test to detect pinholes in the encapsulation.

## Epitaxy

When special types of silicon planar transistor are required, the procedure is modified slightly. When, for example, transistors are required for r.f. and i.f. applications, the silicon substrate is more heavily doped than in other transistors, and it undergoes further treatment in the crystal-growing chamber before being cleaned and covered with the first coat of photoresist. Consequently, the slice is covered with a thin layer—5 to 20 micrometres thick—of lightly-doped silicon. This layer has the same crystal orientation as the original slice and is therefore known as the epitaxial layer. The subsequent treatment of the slice with the epitaxial layer is the same as previously described. In the epitaxial type, however, the transistor is essentially within the thin layer, and the substrate is really a low-resistance back contact which provides a convenient thickness for handling. With the non-epitaxial type, the transistor is within the substrate.

## Field-effect Transistors

Despite the differences in materials and methods of manufacture, the transistors described in the earlier sections of this chapter all have essentially the same construction and principle of operation. They all consist of emitter, base and collector regions, and their properties are all largely a consequence of the movement of electrons and holes across the junctions between these regions or of the existence of the junctions themselves. The field-effect transistor, however, has a structure and characteristics differing from the conventional junction transistor.

### Structure and Operation

Fig. 5 is a schematic diagram of a field-effect transistor. It will be seen that a channel of n-type semiconductor material is enclosed for part of

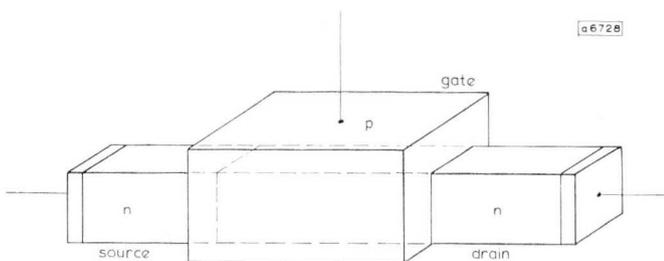


Fig. 5—Schematic diagram of a field-effect transistor

its length by a collar of p-type material. One end of the n-type channel is called the source, and the other end is called the drain. The collar of p-type material is the gate.

If a voltage is applied across the length of the n-channel so that the source is positive with respect to the drain, electrons will flow from the drain to the source; that is, current will flow conventionally from the source to the drain.

If a voltage is applied to the gate so that the gate is negative with respect to the source, the p-n junction formed between the gate and channel will be reverse-biased. No current flows across the junction, but the recombination of holes and electrons that migrate across the junction forms a region in the n-channel depleted of free electrons.

This non-conductive depletion region narrows the conductive n-channel, and thus reduces the current flowing from source to drain. Varying the gate bias voltage will thus vary the source-drain current. The action is analogous to the control of anode-cathode current in a triode valve by means of a negative bias voltage applied to the grid of the valve.

In the field-effect transistor, as in the triode valve, a comparatively small bias voltage will control a large current. Therefore amplification of a signal is possible with the field-effect transistor.

Since the gate-channel junction is reverse-biased during operation, the field-effect transistor is essentially voltage driven, and it therefore has a high input impedance. The device has a low noise figure and good high-frequency performance. For these reasons, field-effect transistors are ideal for use in such applications as the r.f. stages of high-quality f.m. tuners.

### *Manufacture*

The structure of an n-channel field-effect transistor is shown in Fig. 6. The planar process is employed in the manufacture of these transistors.

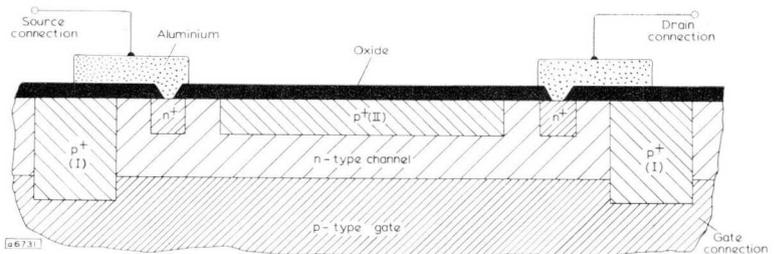


Fig. 6—Structure of a field-effect transistor

An n-type epitaxial layer which eventually will form the n-channel is grown on a substrate of high-conductivity p-type material, which will form the gate. After oxidation of the surface of the epitaxial layer, windows are etched in the oxide layer corresponding to the channel-isolating region I. Through these windows is diffused an additive rich in holes, which creates a 'super-p' or  $p^+$  region penetrating through the epitaxial layer to the p-type substrate, and thus isolating the n-channel.

After re-oxidation, a window is etched corresponding to region II, and another  $p^+$  region is created to form the upper part of the p-gate surrounding the n-channel.

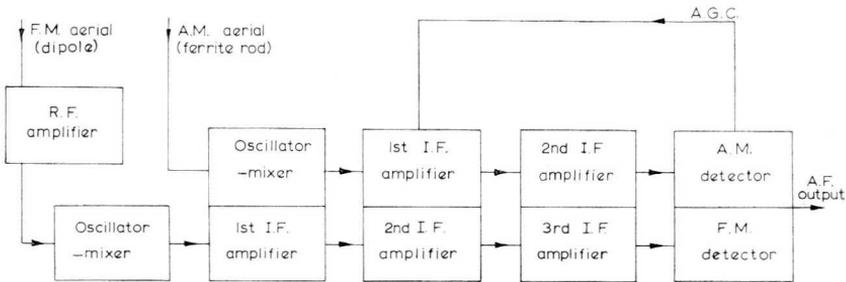
A third diffusion is performed to create 'super-n' or  $n^+$  regions at the ends of the n-channel. Aluminium bonds are deposited on these  $n^+$  regions, and to these are connected the source and drain contact wires. The purpose of the  $n^+$  region is to diminish the series resistance of the source and drain contacts. The gate contact is made to the p-type substrate, and the transistor is encapsulated in a metal envelope.



## CHAPTER 2

# BASIC H.F. CIRCUITS

The block schematic diagram for the high-frequency stages of a typical a.m./f.m. radio receiver is given in Fig. 7. The audio-frequency, or a.f., output is fed to one of several types of a.f. amplifier, which are discussed more fully in Chapter 3. In the present chapter, the operation of each of the circuits named on the block diagram is discussed in general terms, detailed practical circuits being given in later chapters.



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Fig. 7—H.F. stages of a typical a.m./f.m. receiver

### R.F. AMPLIFIER

A typical basic r.f. amplifier circuit is shown in Fig. 8. The transistor is connected in the common-base configuration because this configuration gives the highest gain at frequencies approaching the cut-off frequency. The collector circuit is tuned and is inductively coupled to the self-oscillating mixer circuit.

### MIXER

The mixer, or frequency changer, converts by heterodyne or 'beating' action the wanted frequency of the carrier signal at the aerial to a fixed frequency at the input to the i.f. amplifier. The a.m. carrier frequencies

vary from 160 to 280kHz in the long waveband and from 540 to 1640kHz in the medium waveband. The f.m. carrier frequencies vary from 85 to 100MHz. The intermediate frequency is usually 470kHz for a.m. and 10.7MHz for f.m. The audio-frequency information, carried on the r.f. waveform as modulation of the amplitude or frequency, is transferred from the r.f. carrier signal to the i.f. carrier.

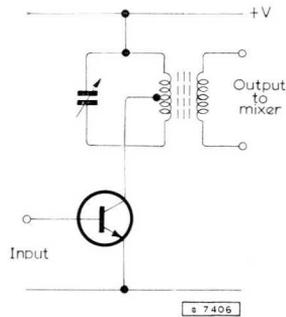


Fig. 8—Basic r.f. amplifier circuit

Heterodyne action is effected by injecting signals of different frequencies into a non-linear element such as the base-emitter diode of a transistor. In a radio receiver, one injected signal is the aerial signal, derived either directly or through an r.f. amplifier, and the other is a signal generated within the receiver by a local oscillator. The signals combine as shown in Fig. 9 to produce a complex waveform. When the waveform is applied between the base and emitter of a transistor, the main components occurring in the collector waveform are the original aerial and oscillator frequencies together with their sum and difference frequencies. The difference frequency (i.f. signal) is preferentially selected by the tuned circuit in the collector of the mixer, and further selectivity is provided by the i.f. amplifier stages. Voltage gain is obtained from the mixer stage in the same manner as the gain obtained from a normal i.f. amplifier, but somewhat reduced in magnitude.

To maintain a constant difference between the aerial and oscillator frequencies, the oscillator frequency must be changed whenever the aerial frequency is changed, that is, the oscillator tuned circuit must 'track' the aerial tuned circuit. Therefore, if the aerial is tuned to 1.5MHz, the local oscillator must be tuned to 1.97MHz, to give a difference frequency of 470kHz, and if the aerial tuning is changed to 1MHz, the oscillator

must be tuned to 1.47MHz. For a.m. reception, the oscillator is usually tuned to frequencies 470kHz above the aerial frequency so that signals in the long waveband, which have frequencies below 470kHz, can be accepted. For f.m. reception the oscillator frequency may be 10.7MHz above or below the aerial frequency dependent upon other design considerations.

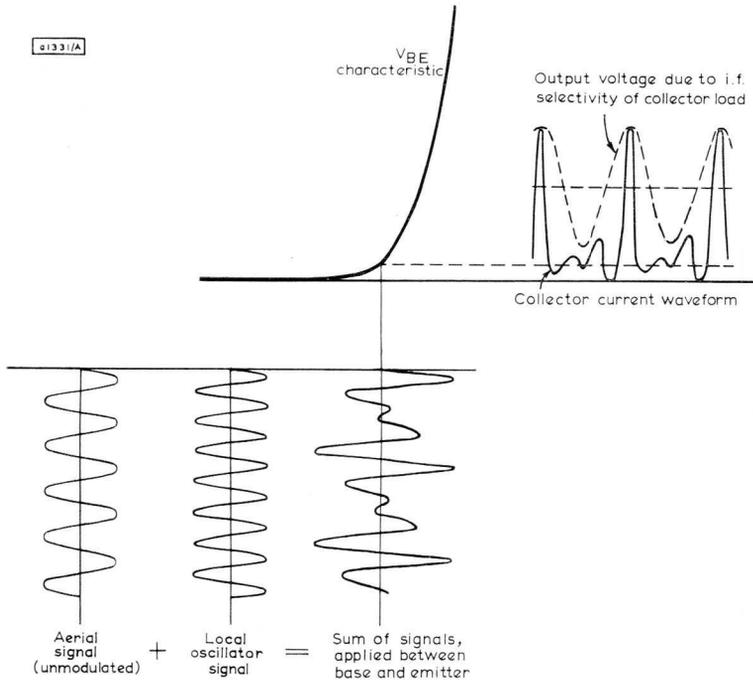


Fig. 9—Diagram illustrating the action of a mixer transistor

### SELF-OSCILLATING MIXER

The local-oscillator signal applied to the mixer may be derived from a separate oscillator transistor in the receiver or one transistor may act as both oscillator and mixer. This latter arrangement is the more common and is known as a self-oscillating mixer.

The basic circuit of a self-oscillating mixer is shown in Fig. 10. At the oscillator frequency, the base of the transistor is effectively connected to earth because the aerial tuned circuit has negligible impedance. The input

electrode for the oscillator action is, therefore, the emitter, which is inductively coupled to the collector of the transistor. Both the emitter winding and the collector winding are closely coupled to the oscillator tuned circuits. Positive feedback is applied from output to input through this coupling, and oscillation occurs at the resonant frequency of the oscillator tuned circuit. The aerial signal is applied from the aerial tuned circuit to the base of the transistor. Both the aerial signal and the oscillator signal are, therefore, in series with the base-emitter diode. The component of the heterodyne output signal having the required intermediate frequency is extracted by the i.f. bandpass filter or transformer in the collector circuit.

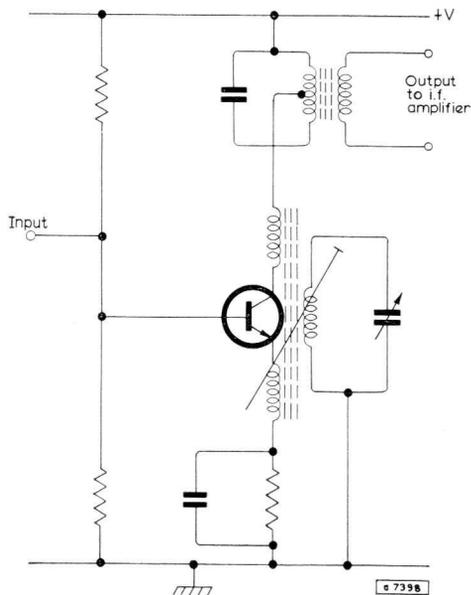


Fig. 10—Basic self-oscillating mixer circuit

A typical self-oscillating mixer for a.m. reception is shown in Fig. 11. The circuit is shown for one waveband only, the different wavebands being obtained by switching other coils into the aerial circuit and additional capacitors into the oscillator circuits. The aerial input is taken to the base of the transistor, and the oscillator feedback from the collector is taken through low-impedance coupling coils to the emitter.

To ensure that the oscillation starts easily, the transistor is biased initially for class A operation by the potential-divider bias circuit. As the oscillation increases in amplitude, rectification of the oscillating signal occurs at the base-emitter diode. This causes the loop gain after each cycle to decrease, stabilising the amplitude of the oscillation and causing the quiescent emitter current to rise slightly (from 250 to 300 $\mu$ A in the circuit shown in Fig. 11).

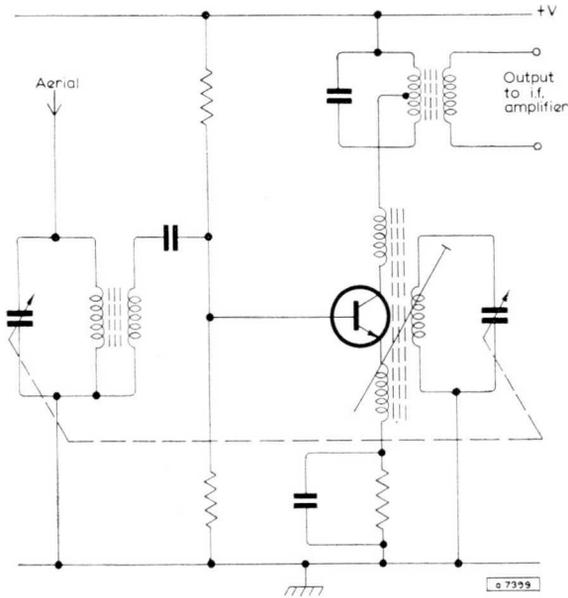


Fig. 11—Typical practical self-oscillating mixer circuit

Correct tracking of the aerial and oscillator tuned circuits to maintain the 470kHz difference in frequency can be obtained by a conventional padder circuit or by using a tuning capacitor with specially-shaped vanes for the oscillator circuit. The value of the tuning capacitance is not critical but must be sufficient to provide the required frequency coverage.

Stray capacitance can exist between the aerial and oscillator sections of the tuning capacitor and so form a path for unwanted feedback between the two sections. To prevent this feedback and the resulting possibility of spurious oscillations, a screen is usually placed between the two sections. Another source of feedback between the oscillator and aerial sections is

through the stray capacitance of the leads to the wave-change switch, and these leads should, therefore, be kept as short as possible.

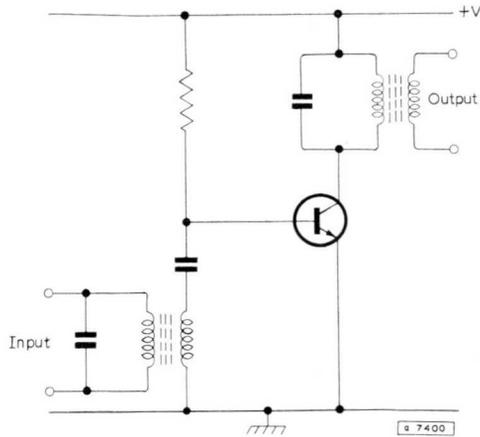


Fig. 12—Basic i.f. amplifier circuit

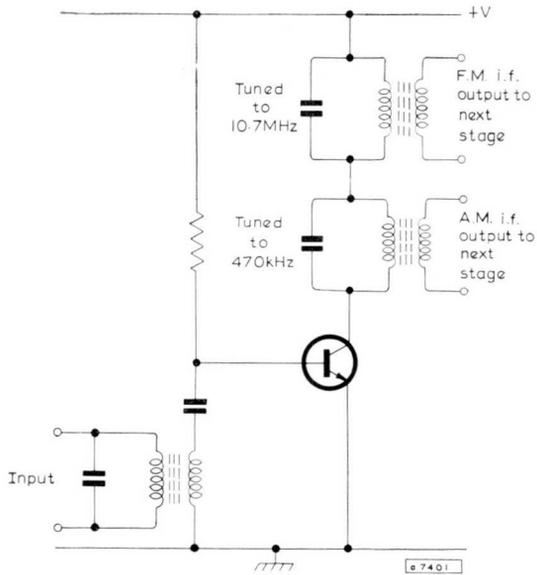


Fig. 13—Basic i.f. stage for an a.m./f.m. receiver

## I.F. AMPLIFIER

The basic circuit of an i.f. amplifier stage is shown in Fig. 12. The input and output transformers are tuned to the intermediate frequency, the selectivity and bandwidth being improved if both windings of the transformers are tuned. In an a.m./f.m. receiver it is necessary for two i.f. transformers to be provided between stages—one tuned to 470kHz and the other to 10.7MHz. A method of connecting these i.f. transformers is illustrated in Fig. 13. The remaining i.f. stages are similar to the first except that, in an a.m./f.m. receiver, the a.m. and f.m. outputs must be separated so that each can be fed to its own detector circuit.

## DETECTOR

The a.m. detector of a transistor receiver is usually a semiconductor diode feeding a potentiometer load. The potentiometer forms the volume control, which feeds the demodulated signal to the audio-frequency stages of the receiver. The potentiometer is usually shunted by a 10nF capacitor, as shown in Fig. 14, to filter out the i.f.

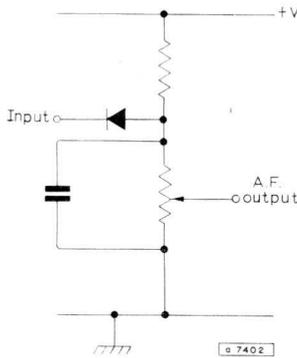


Fig. 14—Basic a.m. detector circuit

The detector stage for f.m. signals is usually of the type known as a ratio detector, the basic circuit of which is shown in Fig. 15.

The ratio detector depends for its operation on the fact that as the frequency of the signal varies, the phase relationships in a circuit tuned to the nominal frequency change. The transformer has three windings, the primary and secondary tuned to the intermediate frequency and the tertiary, close-coupled to the primary, injecting a voltage into the secondary

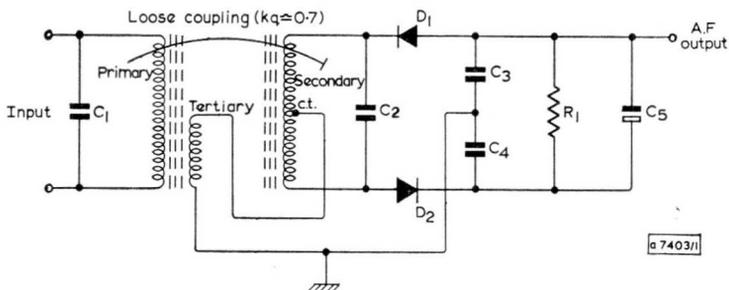


Fig. 15—Basic ratio detector circuit

in series with the voltage across each half of the secondary. Figs. 16 and 17 show the phase relationships. In Fig. 16, the voltage  $V_S$  induced in each half of the secondary is  $90^\circ$  out of phase with the injected primary voltage  $V_P$  at the intermediate frequency. Voltage  $V_{D1}$  and  $V_{D2}$ , applied to the detector diodes, are equal in magnitude, so there is no audio output. Fig. 17 shows the phase conditions when the frequency of the signal differs from the nominal value. The effect of a shift in frequency is to change the phase of the secondary voltage with respect to the injected primary voltage. As the frequency of the signal sweeps above and below the nominal value the variation of the relative phase of the injected primary and secondary voltages produces a variation in the amplitudes of  $V_{D1}$  and  $V_{D2}$  at audio frequency. The voltages are rectified by the two diodes and the a.f. signal taken from across either  $C_3$  or  $C_4$ . The long-time-constant circuit  $R_1C_5$  suppresses any unwanted a.m. signals.

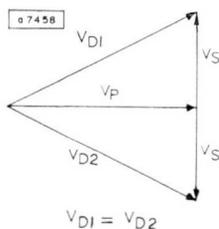


Fig. 16—Vector diagram of voltages in a ratio detector circuit with signal at nominal frequency

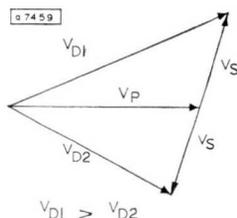
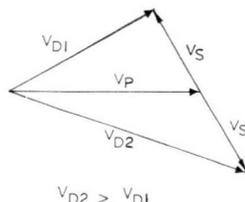


Fig. 17—Vector diagram of voltages in a ratio detector circuit with signal varying from nominal frequency



## AUTOMATIC GAIN CONTROL

It is necessary for the sensitivity of r.f. and i.f. stages in a receiver to be high, so that weak signals are amplified to give a useful output. However, if no automatic control of gain were incorporated in an a.m. receiver, clipping would occur when the receiver was tuned to a strong signal. The automatic gain control (a.g.c.) signal, proportional to the i.f. output, is derived from the detector and applied in series with the base-emitter voltage of the first i.f. transistor (and the r.f. transistor in car radios). The a.g.c. signal therefore controls the bias, and hence the gain, of the transistor. The simplest method of modifying the basic detector and i.f. amplifier is shown in Fig. 18.

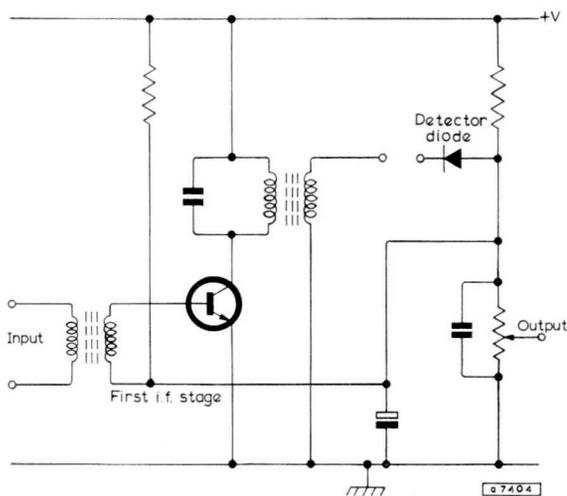


Fig. 18—Simple a.g.c. circuit

To eliminate the audio- and radio-frequency signals from the a.g.c. voltage, the decoupling capacitor of the potential divider feeding the base of the first i.f. transistor is large— $8\mu\text{F}$  is a typical value. The a.g.c. characteristic may be improved by adding a damping diode across the first i.f. transformer. This diode ensures that the a.g.c. action is effective over a larger range of r.f. input voltages than in a normal circuit.

In f.m. receivers the waveform is already limited for a.m. suppression and a.g.c. is generally thought to be unnecessary, although it may be included to improve the performance of the i.f. stages.

## BIAS AND STABILISATION AGAINST TEMPERATURE VARIATIONS

In the foregoing discussion of r.f. and i.f. circuits, no mention is made of biasing requirements. The operating current of a transistor is determined by the biasing voltages or currents applied to it, and these are usually set by means of resistors in the base, emitter and collector circuits. Because of the superior high-frequency performance of silicon transistors, germanium devices are not used in any of the r.f. and i.f. stages described in this book. Therefore only biasing arrangements for silicon transistors in these stages are described in detail.

Ideally, biasing circuits should allow a particular value of operating current to be obtained irrespective of changes in supply voltage and temperature; and spreads in the current amplification factor,  $h_{FE}$ , and the base-emitter voltage,  $V_{BE}$ , of the transistor. Unless an external stabilising element is used, it is impossible to eliminate the effects of variations in supply voltage; but in a good biasing arrangement, the resulting variations in current will not be much greater than the percentage variations in the supply voltage.

Different biasing arrangements satisfy these requirements to different degrees. The biasing arrangement shown in Fig. 19 has been almost universally adopted for low-level class A amplifiers using germanium transistors. In this arrangement the current is only slightly influenced by spreads in  $h_{FE}$ , but a value of emitter voltage greatly in excess of  $V_{BE}$  is required if the current variations resulting from supply voltage variations are to be small. On the other hand, a single biasing resistor in the base circuit, as shown in Fig. 20, gives negligible changes in current with  $V_{BE}$  variations, but the current in this circuit is fully dependent on spreads in  $h_{FE}$ .

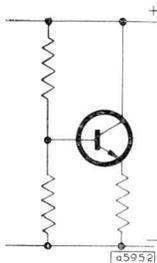


Fig. 19—Conventional voltage - biased transistor

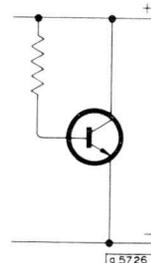


Fig. 20—Conventional current-biased transistor

The two major differences between the characteristics of silicon and germanium transistors that affect the biasing arrangements occur in the base-emitter voltage  $V_{BE}$  and collector leakage current  $I_{CBO}$ . The base-emitter voltage of silicon transistors at low currents is 0.6 to 0.7V, and of germanium transistors, 0.1 to 0.2V; the typical mutual characteristics of a silicon and a germanium transistor are compared in Fig. 21. The difference in  $V_{BE}$  is equivalent to a difference in 'starting' voltage, but the rate of change of current with base-emitter voltage above this 'starting' voltage is identical for silicon and germanium transistors. The only consequence of this difference in  $V_{BE}$  is that, for conventional voltage biasing shown in Fig. 19, a larger drop across the emitter resistor will be required with silicon transistors than with germanium transistors for comparable changes in operating current with supply voltage, unless a stabilised source of bias voltage is available.

The collector leakage current in silicon transistors is negligible up to the highest temperatures likely to be encountered in radio equipment. Consequently, it would seem to be possible to use a high value of d.c. base source resistance, and to dispense with the normal stabilising circuit, which applies negative d.c. feedback to stabilise the operating conditions. However, other effects need consideration and these may necessitate retaining the stabilising circuit and limiting the magnitude of the source resistance. These effects are variations in supply voltage, spreads in  $V_{BE}$  and  $h_{FE}$ , and variations in  $V_{BE}$  and, to a lesser extent,  $h_{FE}$  with temperature.

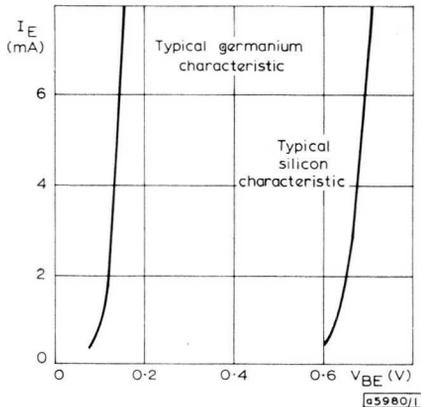


Fig. 21—Typical mutual characteristics of a germanium and a silicon transistor

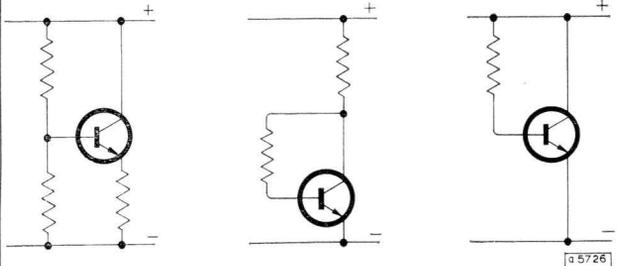
The three most common biasing arrangements are voltage biasing with emitter feedback, current biasing with collector feedback and simple current biasing. The choice of biasing arrangement depends very much on the supply voltage, the proportion of this voltage that can be dropped across a feedback resistor, and the type of transistor used. A comparison of the spread in emitter operating current resulting from spreads in  $h_{FE}$  and  $V_{BE}$ , for each of the three biasing arrangements, is given in Table 1. The changes in operating current when the supply voltage falls to half its nominal value are also compared. An analysis of the biasing arrangements, and worked examples showing their relative effectiveness, are given in Appendix 1.

**TABLE 1**  
**Comparison of Biasing Arrangements**

Nominal values of parameters:

$$V_S = 7V; V_{BE} = 0.7V; h_{FE} = 100$$

$$I_E = 1mA \text{ (approx.)}$$

Biasing arrangement			
	I <sub>E</sub> variation		
$h_{FE} \pm 50\%$	+1, -1.6%	+23, -35%	$\pm 49\%$
$V_{BE} \pm 7\%$	$\pm 1.7\%$	$\pm 0.95\%$	$\pm 0.86\%$
$V_S -50\%$	-62%	-55%	-56%

## CHAPTER 3

# BASIC A.F. CIRCUITS

Audio-frequency amplifiers range from the simple amplifier used in small portable radio receivers, where size and cost are the important factors, to the large multi-stage circuit where cost is of little importance but reproduction of the highest quality is required. In the present chapter, only the basic amplifying stages are considered, the refinements necessary for high-fidelity reproduction being considered in Chapter 7.

The only class of one-transistor amplifier stage in common use is class A. Push-pull stages, either using two similar transistors or a matched complementary pair, may operate in class AB or class B. A special type of class AB push-pull amplifier sometimes encountered is known as ' $\pi$ -mode'.

### CLASS A OPERATION

Class A operation is that in which the values of bias and signal voltage applied to the transistor ensure that collector current always flows. Class A output stages are used mostly in car radios, where current drain is relatively unimportant, although class A circuits are invariably used as the earlier stages of multi-stage amplifiers where the current level is comparatively low. Class A, one-transistor output amplifiers are inefficient and have the additional disadvantage of suffering from even as well as odd harmonic distortion, although they are simple and enable moderate powers to be obtained from circuits consisting of very few components.

A basic class A output stage is shown in Fig. 22. The bias is provided by resistors  $R_1$  and  $R_2$ , and resistor  $R_3$  provides thermal stabilisation.

### PUSH-PULL OPERATION

Push-pull output stages are used almost universally in modern amplifier circuits, and push-pull circuits are often used in the driver stages of multi-stage amplifiers. The output power obtained from a pair of transistors connected in a push-pull configuration is considerably more than double the power obtained from one transistor. Push-pull operation also gives rise to less of the even harmonics sometimes associated with single-transistor, class A amplifiers. The use of transistor push-pull driver and

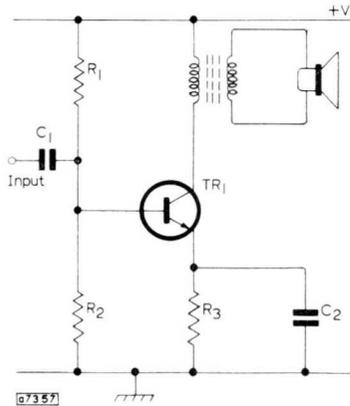


Fig. 22—Basic class A output stage

output circuits has eliminated the need for driver and output transformers, which were an essential part of valve push-pull circuits.

In a class B push-pull output stage, two transistors are biased nearly to cut-off, so that only a small quiescent current flows under zero-signal conditions. The signal is applied in antiphase to each transistor by means of some kind of phase-splitting arrangement, so that one transistor is cut off while the other conducts. With push-pull operation, the efficiency is 60 to 65% and the average current drain is low compared with class A operation. This low current drain is, of course, a great advantage in portable battery receivers.

If both transistors are biased exactly to cut-off, a form of distortion occurs which is extremely unpleasant to the listener. This is called 'crossover' distortion and is overcome by applying a slight forward bias to each transistor.

Output transistors dissipate considerable amounts of power and are, therefore, usually fitted with some kind of heatsink.

Because push-pull circuits using complementary pairs have virtually superseded those using two similar transistors in all but the output stages of high-power amplifiers, they are considered first.

### Complementary Push-Pull Circuits

A basic complementary push-pull output stage is shown in Fig. 23. The signal from the driver transistor  $TR_2$  is applied simultaneously to the bases of the two output transistors,  $TR_3$  and  $TR_4$ , which conduct during alternate halves of the waveform. The amplified signal, occurring as

variations in the potential at point A, is applied via capacitor  $C_4$  to the loudspeaker. The collector load of the driver transistor is returned to the live end of the loudspeaker so that the signal is applied between base and emitter of the output transistors. The output devices therefore operate in common-emitter, giving maximum amplification.

The quiescent bias voltage for the output transistors is developed across a resistor  $R_7$  placed in the collector circuit of the driver transistor. Since the value of  $R_7$  is much lower than the value of  $R_8$  its inclusion does not introduce any significant imbalance at the input of the output transistors. Resistors  $R_9$  and  $R_{10}$  are included in the emitter circuits of the output transistors to improve thermal stability.

Transistor  $TR_1$  acts as a pre-amplifier for a.c. signals and as a d.c. difference-amplifier comparing the voltage  $V_1$ , derived from the potential divider  $R_1$ ,  $R_2$ ,  $R_3$ , with voltage  $V_2$ . The high loop gain of the circuit keeps the small difference between  $V_1$  and  $V_2$  constant, so that  $V_2$  is defined with respect to  $V_1$  regardless of spreads in the characteristics of transistors  $TR_1$  and  $TR_2$  and the tolerance variations in values of  $R_5$ ,  $R_6$ ,  $R_7$  and  $R_8$ .

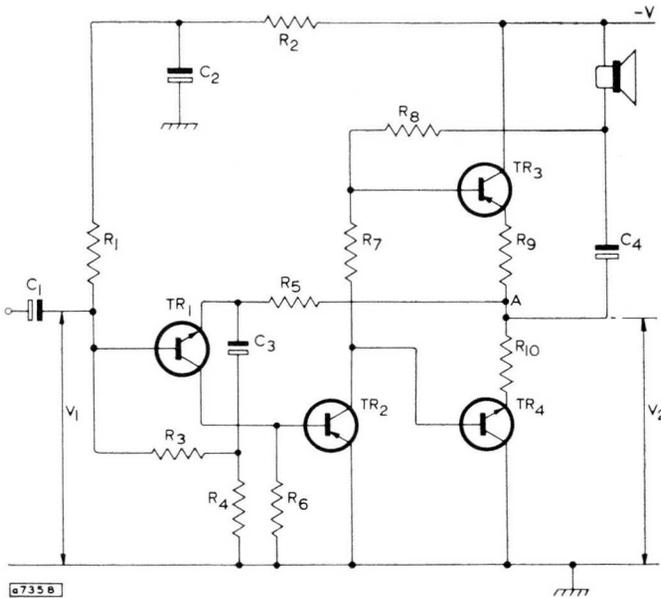


Fig. 23—Basic complementary push-pull circuit

Negative feedback is taken via resistor  $R_5$  from the output to the emitter of  $TR_1$ . Decoupling is provided by capacitor  $C_3$  to remove a.c. feedback between these two points, and a known small amount of feedback is re-introduced by means of  $R_4$  to reduce gain spreads and distortion.

Crossover distortion can be eliminated by biasing the output transistors to give a linear combined transfer characteristic. For a given output stage, an optimum bias condition (and quiescent current) exists for which the crossover distortion is a minimum. Changes in supply voltage or ambient temperature, however, will cause departures from this optimum and therefore increase the crossover distortion.

Considerable spreads about the nominal current may result from tolerance spreads in resistor values and transistor characteristics, and from variations in ambient temperature and supply voltage. The effects of changes in ambient temperature can be minimised by the use of a thermistor in conjunction with the biasing resistor,  $R_7$ , which can be preset to compensate for component spreads. The effects of supply voltage changes can be minimised by means of a diode or other stabilising device from which the bias can be derived.

### **Zobel Network**

The purpose and operation of the Zobel network can be explained by considering the simple complementary-pair output stage shown in Fig. 24. The operating limits of this circuit are defined by the continuous line in Fig. 25. While the load line remains within the enclosed area, the transistors will not be damaged by overloading. With a purely resistive load, this is a fairly easy matter to arrange. However, if the load is inductive, the limits could be exceeded during transients when the amplifier receives a large signal.

In extreme cases, too large a signal to the driver approximates to a large square wave. When such a signal first bottoms the driver transistor, current flows from  $TR_2$  into the load. On the next sharp edge of the input signal,  $TR_1$  is rapidly cut off. With a purely resistive load,  $TR_2$  is cut off,  $TR_3$  conducts, and the current reverses immediately. With an inductive load, however, the inductance opposes the change of current and the potential at point A rapidly decreases.

If the line voltage is less than the maximum permissible voltage of  $TR_2$ , the potential at A will become slightly negative until  $TR_3$  acts as a reverse transistor. The energy stored in the inductance is then safely dissipated before breakdown occurs.

However, if the line voltage exceeds the maximum permissible voltage of  $TR_2$ , the voltage across  $TR_2$  will reach the maximum permissible voltage before A becomes negative. Consequently, the energy stored in

the inductance will be dissipated in the breakdown region of TR<sub>2</sub> and may be sufficient to cause failure of the transistor. Failure of TR<sub>2</sub> will be followed by failure of TR<sub>3</sub> as this will then be subjected to the full line voltage.

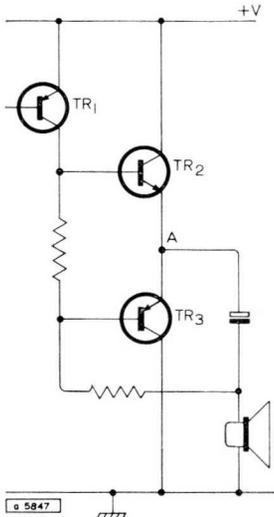


Fig. 24—Basic complementary-pair output stage

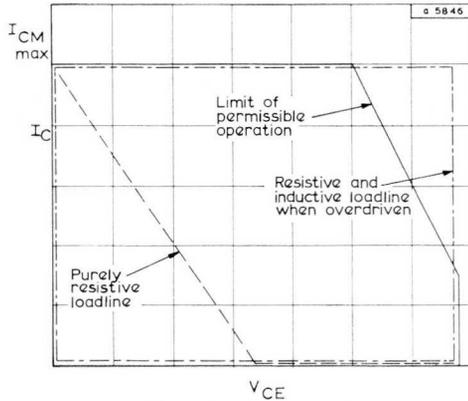


Fig. 25—Operating limits and load lines for a transistor in a complementary pair

As nearly all loudspeakers contain inductance, output circuits must be designed to allow for it. This can be done either by using transistors with high breakdown voltages or by taking precautions to prevent the conditions for transistor breakdown being satisfied. If the transistors were presented with a purely resistive load, the breakdown of TR<sub>2</sub> would not occur. This can be achieved by connecting a Zobel network in parallel with the loudspeaker as shown in Fig. 26. The Zobel network is a capacitance, C<sub>Z</sub>, in series with a resistance, R<sub>Z</sub>, the values of these components having a certain relationship to the inductance and resistance of the loudspeaker. If the loudspeaker is equivalent to a resistance, R<sub>S</sub>, in series with an inductance, L<sub>S</sub>, the components of the Zobel network must have values given by

$$R_Z = R_S$$

and

$$C_Z = \frac{L_S}{R_S^2}$$

When these conditions are satisfied, the parallel combination of the loudspeaker and the Zobel network will present a purely resistive load to the output transistors. In practice, of course, the impedance of the loudspeaker is only approximately a resistance in series with an inductance. Consequently, the use of a Zobel network will not result in a perfect resistive load, but the similarity is very close.

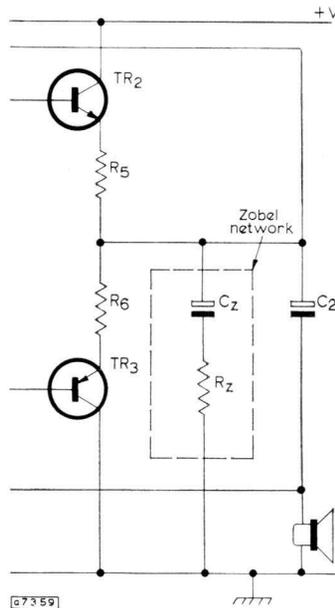


Fig. 26—Basic complementary push-pull circuit with Zobel network

### Push-pull Circuits using Two Similar Transistors

The complementary push-pull circuit is normally used for amplifiers with low output powers, but the push-pull circuit using two similar transistors is still often used as the output stage of high-power amplifiers. This is because n-p-n silicon transistors capable of handling high powers are more readily available than p-n-p transistors. The most usual arrangement for high-power amplifiers is for an output stage consisting of two n-p-n transistors connected in a push-pull configuration to be driven by a

complementary push-pull circuit as shown in Fig. 27 (quasi-complementary configuration).

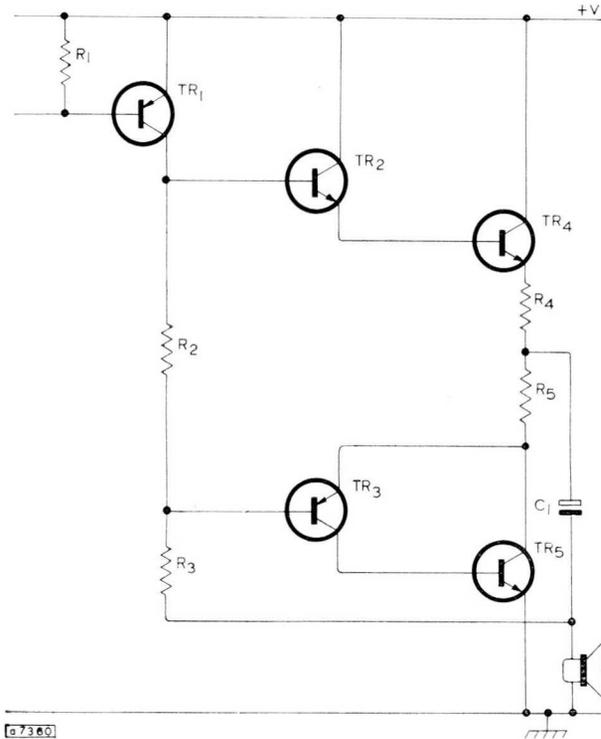


Fig. 27—Push-pull output stage using two n-p-n transistors driven by a complementary push-pull circuit

### Pi-Mode Operation

Class AB operation is that in which the values of bias and signal voltage applied to the transistor cause collector current to flow for appreciably more than a half, but less than a whole, cycle of the signal voltage.

A class AB amplifier which operates in the  $\pi$ -mode differs from a normal class AB amplifier in that the total current remains constant with drive. Increasing the level of drive causes the operating point of the transistors to change first from class A to AB and then to class B.

With  $\pi$ -mode operation, the problem of crossover distortion associated with straight-forward class B operation does not arise. Regulation of the

power supply is not important since, with  $\pi$ -mode operation, the current drain from the supply is constant and adequate smoothing of the power supply can be obtained by simple RC filtering. Distortion at normal listening levels is very low since the transistors operate in class A at low power levels and, with the use of emitter-loaded operation, the distortion of the amplifier over the full power range can be controlled to specific limits by a suitable choice of driver-stage source impedance.

The chief disadvantage of  $\pi$ -mode operation is that it requires a relatively large number of transistors to give the required power output.

### **CLASS D OPERATION**

Class D operation differs from the modes of operation already considered in that the output transistors are used as switches in a single-ended push-pull arrangement. The transistors are fed with a square wave which carries the audio information as pulse-width modulation. The transistors switch the load between positive and negative voltages, the duration for which it is switched to either supply depending on the mark/space ratio of the input waveform. The transistor output is coupled to the load through a low-pass filter which removes the high-frequency content and feeds an audio-frequency waveform to the load.

This arrangement makes use of the fast switching times and low saturation voltages of the modern switching transistor. It offers potential benefits over other modes of operation: only the amount of power supplied to the load at any instant is drawn from the power supply and no excess power is converted to heat by the output transistors; the linearity of the circuit is independent of the transistors; large component tolerances are acceptable because the transistors alternate between fully 'off' and fully 'on', and no biasing currents are required; efficiencies of 95% can be realised and a large range of load impedances can be connected without substantially affecting efficiency. However, the high-speed circuitry and radiation due to fast switching present problems, and this concept is still in the development stage. No class D circuits are given in this book.

### **LOUDSPEAKER DIVIDING NETWORK**

In the practical circuits which follow this chapter, the only loudspeaker specification quoted is impedance. However, it should be pointed out that the choice of loudspeaker is important in any audio system and that a dual system is invariably preferable to a single unit.

In a dual system, two speakers—one for high frequencies (the tweeter) and one for low frequencies (the woofer)—are used, together with a suitable crossover network to divide the audio output into two ranges. Loudspeaker manufacturers often recommend a suitable network and it is advisable to

follow their recommendations. However, an example of a two-way network is shown in Fig. 28. The values of inductor  $L$  and capacitor  $C$  are given in terms of loudspeaker impedance  $R$  and crossover frequency  $f$  by the following equations:

$$L = \frac{R\sqrt{2}}{2\pi f},$$

$$C = \frac{\sqrt{2}}{4\pi fR}.$$

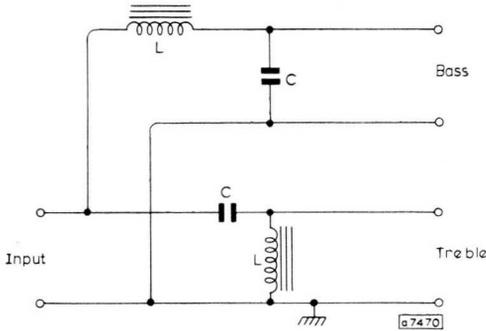


Fig. 28—Loudspeaker dividing network

## OUTPUT POWER RATINGS

In practical circuits, a number of different ratings may be used to define the output power from an audio amplifier; they are:

1. Speech and music: the equivalent sine-wave output that will be obtained when peaks occur in low-level passages of speech or music. (Since this energy is taken from the reservoir capacitor, the impedance of the supply does not influence this figure.)
2. Sustained music: the equivalent sine-wave output that will be obtained during sustained high-level passages of music. (This may be lower than the first rating because the supply voltage may fall due to regulation.)
3. Sine-wave: output power attained when the amplifier is sine-wave driven.

These ratings may be quoted:

- (a) at a specified distortion; the output power obtained at the specified level of distortion, often 10%;
- (b) at clipping; the output power at which clipping commences, that is when the working point of the transistors reaches the knee of the output characteristic resulting in a distortion of the output waveform.

The first two ratings constitute a useful measure of the output power capability of the amplifier. The third indicates the power to be obtained when the amplifier is tested with a sine-wave drive and is a lower figure than the first two.

In the I.H.F.M. (Institute of High Fidelity Manufacturers) system, the following two ratings are used:

1. Continuous power: the power an amplifier is capable of delivering for at least 30 seconds with sine-wave drive.
2. Music power: the power obtainable after the application of a signal, measured during a time interval so short that the supply voltages in the amplifier have not changed from their zero-signal values.

### **HEATSINKS**

In determining the size of heatsink required for output, and sometimes driver, transistors in audio amplifiers three factors are taken into consideration:

1. the maximum permissible junction temperature of the device;
2. the thermal conductivity of the semiconductor material and encapsulation of the device, and of the heatsink material;
3. maximum ambient temperature.

The circuits given in this book are designed for operation in ambient temperatures up to 45°C and the minimum size of heatsink, to be mounted vertically in free air, has been specified for each circuit. It should be remembered that if a different heatsink material is used the size of heatsink must be adjusted accordingly.

## CHAPTER 4

# RADIOGRAMS, RECORD PLAYERS AND PORTABLE RADIOS

The chapter is divided into two sections comprising:

1. A.F. amplifiers with output powers of 1W, 3W and 10W; a pre-amplifier for use with the 3W and 10W amplifiers; a 3W record-player amplifier.
2. R.F. and i.f. stages for an a.m. receiver and an a.m./f.m. receiver, both using a 9V supply.

Component lists for the circuits are given at the end of the chapter.

Circuits for high-quality stereo amplifiers are given in Chapter 7.

## A.F. STAGES

### 1W AUDIO AMPLIFIER

The circuit diagram for a 1W transformerless audio amplifier is shown in Fig. 29. The circuit includes a complementary output pair comprising one AC127 and one AC128 transistor, an AC128 driver transistor and an AC127 pre-amplifier. The use of high-gain output transistors allows a simple amplifier, with capacitively-coupled load, to be designed with a relatively low quiescent current. The n-p-n pre-amplifier transistor contributes to very good d.c. stability.

#### Circuit Description

The features of this design are the economy effected in the number of components required, and the extremely good stability of the d.c. potential  $V_M$ . The latter implies less variation of output with temperature changes compared with other forms of output stage using a capacitively-coupled load.

The load is capacitively-coupled to the emitters of  $TR_3$  and  $TR_4$ , the bases being driven directly from the collector of  $TR_2$ . The collector load  $R_7$  of  $TR_2$  is returned to the live end of the loudspeaker, so that the output transistors operate in common-emitter configuration, giving maximum amplification.

A small quiescent bias voltage is required for transistors operating in class B push-pull. This is developed by the collector current of  $TR_2$  flowing through  $R_9$ . Thermistor  $R_8$  is used to compensate for the temperature dependence of the quiescent current.

The transistor  $TR_1$  serves a dual purpose. It acts as a pre-amplifier for a.c. signals and also as a d.c. difference-amplifier comparing the voltage  $V_1$  derived from the potential divider  $R_1, R_2, R_3$ , with the voltage  $V_M$ . The high loop gain of the circuit keeps the small difference between  $V_M$  and  $V_1$  constant, so that  $V_M$  is defined with respect to  $V_1$ , irrespective of spreads in the characteristics of the transistors  $TR_1$  and  $TR_2$  and the tolerance variations in the values of  $R_5, R_6, R_7, R_8$  and  $R_{10}$ .

Negative feedback is taken via the resistor  $R_5$  from the output stage to the emitter of  $TR_1$ . Decoupling is provided by the large-valued capacitor  $C_2$  to remove a.c. feedback between these points, and a small known amount of a.c. feedback is re-introduced by means of  $R_4$  to reduce gain spreads and distortion.

## Performance

Output power at 10% distortion	1.2W r.m.s.
Output power at 4% distortion	0.8W r.m.s.
Sensitivity (source impedance $R_S = 2k\Omega$ ):	
output 50mW, 6dB feedback	2.2mV
output 1.2W, 6dB feedback	10mV
Frequency response (-3dB points)	100Hz to 20kHz
Driver current	7.7mA
Peak collector current	470mA
Total quiescent current	13mA

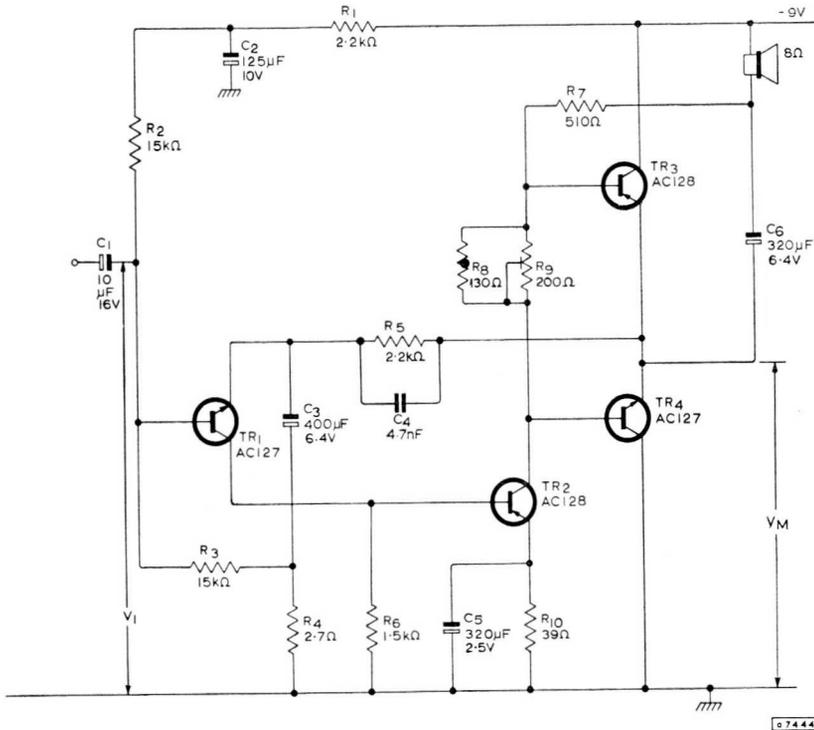


Fig. 29—1W audio amplifier circuit

### Tone Control Circuit

As feedback is applied over three stages in the amplifier of Fig. 29, negative-feedback tone controls can cause instability and passive controls at the input should be used. Fig. 30 shows a simple arrangement for obtaining variable bass and treble cut, without significant loss of gain at mid-frequencies.

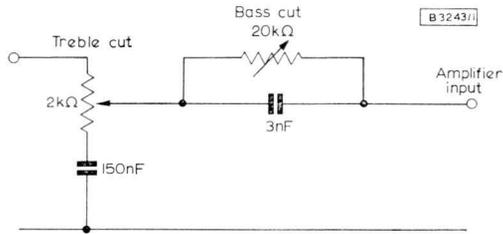


Fig. 30—Tone control circuit

### 3W AUDIO AMPLIFIER

The circuit for a directly-coupled 3W audio amplifier is shown in Fig. 31. The complementary matched output pair comprises one AC176 and one AC128 transistor, the driver is an AC128 and the pre-amplifier is a BC148 or BC108 transistor.

#### Circuit Description

A conventional four-transistor configuration delivers 3W into a 12 $\Omega$  load. The use of a fixed resistor R<sub>7</sub> for bias is acceptable because of the relatively high values of emitter resistors and the large amount of feedback. It is recommended that the resistors which determine the working point—that is resistors R<sub>1</sub>, R<sub>2</sub>, R<sub>3</sub>, R<sub>7</sub>, R<sub>8</sub>—should be 5% tolerance components.

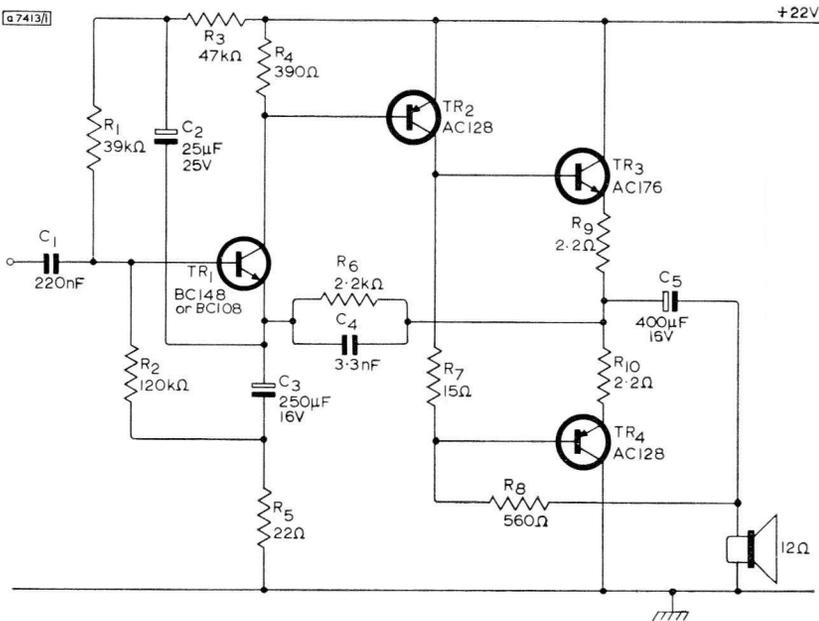


Fig. 31—3W audio amplifier circuit

## Power Supply

A suitable power supply is shown in Fig. 32; the requirements are:

Quiescent consumption	25mA
Full power consumption	200mA
Effective output resistance	$\geq 20\Omega$

## Performance

Output power	3W r.m.s.
Sensitivity for 3W output	70mV
Frequency response ( $-3\text{dB}$ points)	40Hz to 20kHz
Input resistance	80k $\Omega$
Feedback	20dB
Distortion at 3W output (see Fig. 33)	1.7%

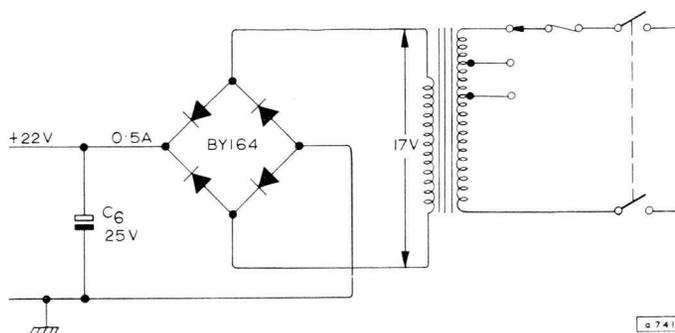


Fig. 32—Power supply circuit for 3W amplifier

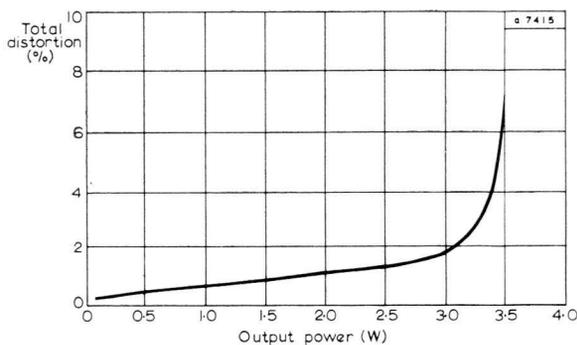


Fig. 33—Variation of total harmonic distortion with output power

## 10W AUDIO AMPLIFIER

The circuit of a 10W amplifier is shown in Fig. 34. In this circuit, a complementary matched pair push-pull output stage is used, and a Zobel network is incorporated.

### Circuit Description

The emitter of transistor  $TR_1$  is connected to the output stage via  $R_5$  to provide a path for negative feedback. The quiescent current of  $TR_3$  and  $TR_4$  is set to approximately 15mA by means of  $R_9$ . The thermistor  $R_8$  compensates for temperature changes and maintains a constant quiescent current. The amplifier can deliver an output of 10W into a  $4\Omega$  loudspeaker with a distortion of less than 3% (see Fig. 36).

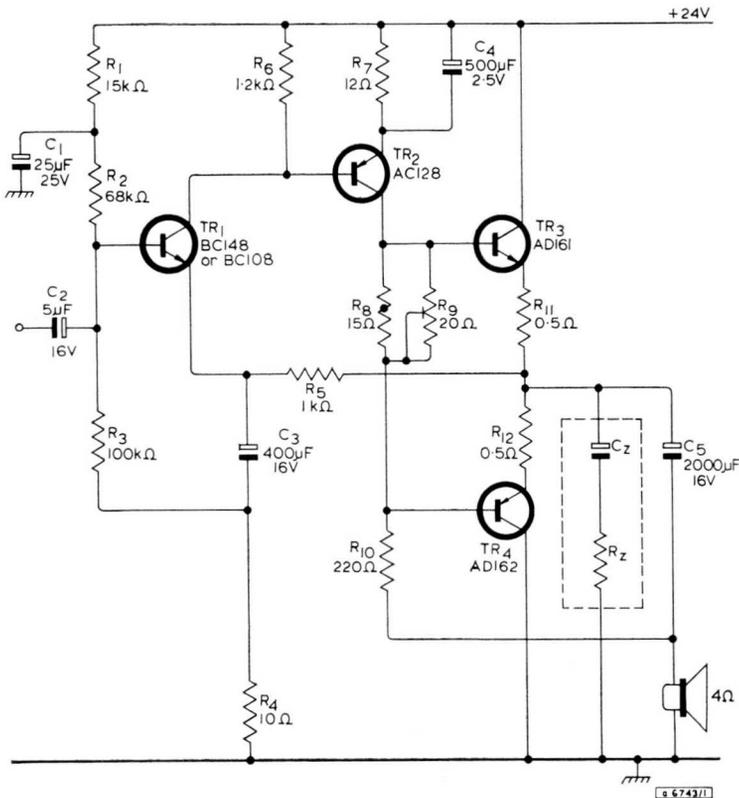


Fig. 34—10W audio amplifier circuit incorporating a Zobel network

### Zobel Network

The purpose and operation of the Zobel network is explained in Chapter 3. From the formulae given on page 27, and for a  $4\Omega$  loudspeaker with an inductance of  $200\mu\text{H}$

$$R_Z = 4\Omega,$$
$$C_Z = \frac{200 \times 10^{-6}}{16} = 12.5\mu\text{F}.$$

(A 25V component is required.)

### Power Supply

The nominal line voltage required by the amplifier is  $+24\text{V}$  and the absolute maximum voltage is  $+27\text{V}$ . The maximum value of direct current per channel is  $0.8\text{A}$ .

The circuit of a simple power supply suitable for use with a stereo system is shown in Fig. 35. The mains transformer has a secondary output of  $18\text{V}$  which is rectified by a diode bridge and smoothed by capacitor  $C_6$ .

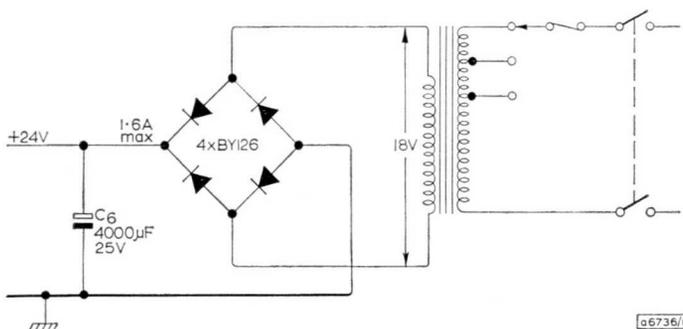


Fig. 35—Power supply circuit for 10W amplifier

### Performance

Output power	10W r.m.s.
Sensitivity (voltage at base of $\text{TR}_1$ for rated output)	80mV
Frequency response ( $-3\text{dB}$ points)	40Hz to 20kHz
Input impedance	$30\text{k}\Omega$
Negative feedback	15dB
Distortion at 10W output (see Fig. 36)	2.9%

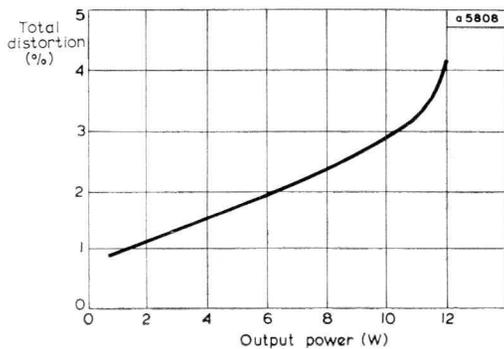


Fig. 36—Variation of total harmonic distortion with output power

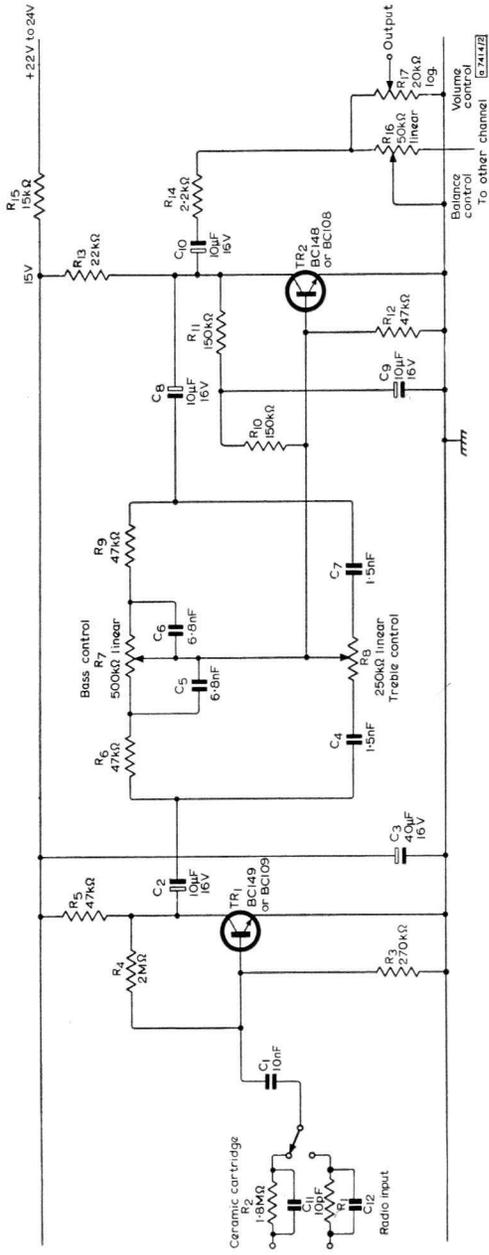


Fig. 37—Pre-amplifier circuit for use with 3W and 10W amplifiers

## PRE-AMPLIFIER FOR USE WITH THE 3W AND 10W AMPLIFIERS

The circuit for a two-stage pre-amplifier which may be used with the 3W and 10W amplifiers already described is shown in Fig. 37. The first stage uses a low-noise BC149 or BC109 transistor and the second stage a BC148 or BC108 transistor.

### Circuit Description

The input stage provides matching for a ceramic cartridge and for radio, the resistor  $R_1$  being chosen to give the required sensitivity in the latter case. A capacitor  $C_{12}$  is connected in parallel with  $R_1$ , the value of capacitance being chosen to give, with  $R_1$ , a time-constant of  $18\mu s$ . The second stage provides comprehensive tone control, with 10dB boost and cut at 100Hz and 10kHz. This stage is followed by a simple balance control for stereo use and a volume control.

### Performance

Sensitivity:

ceramic input, for 80mV output	180mV
radio input, with $R_1 = 470k\Omega$	45mV
Signal handling, output at clipping	1.5V

### 3W RECORD-PLAYER AMPLIFIER

The amplifier shown in Fig. 38 is suitable for use with cartridges giving an output of 300mV at 1cm/s, and may be adapted to include comprehensive tone control (see Fig. 41). The circuit uses a complementary output pair of one AC176 and one AC128 transistor, a BC107 driver transistor and a BC108 transistor.

#### Circuit Description

A crystal pick-up requires a high load, 1 to 2M $\Omega$ , if the bass response is to be adequate. A simple way to provide this load, and at the same time minimise gain spreads, is to apply feedback in series with the input. This technique is used in this amplifier.

Transistor TR<sub>1</sub> is an emitter follower supplying the driver transistor TR<sub>2</sub>. Because of the large amount of feedback used in the circuit, the output transistors, TR<sub>3</sub> and TR<sub>4</sub>, can have simple resistive bias. The output voltage is divided by resistors R<sub>11</sub> and R<sub>12</sub> and fed back to the input. The network C<sub>4</sub> and R<sub>10</sub> forms a simple treble cut control.

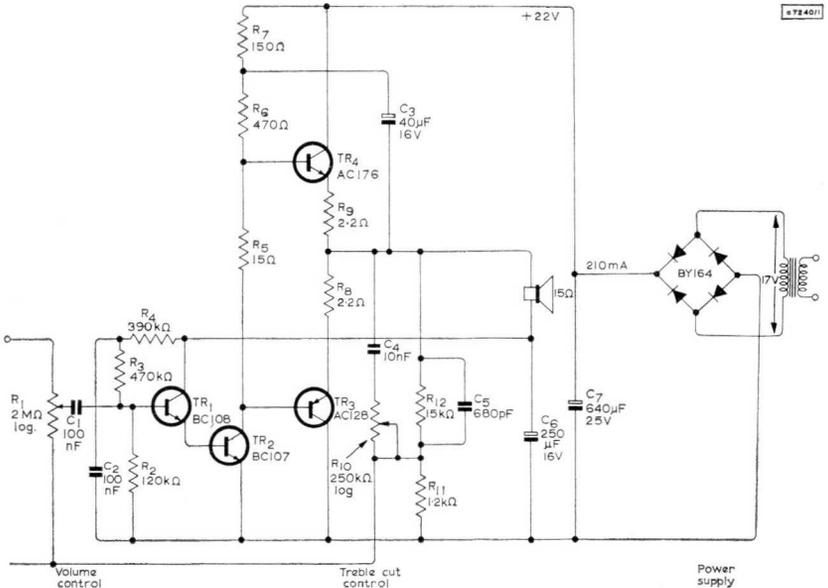


Fig. 38—3W record player amplifier circuit

The loudspeaker and capacitor  $C_6$  are interchanged with respect to their conventional positions to provide a low-voltage supply for the collector of transistor  $TR_1$ , and also a point relatively free from a.c. signals from which d.c. feedback can be taken. The output mid-point voltage is compared with the base voltage of transistor  $TR_1$  by the potential divider comprising resistors  $R_2$ ,  $R_3$  and  $R_4$ . Although the voltage is taken from a nominally d.c. point, decoupling is still required to remove low frequencies.

### Performance

Output power	3W r.m.s.
Sensitivity for full output	600mV
Input resistance:	
with volume control at maximum	660k $\Omega$
with volume control at minimum	2M $\Omega$
Feedback, depending on position of volume control, up to	25dB
Distortion at 2W output:	
with volume control at maximum	0.4%
with volume control at -10dB	2%
Quiescent current	20mA
Total current at 3W output	210mA

Fig. 39 shows the variation in bass response with volume control setting, due to the variation in input resistance. It should be noted that the circuit given in Fig. 39 representing the pick-up was used to obtain these curves.

Fig. 40 shows the variation of distortion with output power. With the volume control at maximum setting the feedback is high and the distortion low. However, at intermediate settings of the volume control the feedback is reduced, because of the increase in source impedance, and the distortion is higher.

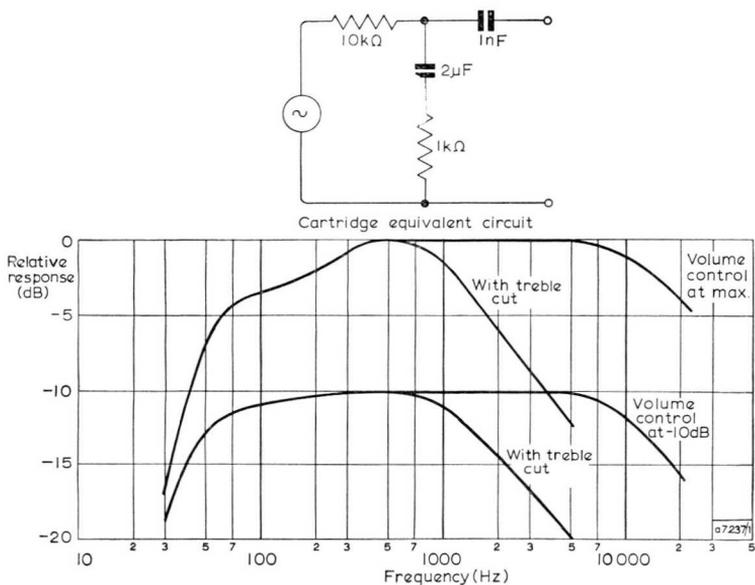


Fig. 39—Frequency response of amplifier

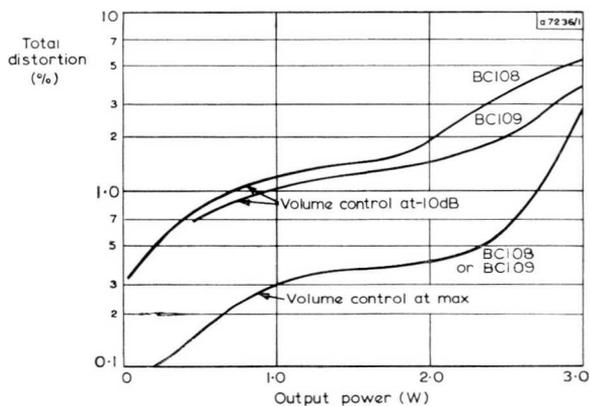


Fig. 40—Variation of total harmonic distortion with output power for basic amplifier and modified circuits

### Circuit adapted to include Comprehensive Tone Control

The feedback circuit may be modified to give bass and treble cut and boost controls, as shown in Fig. 41.

The input transistor  $TR_1$  is a BC109, since this device gives a useful improvement in bass response and also in distortion (see Fig. 40). The tone control characteristics with volume control at maximum and at  $-10\text{dB}$  are shown in Figs. 42 and 43. The value of capacitor  $C_1$  is increased to ensure low-frequency stability with bass boost applied. Capacitor  $C_9$  is included to block d.c. from the bass control, and so prevent noisy operation.

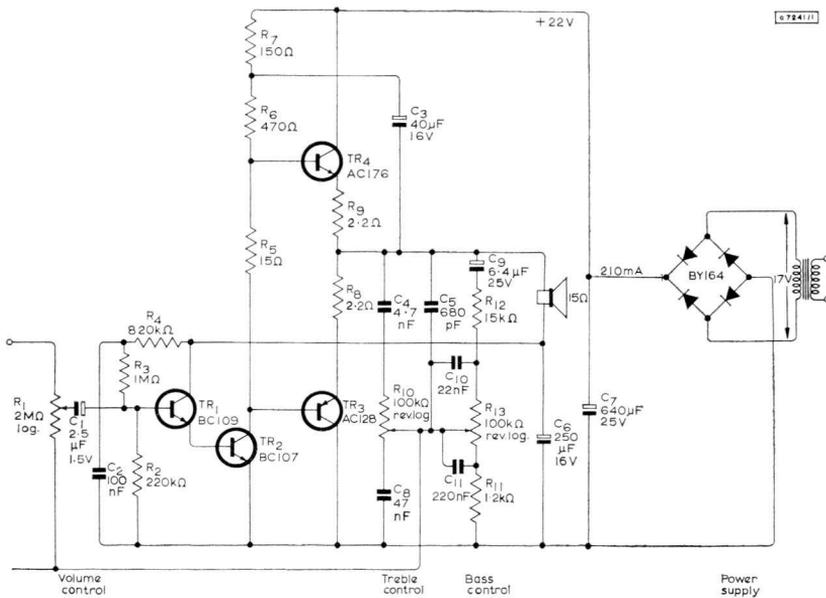


Fig. 41—Amplifier circuit modified to include tone control

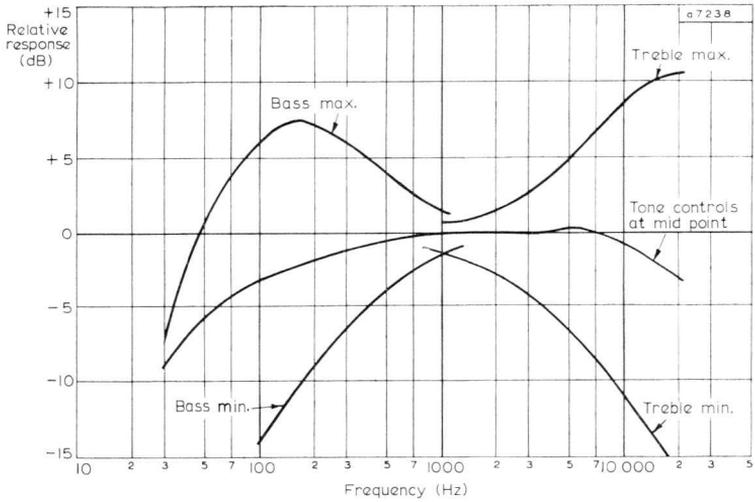


Fig. 42—Tone control characteristics with volume control at maximum

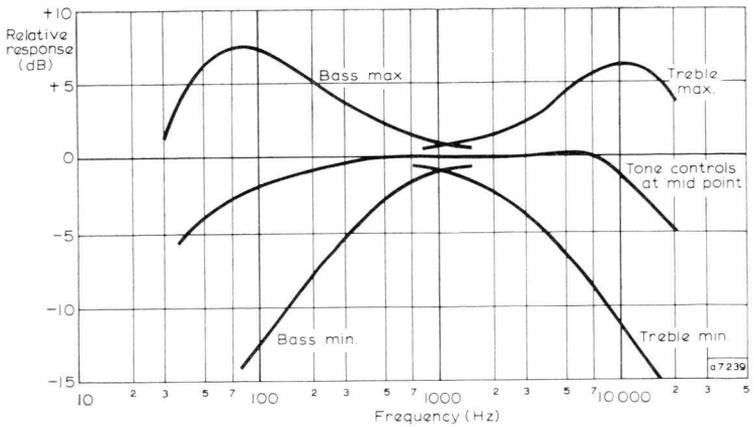


Fig. 43—Tone control characteristics with volume control at -10dB

## R.F. AND I.F. STAGES

Attention is drawn to the difficulties associated with the construction and alignment of r.f. and i.f. stages. As stated earlier, access to specialised equipment is essential to those wishing to build these circuits.

### A.M. RECEIVER

The r.f. and i.f. stages of a nine-volt medium-wave receiver are shown in Fig. 44. The circuit uses Lockfit transistors, types BF194 and BF195. Note: The BF194 and BF195 are supplied to receiver manufacturers in sets of three devices. The devices in these sets carry the letters B, C or D added to the normal type number. For replacement or home-construction purposes, these letters should be ignored and the required devices ordered simply by their type numbers, BF194 and BF195.

### Circuit Description

#### *Self-oscillating Mixer Stage*

The self-oscillating mixer is a conventional circuit, and the BF194 transistor is operated with a collector-emitter voltage of 4.8V, and an emitter current of 1mA. Voltage biasing is used to stabilise the operating point against  $h_{FE}$  and  $V_{BE}$  spreads; the emitter RC circuit is also necessary to stabilise the oscillator voltage.

The aerial source impedance is  $400\Omega$ , and the i.f. load on the mixer is  $9k\Omega$ . The working Q-factor of the first i.f. transformer is 80.

#### *First I.F. Stage*

The first i.f. transistor is a BF195, and is current-biased from a tap on the detector-diode forward-bias chain. It operates at a collector-emitter voltage of 7.5V, and an emitter current of 1mA.

To ensure good large-signal handling properties, a very large step-down ratio is used between the mixer load and the first i.f. stage. (The signal-handling ability is limited by the amplitude of the signal which can be accommodated at the base of the gain-controlled stage.) Because of the large step-down ratio, the source impedance of the first i.f. stage is very low ( $21.5\Omega$ ). Since this stage drives a load of  $50k\Omega$ , it has a very high stability factor (24). However, the gain is sufficiently high, and any increase in load impedance would result in gain spreads caused by variations in output conductance.

#### *Second I.F. Stage*

The second i.f. transistor is a BF195, and is current-biased. It operates at a collector-emitter voltage of 7.5V, and an emitter current of 1mA.

The load impedance of the second i.f. stage is  $7.5k\Omega$ , and this value ensures maximum power for the a.g.c. line. The source impedance is  $530\Omega$ , and therefore the stability factor of the second i.f. stage is 6.5.

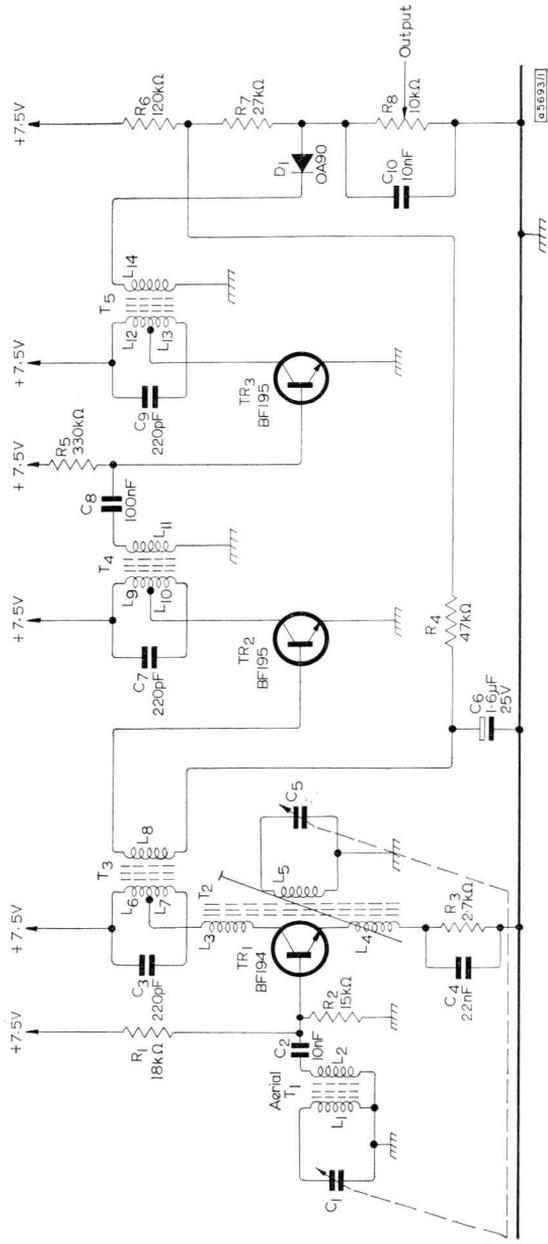


Fig. 44—R.F. and i.f. stages of an a.m. receiver  
 (Line-up using sets of transistors: TR<sub>1</sub>—BF194B, TR<sub>2</sub>—BF195C, TR<sub>3</sub>—BF195D)

*Detector*

The OA90 germanium detector diode is forward-biased by  $15\mu\text{A}$  to improve the small-signal efficiency, and to ensure constant loading on the last i.f. transformer.

**Performance**

A.G.C. range for 6dB change in output (see Fig. 45)	45dB
I.F. bandwidth ( $-6\text{dB}$ points)	$\pm 3.8\text{kHz}$
Attenuation at 9kHz off-tune	28dB
Gain reduction when the supply voltage is reduced to half its nominal value	15dB
Gain spreads (95% limits) resulting from spreads in $h_{FE}$ , $V_{BE}$ , and 10% resistor tolerances (but excluding coil spreads)	$\pm 4\text{dB}$

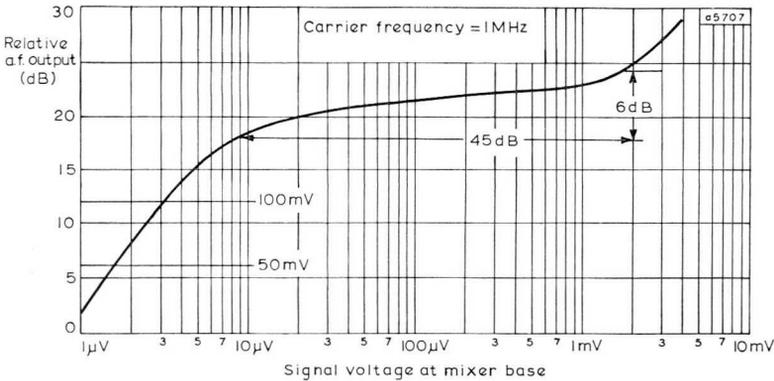


Fig. 45—Automatic gain control characteristic

## A.M./F.M. RECEIVER

The r.f. and i.f. stages of an a.m./f.m. receiver operating from a 9V supply are shown in Fig. 47. The design uses three BF195 and two BF194 transistors.

### Circuit Description

#### *F.M. Tuner*

The f.m. tuner is conventional in design, using a BF195 operated at 1mA as an r.f. amplifier. The self-oscillating mixer uses a BF195 operated at 2mA, the best compromise to obtain minimum oscillator drift with any change in supply voltage (and also good operation at a reduced supply voltage).

#### *A.M. Mixer and A.M./F.M. I.F. Amplifier*

The a.m. self-oscillating mixer, TR<sub>3</sub>, is voltage-biased using a 3.9k $\Omega$  emitter resistor in order to obtain stable operation with 100mV drive into the emitter.

The bias arrangement for the a.g.c. stage TR<sub>4</sub> uses d.c. feedback from the collector in order to achieve good gain stability with source voltage variations. However, current biasing of the controlled stage requires some compromise between gain stability, gain spread and a.g.c. voltage; diode D<sub>1</sub> is forward-biased by only 13 $\mu$ A to achieve good a.g.c. properties. Detector efficiency and distortion are not adversely affected by this low forward-bias current.

The third stage is voltage-biased, to assist in the achievement of a large output voltage swing at the collector.

The f.m. i.f. amplifier is of conventional double-tuned design; the a.m. i.f. amplifier uses single-tuned circuits.

### A.M. Performance

6dB bandwidth	$\pm 3$ kHz
Selectivity at 9kHz off-tune	22dB*
Maximum signal handling	110mV/metre
Input change for 6dB change in output	46dB
Oscillator drive at 1MHz	100mV
Lower limit of supply voltage for oscillator operation	2.7V
A.G.C. and signal/noise characteristic	see Fig. 46

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\*This figure may be increased by increasing the working Q-factor at the expense of the 6dB bandwidth.

## M. Performance

3dB bandwidth	$\pm 160\text{kHz}$
Selectivity at 300kHz off tune	43dB
Image rejection ratio	26dB
Limiting sensitivity (3dB below maximum output)	22 $\mu\text{V}$ (aerial e.m.f.)
Maximum signal handling	20mV (aerial e.m.f.)
Oscillator drive	200mV
Oscillator drift for 2V change in supply voltage	< 25kHz
Oscillator pulling with signal input, at maximum signal	< 4kHz
Limiting and signal-to-noise characteristic	see Fig. 48
Total distortion	see Fig. 49
A.M. rejection	see Fig. 50

## Transistor and Diode Currents

The quiescent collector currents of the transistors are as follows:

TR <sub>1</sub> , TR <sub>3</sub> , TR <sub>4</sub> , TR <sub>5</sub>	1mA
TR <sub>2</sub>	2mA

The diode currents are:

D <sub>1</sub>	13 $\mu\text{A}$
D <sub>2</sub> , D <sub>3</sub>	5.3 $\mu\text{A}$

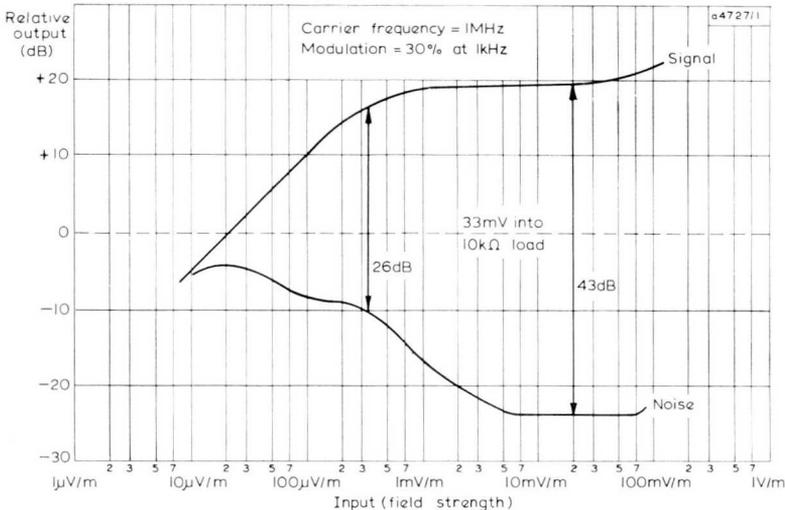
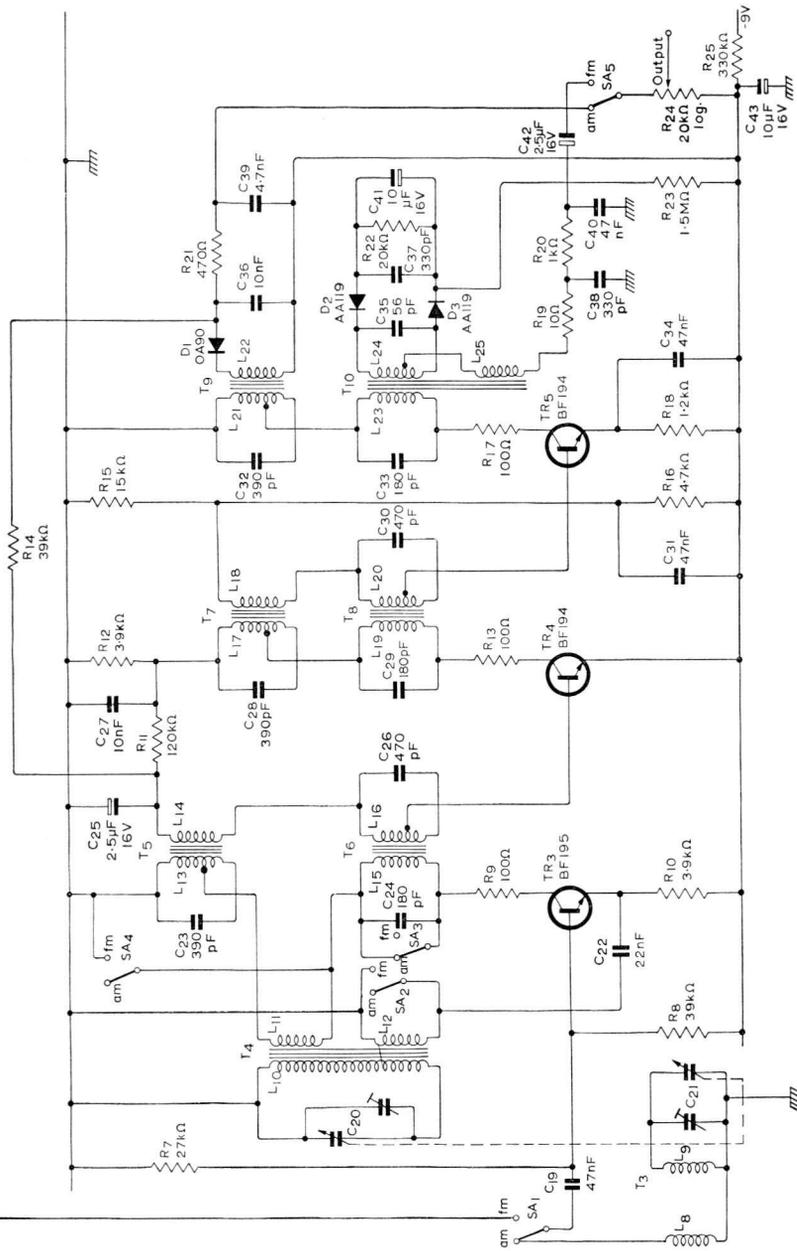


Fig 46—Automatic gain control and signal-to-noise characteristic (a.m.)





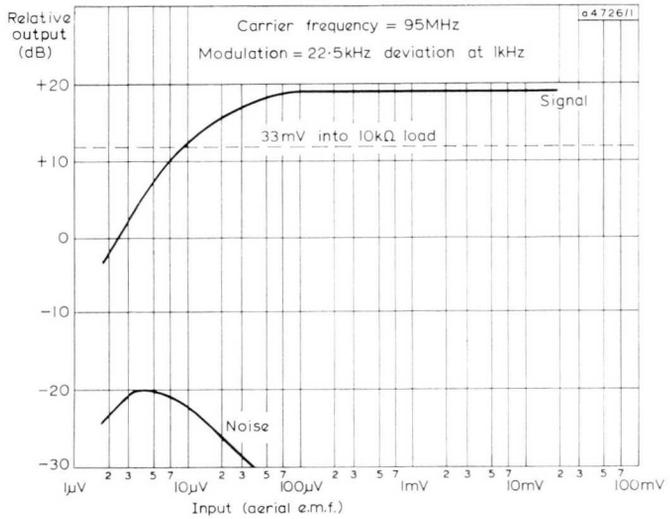


Fig. 48.—Limiting and signal-to-noise characteristic (f.m.)

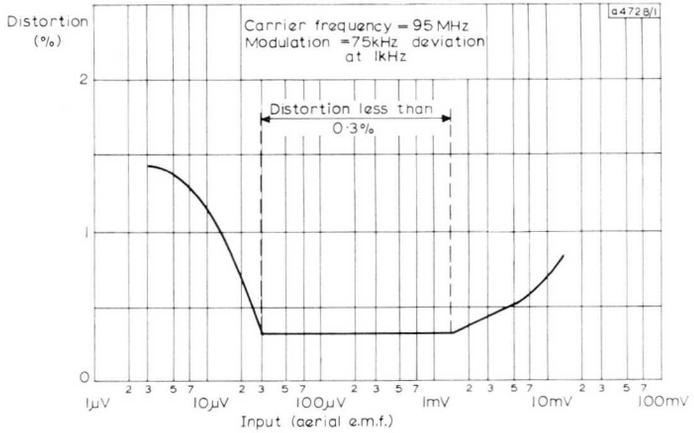


Fig. 49—Variation of audio distortion with input voltage (f.m.)

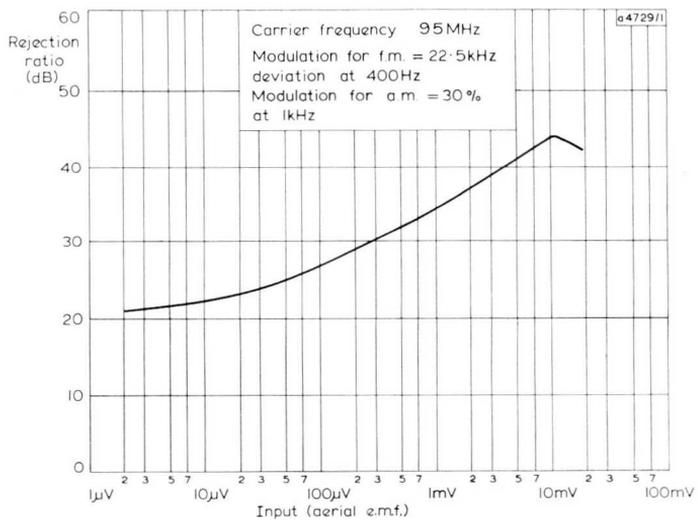


Fig. 50—A.M. rejection ratio

## COMPONENT LISTS FOR CIRCUITS IN CHAPTER 4

### 1W Audio Amplifier (page 35)

#### Transistors

Circuit reference	Mullard type
TR <sub>1</sub>	AC127
TR <sub>2</sub>	AC128
TR <sub>3</sub>	AC128
TR <sub>4</sub>	AC127

#### Resistors

Tolerance:  $\pm 5\%$

Power rating:  $\frac{1}{8}$ W

Circuit reference	Value
R <sub>1</sub>	2.2k $\Omega$
R <sub>2</sub>	15k $\Omega$
R <sub>3</sub>	15k $\Omega$
R <sub>4</sub>	2.7 $\Omega$
R <sub>5</sub>	2.2k $\Omega$
R <sub>6</sub>	1.5k $\Omega$
R <sub>7</sub>	510 $\Omega$
R <sub>8</sub> thermistor type VA1040	130 $\Omega$
R <sub>9</sub> preset potentiometer	200 $\Omega$
R <sub>10</sub>	39 $\Omega$

#### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	10 $\mu$ F	electrolytic 16V	C426AR/E10
C <sub>2</sub>	125 $\mu$ F	electrolytic 10V	C426AR/D125
C <sub>3</sub>	400 $\mu$ F	electrolytic 6.4V	C437AR/D400
C <sub>4</sub>	4.7nF	polyester	C296AC/A4K7
C <sub>5</sub>	320 $\mu$ F	electrolytic 2.5V	C426AR/A320
C <sub>6</sub>	320 $\mu$ F	electrolytic 6.4V	C426AR/C320

#### Heatsinks

For output transistor TR<sub>3</sub> (AC128) a cooling clip is required. For output transistor TR<sub>4</sub> (AC127) a cooling clip mounted on a 1.5mm (16 gauge) bright aluminium heatsink with an area of 12.5cm<sup>2</sup> is required.

### 3W Audio Amplifier (page 37)

#### Transistors and Rectifier

Circuit reference	Mullard type
TR <sub>1</sub>	BC148 or BC108
TR <sub>2</sub>	AC128
TR <sub>3</sub>	AC176
TR <sub>4</sub>	AC128

Full-wave bridge rectifier BY164

#### Resistors

Circuit reference	Value	Tolerance (%)	Power rating (W)
R <sub>1</sub>	39k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>2</sub>	120k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>3</sub>	47k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>4</sub>	390 $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>5</sub>	22 $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>6</sub>	2.2k $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>7</sub>	15 $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>8</sub>	560 $\Omega$	$\pm 5$	$\frac{1}{2}$
R <sub>9</sub>	2.2 $\Omega$	$\pm 10$	$\frac{1}{2}$
R <sub>10</sub>	2.2 $\Omega$	$\pm 10$	$\frac{1}{2}$

#### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	220nF	polyester	C296AA/A220K
C <sub>2</sub>	25 $\mu$ F	electrolytic 25V	C426AR/F25
C <sub>3</sub>	250 $\mu$ F	electrolytic 16V	C437AR/E250
C <sub>4</sub>	3.3nF	polyester	C296AC/A3K3
C <sub>5</sub>	400 $\mu$ F	electrolytic 16V	C437AR/E400
C <sub>6</sub> (mono)	1250 $\mu$ F	electrolytic 25V	C431BR/F1250
C <sub>6</sub> (stereo)	2000 $\mu$ F	electrolytic 25V	C431BR/F2000

#### Mains Transformer

The transformer used in this circuit may be obtained from the following manufacturers under the type numbers given:

Colne Electric Limited, Rickmansworth, Herts	20040
Drake Transformers Limited, Billericay, Essex	1471-136
Gardners Transformers Limited, Christchurch, Hants	GR 97180
Parmeko Limited, Aylestone Park, Leicester	P 3201

#### Heatsinks

The driver and output transistors should be mounted in clips having good thermal contact and fixed to heatsinks of 1.5mm (16 gauge) bright aluminium. The area required for the driver is 12cm<sup>2</sup> and for each output transistor 35cm<sup>2</sup>.

## 10W Audio Amplifier (page 39)

### Transistors and Rectifier

Circuit reference	Mullard type
TR <sub>1</sub>	BC148 or BC108
TR <sub>2</sub>	AC128
TR <sub>3</sub>	AD161
TR <sub>4</sub>	AD162
Rectifier bridge	4 × BY126

### Resistors

Tolerance:  $\pm 5\%$

Power rating:  $\frac{1}{8}$ W except R<sub>10</sub>, which should be a 1W component, R<sub>11</sub> and R<sub>12</sub>, which should be  $\frac{1}{2}$ W components

Circuit reference	Value	Circuit reference	Value
R <sub>1</sub>	15k $\Omega$	R <sub>7</sub>	12 $\Omega$
R <sub>2</sub>	68k $\Omega$	R <sub>8</sub> thermistor	15 $\Omega$
R <sub>3</sub>	100k $\Omega$	type VA1100	
R <sub>4</sub>	10 $\Omega$	R <sub>9</sub> preset potentiometer	20 $\Omega$
R <sub>5</sub>	1k $\Omega$	R <sub>10</sub>	220 $\Omega$
R <sub>6</sub>	1.2k $\Omega$	R <sub>11</sub>	0.5 $\Omega$
		R <sub>12</sub>	0.5 $\Omega$

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	25 $\mu$ F	electrolytic 25V	C426AR/F25
C <sub>2</sub>	5 $\mu$ F	electrolytic 16V	C426AR/H5
C <sub>3</sub>	400 $\mu$ F	electrolytic 16V	C437AR/E400
C <sub>4</sub>	500 $\mu$ F	electrolytic 2.5V	C426AR/A500
C <sub>5</sub>	2000 $\mu$ F	electrolytic 16V	C431BR/E2000
C <sub>6</sub>	4000 $\mu$ F	electrolytic 25V	C431BR/F4000

### Mains Transformer

The transformer used in this circuit may be obtained from the following manufacturers under the type numbers given:

Colne Electric Limited, Rickmansworth, Herts	20041
Drake Transformers Limited, Billericay, Essex	294-139
Gardners Transformers Limited, Christchurch, Hants	GR 97181
Parmeko Limited, Aylestone Park, Leicester	P 3202

### Heatsinks

Transistors TR<sub>2</sub>, TR<sub>3</sub> and TR<sub>4</sub> should be mounted on a common 1.5mm (16 gauge) bright aluminium heatsink with a minimum area of 100cm<sup>2</sup> or blackened aluminium with an area of 60cm<sup>2</sup>. Transistor TR<sub>2</sub> has an isolated can, but TR<sub>3</sub> and TR<sub>4</sub> should both be mounted on mica washers.

## Pre-amplifier (page 42)

### Transistors

Circuit reference	Mullard type
TR <sub>1</sub>	BC149 or BC109
TR <sub>2</sub>	BC148 or BC108

### Resistors

Tolerance:  $\pm 5\%$  except R<sub>2</sub> and R<sub>4</sub>, which may be  $\pm 10\%$  components  
Power rating:  $\frac{1}{8}$ W

Circuit reference	Value
R <sub>1</sub>	see text
R <sub>2</sub>	1.8M $\Omega$
R <sub>3</sub>	270k $\Omega$
R <sub>4</sub>	2M $\Omega$
R <sub>5</sub>	47k $\Omega$
R <sub>6</sub>	47k $\Omega$
R <sub>7</sub> linear potentiometer	500k $\Omega$
R <sub>8</sub> linear potentiometer	250k $\Omega$
R <sub>9</sub>	47k $\Omega$
R <sub>10</sub>	150k $\Omega$
R <sub>11</sub>	150k $\Omega$
R <sub>12</sub>	47k $\Omega$
R <sub>13</sub>	22k $\Omega$
R <sub>14</sub>	2.2k $\Omega$
R <sub>15</sub>	15k $\Omega$
R <sub>16</sub> linear potentiometer	50k $\Omega$
R <sub>17</sub> logarithmic potentiometer	20k $\Omega$

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	10nF	polyester	C296AA/A10K
C <sub>2</sub>	10 $\mu$ F	electrolytic 16V	C426AR/E10
C <sub>3</sub>	40 $\mu$ F	electrolytic 16V	C426AR/E40
C <sub>4</sub>	1.5nF	polyester	C296AC/A1K5
C <sub>5</sub>	6.8nF	polyester	C296AC/A6K8
C <sub>6</sub>	6.8nF	polyester	C296AC/A6K8
C <sub>7</sub>	1.5nF	polyester	C296AC/A1K5
C <sub>8</sub>	10 $\mu$ F	electrolytic 16V	C426AR/E10
C <sub>9</sub>	10 $\mu$ F	electrolytic 16V	C426AR/E10
C <sub>10</sub>	10 $\mu$ F	electrolytic 16V	C426AR/E10
C <sub>11</sub>	10pF	polystyrene	
C <sub>12</sub>	see text		

### 3W Record-player Amplifier

#### Components for Basic Version (page 44)

##### Transistors and Rectifier

Circuit reference	Mullard type
TR <sub>1</sub>	BC108
TR <sub>2</sub>	BC107
TR <sub>3</sub>	AC128
TR <sub>4</sub>	AC176
Full-wave bridge rectifier	BY164

##### Resistors

Circuit reference	Value	Tolerance (%)	Power rating (W)
R <sub>1</sub> logarithmic potentiometer	2M $\Omega$		
R <sub>2</sub>	120k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>3</sub>	470k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>4</sub>	390k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>5</sub>	15 $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>6</sub>	470 $\Omega$	$\pm 5$	$\frac{1}{2}$
R <sub>7</sub>	150 $\Omega$	$\pm 5$	$\frac{1}{2}$
R <sub>8</sub>	2.2 $\Omega$	$\pm 10$	$\frac{1}{4}$
R <sub>9</sub>	2.2 $\Omega$	$\pm 10$	$\frac{1}{4}$
R <sub>10</sub> logarithmic potentiometer	250k $\Omega$		
R <sub>11</sub>	1.2k $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>12</sub>	15k $\Omega$	$\pm 10$	$\frac{1}{8}$

##### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	100nF	polyester	C296AA/A100K
C <sub>2</sub>	100nF	polyester	C296AA/A100K
C <sub>3</sub>	40 $\mu$ F	electrolytic 16V	C426AR/E40
C <sub>4</sub>	10nF	polyester	C296AA/A10K
C <sub>5</sub>	680pF	polystyrene	C295AC/680E
C <sub>6</sub>	250 $\mu$ F	electrolytic 16V	C437AR/E250
C <sub>7</sub>	640 $\mu$ F	electrolytic 25V	C437AR/F640

##### Mains Transformer

The transformer used in this circuit may be obtained from the following manufacturers under the type numbers given:

Colne Electric Limited, Rickmansworth, Herts	20042
Drake Transformers Limited, Billericay, Essex	351-245
Gardners Transformers Limited, Christchurch, Hants	GR 97182
Parmeko Limited, Aylestone Park, Leicester	P 3203

## Components for Version including Comprehensive Tone Control (page 47)

### Transistors and Rectifier

Circuit reference	Mullard type
TR <sub>1</sub>	BC109
TR <sub>2</sub>	BC107
TR <sub>3</sub>	AC128
TR <sub>4</sub>	AC176
Full-wave bridge rectifier	BY164

### Resistors

Circuit reference	Value	Tolerance (%)	Power rating (W)
R <sub>1</sub> logarithmic potentiometer	2M $\Omega$		
R <sub>2</sub>	220k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>3</sub>	1M $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>4</sub>	820k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>5</sub>	15 $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>6</sub>	470 $\Omega$	$\pm 5$	$\frac{1}{2}$
R <sub>7</sub>	150 $\Omega$	$\pm 5$	$\frac{1}{2}$
R <sub>8</sub>	2.2 $\Omega$	$\pm 10$	$\frac{1}{4}$
R <sub>9</sub>	2.2 $\Omega$	$\pm 10$	$\frac{1}{4}$
R <sub>10</sub> reverse logarithmic potentiometer	100k $\Omega$		
R <sub>11</sub>	1.2k $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>12</sub>	15k $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>13</sub> reverse logarithmic potentiometer	100k $\Omega$		

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	2.5 $\mu$ F	electrolytic 1.5V	
C <sub>2</sub>	100nF	polyester	C296AA/A100K
C <sub>3</sub>	40 $\mu$ F	electrolytic 16V	C426AR/E40
C <sub>4</sub>	4.7nF	polyester	C296AC/A4K7
C <sub>5</sub>	680pF	polystyrene	C295AC/680E
C <sub>6</sub>	250 $\mu$ F	electrolytic 16V	C437AR/E250
C <sub>7</sub>	640 $\mu$ F	electrolytic 25V	C437AR/F640
C <sub>8</sub>	47nF	polyester	C296AA/A47K
C <sub>9</sub>	6.4 $\mu$ F	electrolytic 25V	C426AR/F6.4
C <sub>10</sub>	22nF	polyester	C296AA/A22K
C <sub>11</sub>	220nF	polyester	C296AA/A220K

### Mains Transformer

For suppliers of the transformer, see page 62.

### Heatsinks

Each output transistor should be mounted on a 1.5mm (16 gauge) bright aluminium heatsink with an area of 30cm<sup>2</sup>. In the circuit shown the driver transistor does not require a heatsink. However, an increase in output power (3W at clipping) may be obtained, by fitting a heat clip on the driver transistor and reducing the value of R<sub>6</sub> to 330Ω to give a higher drive current, with a 12Ω load. (Alternatively, a larger driver transistor, the BFY51, may be used with the same reduction in the value of R<sub>6</sub> and a 12Ω load.)

### A.M. Receiver (page 50)

#### Transistors and Diode

See note on page 49

Circuit reference	Mullard type
TR <sub>1</sub>	BF194
TR <sub>2</sub>	BF195
TR <sub>3</sub>	BF195
D <sub>1</sub>	OA90

#### Resistors

Tolerance:  $\pm 5\%$   
Power rating:  $\frac{1}{8}$ W

Circuit reference	Value	Circuit reference	Value
R <sub>1</sub>	18kΩ	R <sub>5</sub>	330kΩ
R <sub>2</sub>	15kΩ	R <sub>6</sub>	120kΩ
R <sub>3</sub>	2.7kΩ	R <sub>7</sub>	27kΩ
R <sub>4</sub>	47kΩ	R <sub>8</sub>	logarithmic carbon potentiometer

## Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub> } C <sub>5</sub> }		foil dielectric variable capacitor	AC0039
C <sub>2</sub>	10nF	polyester	C296AA/A10K
C <sub>3</sub>	220pF	ceramic plate	C333CH/C220E
C <sub>4</sub>	22nF	polyester	C296AA/A22K
C <sub>6</sub>	1·6μF	electrolytic 25V	
C <sub>7</sub>	220pF	ceramic plate	C333CH/C220E
C <sub>8</sub>	100nF	polyester	C296AA/A100K
C <sub>9</sub>	220pF	ceramic plate	C333CH/C220E
C <sub>10</sub>	10nF	polyester	C296AA/A10K

## Transformers

### Aerial transformer—T<sub>1</sub>

L <sub>1</sub>	80 turns of 12×46 s.w.g. stranded wire; close-wound to fit Mullard 9·5mm diameter ferrite rod, type FX1247
L <sub>2</sub>	3½ turns of 12×46 s.w.g. stranded wire; interwound with earth end of L <sub>1</sub>

### Oscillator transformer—T<sub>2</sub>

L <sub>3</sub>	10 turns of 3×46 s.w.g. stranded wire
L <sub>4</sub>	2 turns of 3×46 s.w.g. stranded wire
L <sub>5</sub>	100 turns of 3×46 s.w.g. stranded wire; wave-wound on 4·8mm former

### First i.f. transformer—T<sub>3</sub>

L <sub>6</sub> +L <sub>7</sub>	42+108 turns of 3×46 s.w.g. stranded wire
L <sub>8</sub>	2 turns of 3×46 s.w.g. stranded wire; wave-wound on 4·8mm former; Q <sub>O</sub> ≈ Q <sub>L</sub> = 80 when L <sub>6</sub> +L <sub>7</sub> is shunted with 330kΩ resistor

### Second i.f. transformer—T<sub>4</sub>

L <sub>9</sub> +L <sub>10</sub>	80+70 turns of 3×46 s.w.g. stranded wire
L <sub>11</sub>	9 turns of 3×46 s.w.g. stranded wire; wound on 4·8mm former; Q <sub>O</sub> = 120, Q <sub>L</sub> = 95

### Third i.f. transformer—T<sub>5</sub>

L <sub>12</sub> +L <sub>13</sub>	51+99 turns of 3×46 s.w.g. stranded wire
L <sub>14</sub>	32 turns of 3×46 s.w.g. stranded wire; wound on 4·8mm former; Q <sub>O</sub> = 120, Q <sub>L</sub> = 40

## A.M./F.M. Receiver (pages 54 and 55)

### Transformers and Coils

Except where otherwise stated, all transformers and coils are wound on 4mm formers with ferrite frames and slugs.

#### F.M. aerial transformer— $T_1$

$L_1 + L_2$  2+2 turns of 24 s.w.g. enamelled-copper wire; wound on ferrite twin bead

#### First f.m. i.f. transformer— $T_2$

$L_6 + L_7$  14+14 turns of 36 s.w.g. enamelled-copper wire; wound on a 4.4mm diameter former  
 $L_7$  is critically coupled to  $L_6$  when  $L_7$  is loaded with  $600\Omega$  at the capacitive tap

#### Medium-wave aerial transformer— $T_3$

$L_8$  80 turns of  $12 \times 46$  s.w.g. silk-covered enamelled-copper wire; wound on Mullard ferrite rod, type FX1247 ( $203 \times 9.5\text{mm}$ );  $Q_0 = 200$

$L_9$   $3\frac{1}{2}$  turns of  $12 \times 46$  s.w.g. silk-covered enamelled-copper wire; interwound with earth end of  $L_8$

#### A.M. oscillator transformer— $T_4$

$L_{10}$  (primary)  $119\frac{3}{8}$  turns of  $6 \times 48$  s.w.g. enamelled-copper wire;  $Q_0 = 145$

$L_{11}$  (collector)  $9\frac{1}{2}$  turns of  $6 \times 48$  s.w.g. enamelled-copper wire

$L_{12}$  (emitter)  $1\frac{7}{8}$  turns of  $6 \times 48$  s.w.g. enamelled-copper wire; wound on 'baby' coil former;

#### First a.m. i.f. transformer— $T_5$

$L_{13}$  (primary) 130 turns of  $3 \times 46$  s.w.g. enamelled-copper wire; tapped at 41 turns from the earth end; tap impedance =  $6.5k\Omega$ ;  $Q_0 = 75$ ,  $Q_L = 70$

$L_{14}$  (secondary)  $5\frac{1}{4}$  turns of  $3 \times 46$  s.w.g. enamelled-copper wire

Turns ratio, primary tap: secondary = 7.8:1

#### Second f.m. i.f. transformer— $T_6$

$L_{15}$  (primary) 8 turns of 36 s.w.g. enamelled-copper wire;  $Q_0 = Q_L = 53$

$L_{16}$  (secondary) 6 turns of 36 s.w.g. enamelled-copper wire tapped at  $1\frac{3}{4}$  turns from earth end; unloaded tap impedance =  $118\Omega$ ;  $Q_0 = 53$ ,  $Q_L = 50$

$L_{16}$  is critically coupled when secondary tap is loaded with  $2.2k\Omega$

Turns ratio, primary:secondary tap = 4.5:1

#### Second a.m. i.f. transformer— $T_7$

$L_{17}$  (primary) 110 turns of  $3 \times 46$  s.w.g. enamelled-copper wire tapped at 73 turns from earth end; tap impedance =  $35.6k\Omega$ ;  $Q_0 = 98$ ,  $Q_L = 70$

$L_{18}$  (secondary) 10 turns of  $3 \times 46$  s.w.g. enamelled-copper wire

Turns ratio, primary tap:secondary = 6.9:1

#### Third f.m. i.f. transformer— $T_8$

$L_{19}$  (primary) As  $L_{15}$  ( $T_6$ )

$L_{20}$  (secondary) As  $L_{16}$  ( $T_6$ )

Third a.m. i.f. transformer— $T_9$

$L_{21}$  (primary) 110 turns of  $3 \times 46$  s.w.g. enamelled-copper wire tapped at 48 turns from earth end; tap impedance =  $21.6k\Omega$ ;  $Q_0 = 140$ ,  $Q_L = 50$

$L_{22}$  (secondary) 31 turns of  $3 \times 46$  s.w.g. enamelled-copper wire

Turns ratio, primary tap:secondary =  $1.53:1$

F.M. ratio detector transformer— $T_{10}$

$L_{23}$  (primary) 8 turns of 34 s.w.g. enamelled-copper wire;  $Q_0 = 90$ ,  $Q_L = 58$

$L_{24}$  (secondary)  $2 \times 7$  turns of 36 s.w.g. enamelled-copper wire;  $Q_0 = 75$

$L_{25}$  (tertiary)  $3\frac{1}{2}$  turns of 36 s.w.g. enamelled-copper wire; overwound on primary at earth end. Primary to secondary coupling is 0.7 with secondary loaded with  $10k\Omega$  and tertiary open-circuited.

Coil  $L_3$   $3\frac{1}{2}$  turns of 20 s.w.g. tinned-copper wire; spaced one diameter and wound on a 6mm diameter former

Coil  $L_4$  12 turns of 28 s.w.g. enamelled-copper wire; wound on a 4.4mm former with ferrite core

Coil  $L_5$   $3\frac{1}{2}$  turns of 20 s.w.g. tinned-copper wire; spaced two diameters and wound on a 6mm diameter former; tapped two turns from the earth end

### Transistors and Diodes

Circuit reference	Mullard type	Circuit reference	Mullard type
TR <sub>1</sub>	BF195	D <sub>1</sub>	OA90
TR <sub>2</sub>	BF195	D <sub>2</sub>	AA119
TR <sub>3</sub>	BF195	D <sub>3</sub>	AA119
TR <sub>4</sub>	BF194		
TR <sub>5</sub>	BF194		

### Resistors

Tolerance:  $\pm 5\%$  except  $R_{23}$ , which may be a  $\pm 10\%$  component

Power rating:  $\frac{1}{8}W$

Circuit reference	Value	Circuit reference	Value
R <sub>1</sub>	$1k\Omega$	R <sub>14</sub>	$39k\Omega$
R <sub>2</sub>	$5.6k\Omega$	R <sub>15</sub>	$15k\Omega$
R <sub>3</sub>	$18k\Omega$	R <sub>16</sub>	$4.7k\Omega$
R <sub>4</sub>	$680\Omega$	R <sub>17</sub>	$100\Omega$
R <sub>5</sub>	$5.6k\Omega$	R <sub>18</sub>	$1.2k\Omega$
R <sub>6</sub>	$18k\Omega$	R <sub>19</sub>	$10\Omega$
R <sub>7</sub>	$27k\Omega$	R <sub>20</sub>	$1k\Omega$
R <sub>8</sub>	$39k\Omega$	R <sub>21</sub>	$470\Omega$
R <sub>9</sub>	$100\Omega$	R <sub>22</sub>	$20k\Omega$
R <sub>10</sub>	$3.9k\Omega$	R <sub>23</sub>	$1.5M\Omega$
R <sub>11</sub>	$120k\Omega$	R <sub>24</sub>	logarithmic potentiometer
R <sub>12</sub>	$3.9k\Omega$		
R <sub>13</sub>	$100\Omega$	R <sub>25</sub>	$330k\Omega$

## Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	1nF	polyester	C296AC/A1K
C <sub>2</sub>	12pF	ceramic plate	C333CB/L12E
C <sub>3</sub>	1nF	polyester	C296AC/A1K
C <sub>4</sub>	2 to 12pF	trimmer	
C <sub>5</sub>	2 to 13·6pF	ganged tuning capacitor	
C <sub>13</sub>	2 to 13·6pF		
C <sub>6</sub>	33pF		ceramic plate
C <sub>7</sub>	4·7pF	ceramic plate	C333CB/L4E7
C <sub>8</sub>	270pF	polystyrene	
C <sub>9</sub>	39pF	ceramic plate	C333CC/C39E
C <sub>10</sub>	1nF	polyester	C296AC/A1K
C <sub>11</sub>	4·7pF	ceramic plate	C333CB/L4E7
C <sub>12</sub>	2 to 12pF	trimmer	
C <sub>14</sub>	33pF	ceramic plate	C333CC/C33E
C <sub>15</sub>	68pF	ceramic plate	C333CH/C68E
C <sub>16</sub>	1nF	polyester	C296AC/A1K
C <sub>17</sub>	68pF	ceramic plate	C333CH/C68E
C <sub>18</sub>	1nF	polyester	C296AC/A1K
C <sub>19</sub>	47nF	metallised foil	C280AE/P47K
C <sub>20</sub>	ganged tuning capacitor, Plessey 'W' type		
C <sub>21</sub>			
C <sub>22</sub>	22nF	metallised foil	C280AE/P22K
C <sub>23</sub>	390pF	polystyrene	
C <sub>24</sub>	180pF	ceramic plate	C333CH/C180E
C <sub>25</sub>	2·5μF	electrolytic 16V	C426AR/H2·5
C <sub>26</sub>	470pF	polystyrene	
C <sub>27</sub>	10nF	metallised foil	C280AE/P10K
C <sub>28</sub>	390pF	polystyrene	
C <sub>29</sub>	180pF	ceramic plate	C333CH/C180E
C <sub>30</sub>	470pF	polystyrene	
C <sub>31</sub>	47nF	metallised foil	C280AE/P47K
C <sub>32</sub>	390pF	polystyrene	
C <sub>33</sub>	180pF	ceramic plate	C333CH/C180E
C <sub>34</sub>	47nF	metallised foil	C280AE/P47K
C <sub>35</sub>	56pF	ceramic plate	C333CH/C56E
C <sub>36</sub>	10nF	metallised foil	C280AE/P10K
C <sub>37</sub>	330pF	polystyrene	
C <sub>38</sub>	330pF	polystyrene	
C <sub>39</sub>	4·7nF	polyester	C296AC/A4K7
C <sub>40</sub>	47nF	metallised foil	C280AE/P47K
C <sub>41</sub>	10μF	electrolytic 16V	C426AR/E10
C <sub>42</sub>	2·5μF	electrolytic 16V	C426AR/H2·5
C <sub>43</sub>	10μF	electrolytic 16V	C426AR/E10

## CHAPTER 5

# TAPE RECORDERS

In this chapter, a 4W tape recorder amplifier and a tape pre-amplifier are described, and the modifications necessary for stereo operation are considered. An automatic gain control circuit for use with tape recorders is also included.

The amplifier and pre-amplifier circuits are designed around the Marriott type X/RPS/36 recording head and X/ES/11 erase head; they will not operate with heads of different inductance and bias requirements.

Component lists for the circuits are given at the end of the chapter.

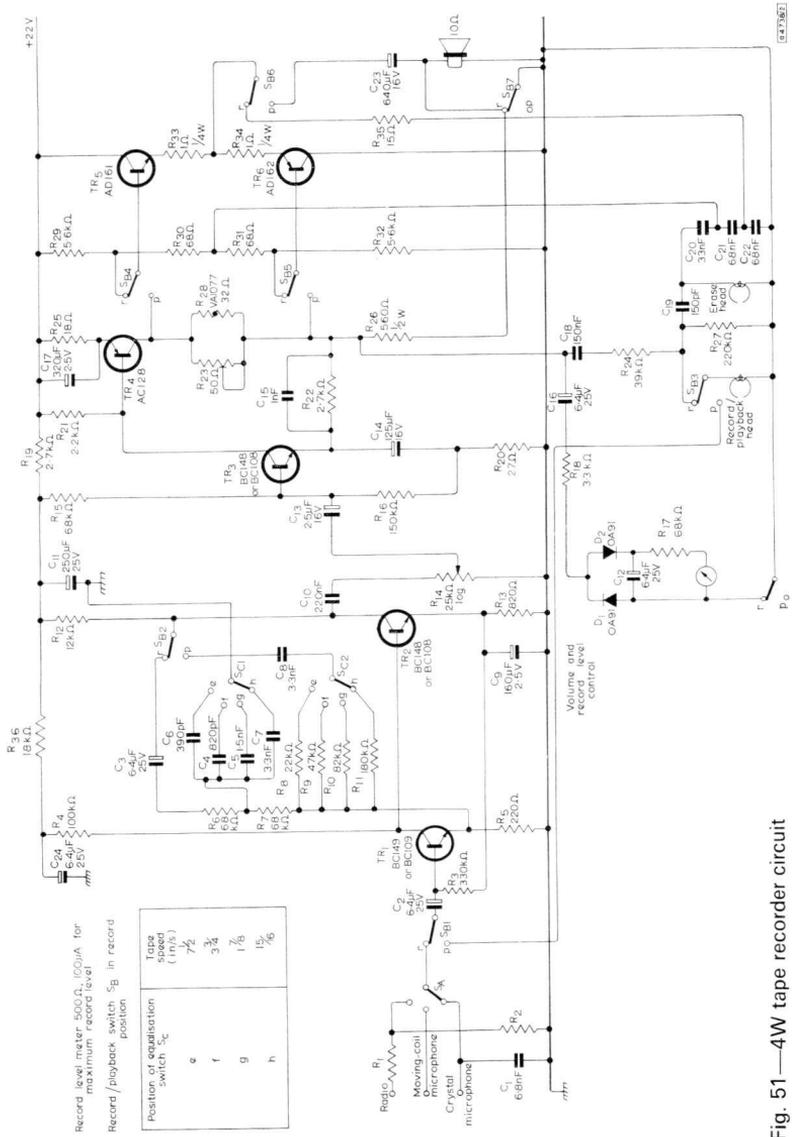


Fig. 51—4W tape recorder circuit

## 4W TAPE RECORDER

The 4W tape recorder shown in Fig. 51 uses silicon transistors in the first three stages to obtain high sensitivity. The output stage uses a complementary matched pair, transistors AD161 (n-p-n) and AD162 (p-n-p), which are also used for the oscillator during recording. Equalisation is provided for tape speeds of  $7\frac{1}{2}$ in/s (19.1cm/s),  $3\frac{3}{4}$ in/s (9.5cm/s),  $1\frac{7}{8}$ in/s (4.8cm/s) and  $\frac{1}{8}$ in/s (2.4cm/s), which conforms to C.C.I.R. standards where appropriate.

### Circuit Description

#### *Playback*

The BC149 or BC109 has been chosen for the input stage because it is particularly suitable for use in audio input stages where low noise is essential. Its collector is directly connected to the base of TR<sub>2</sub>; its emitter is connected via an RC network to the collector of TR<sub>2</sub>. This RC network provides a path for negative feedback by means of which equalisation is effected. The frequency response curves on playback are shown in Fig. 53.

A d.c. feedback path is also provided from the emitter of TR<sub>2</sub> to the base of TR<sub>1</sub>. The d.c. feedback along this path stabilises the working points of TR<sub>1</sub> and TR<sub>2</sub>.

The other transistors in the tape recorder form a conventional amplifier. The complementary pair TR<sub>5</sub> and TR<sub>6</sub>, is driven by TR<sub>4</sub>, which is itself driven by the high-gain BC148 or BC108 transistor. Potentiometer R<sub>23</sub> is adjusted to give a quiescent output-stage current of 5mA.

#### *Record*

Different input circuits are needed to match the different signal sources. For example, the input circuit for a crystal microphone contains a shunt capacitor, C<sub>1</sub>, and that for a radio receiver is a potential divider. A moving coil microphone, however, can be connected directly because the amplifier has an input resistance of 200k $\Omega$ . During recording, TR<sub>5</sub> and TR<sub>6</sub> operate as an oscillator at 50kHz, the erase head being used as an oscillator coil. The capacitive taps, C<sub>20</sub>, C<sub>21</sub> and C<sub>22</sub>, also provide the necessary conditions for sustained oscillation.

The recording level indicator gives a reading proportional to the peak-to-peak voltage at the collector of TR<sub>4</sub>. The full recording level with a sine-wave is 4V r.m.s., which produces a current of 95 $\mu$ A through the meter and 110 $\mu$ A r.m.s. through the recording head.

During recording, the equalisation circuits connected to switch S<sub>C</sub> are not used; feedback is via the path C<sub>3</sub>, R<sub>6</sub> and R<sub>7</sub>, which has been designed

to give treble boost. The frequency response curves on record are shown in Fig. 54.

The recording current is taken from the collector of TR<sub>4</sub>, and the recording head is a Marriott type X/RPS/36\* with the following characteristics:

Quarter-track head:	
Gap	0.0001in
Width	0.043in
Spacing	0.136in
Inductance at 1kHz	70mH
Bias at 50kHz	> 11V
Recording current for 2dB below 2% distortion	110μA
Output at 1kHz using E.M.I. test tape T.B.T.I.	0.44mV
Output at 2kHz for 110μA recording current	1.07mV

### Power Supply

The circuit of a simple power supply suitable for use with the tape recorder is shown in Fig. 52. It contains a mains transformer with a secondary output of 17V. This is rectified by means of a bridge rectifier, type BY164, and smoothed by means of a 640μF capacitor.

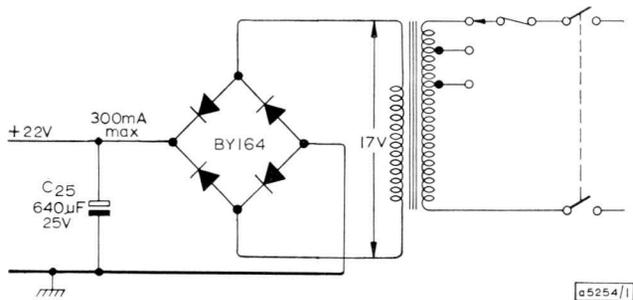


Fig. 52—Power supply circuit for a 4W tape recorder

\*Record/playback heads with a larger inductance are not suitable because they would require a larger bias voltage.

## Performance

### Overall frequency response

tape speed = $7\frac{1}{2}$ in/s	55Hz to 20kHz
tape speed = $3\frac{3}{4}$ in/s	55Hz to 12kHz
tape speed = $1\frac{7}{8}$ in/s	55Hz to 6kHz

### Playback

Output power	4W r.m.s.
Sensitivity at base of TR <sub>1</sub> , at 1kHz and with tape speed of $7\frac{1}{2}$ in/s	400 $\mu$ V
Distortion for 4W output	1.2%
Noise relative to 4W, with volume control set so that a signal produced with 110 $\mu$ A recording current gives 4W output; 3dB bandwidth = 30Hz to 15kHz:	

tape speed = $7\frac{1}{2}$ in/s	-60dB
tape speed = $3\frac{3}{4}$ in/s	-57dB
tape speed = $1\frac{7}{8}$ in/s	-55dB
tape speed = $\frac{15}{16}$ in/s	-50dB

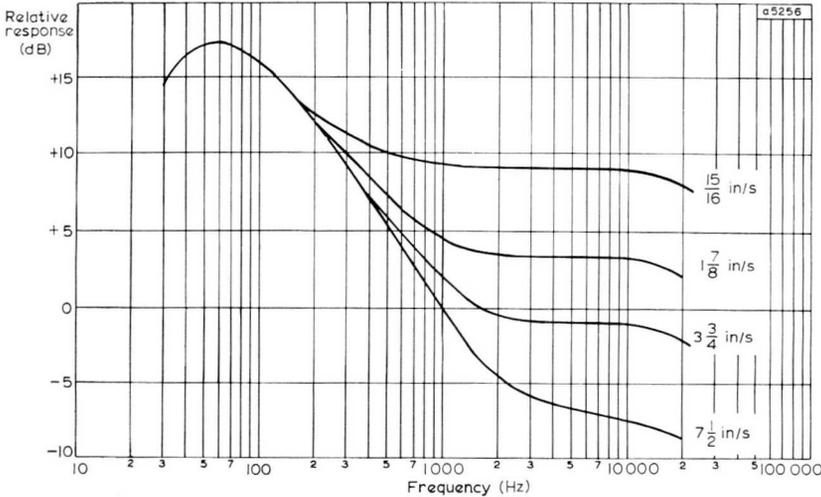


Fig. 53—Playback characteristic

*Record*

Sensitivity at base of TR<sub>1</sub> for 110 $\mu$ A recording current,

with volume control at maximum setting

100 $\mu$ V

Distortion at full record level

1%

Recording current level for 4W output,

with volume control at maximum setting

40 $\mu$ A

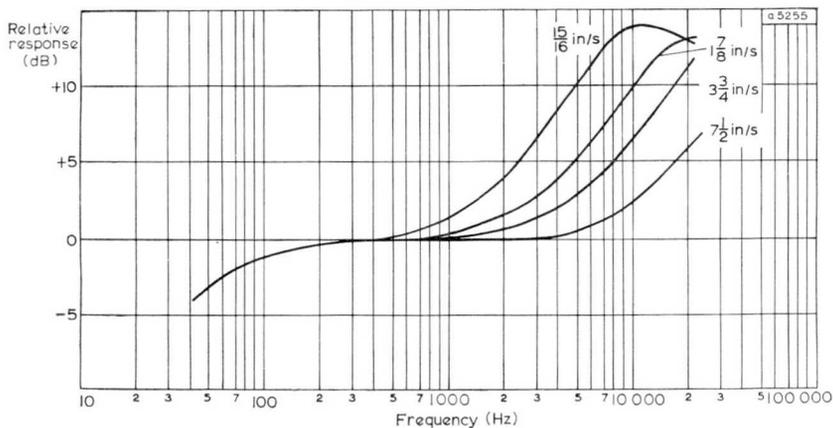


Fig. 54—Record characteristic

## TAPE PRE-AMPLIFIER

### Circuit Description

Fig. 56 shows a pre-amplifier circuit derived from the tape recorder circuit already described. The oscillator stage in this circuit uses a complementary pair comprising one AC176 and one AC128 transistor.

### Performance

The distortion measured at the collector of transistor TR<sub>4</sub> (AC128) in the playback position is shown in Fig. 55. The measurements were made at a speed of 3 $\frac{3}{4}$  in/s, although these characteristics vary little with speed.

At a speed of 7 $\frac{1}{2}$  in/s with the volume control at maximum, the output voltage is 6.55V for an input voltage of 400 $\mu$ V.

The total current drain on playback is 25mA.

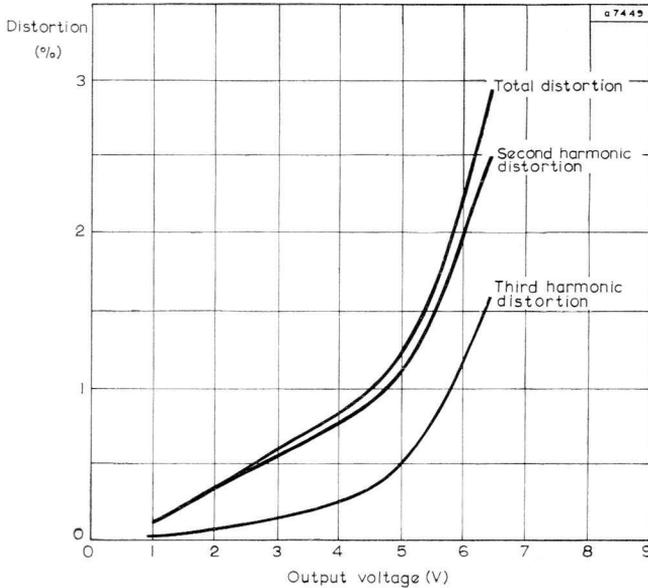


Fig. 55—Variation of harmonic distortion with output voltage for pre-amplifier circuit

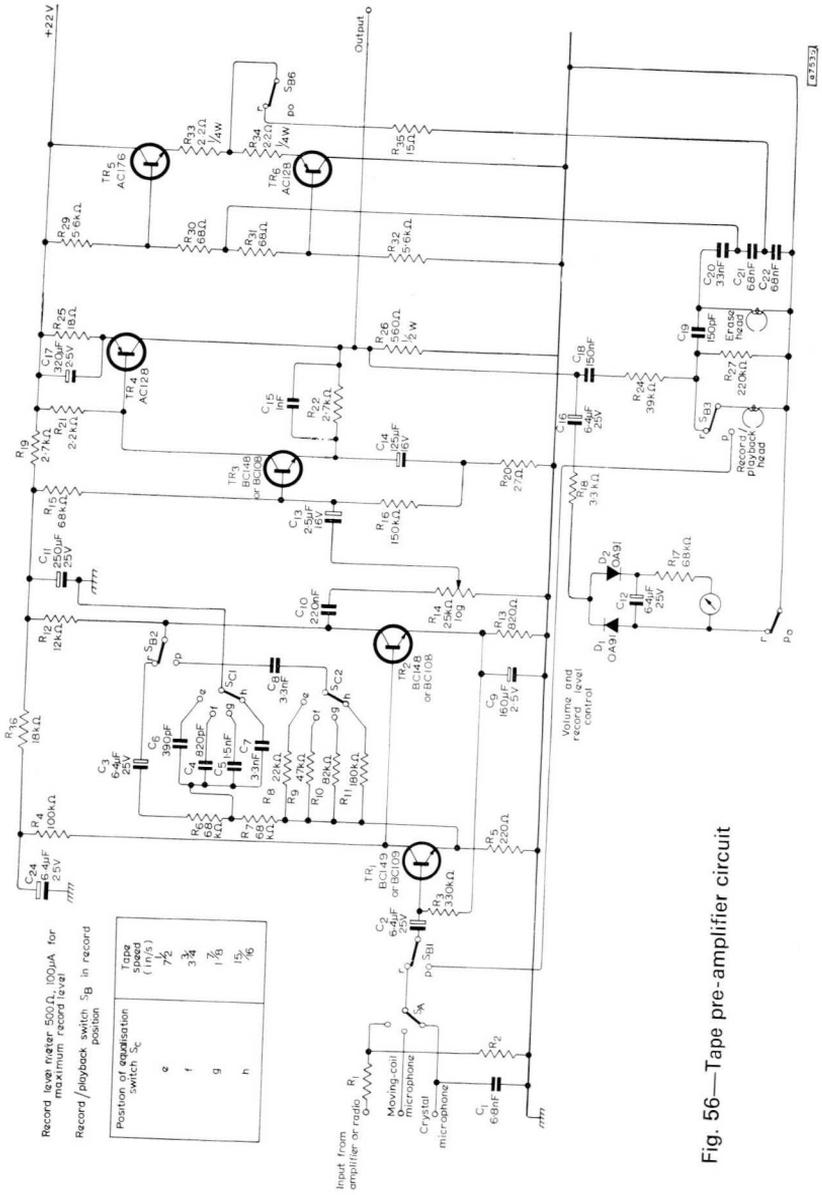


Fig. 56—Tape pre-amplifier circuit





derived from the erase voltages across the erase heads as in the mono design. This has the advantage that the other pair of complementary transistors used for the output stage during playback may now be used as a monitoring facility.

### Bias and erase power from two oscillators with locked frequencies

A circuit that uses two locked identical oscillators for stereo operation is given in Fig. 58. Locking of the oscillators is achieved by connecting together the two feedback paths.

### Recording level indicator

Fig. 59 shows a recording level indicator for stereo operation. The meter gives a reading proportional to the peak-to-peak voltage at the collector of the driver transistor in the channel which has the highest recording level. For an input of 4V r.m.s. (this corresponds to the r.m.s. voltage at the collector of the driver transistor when distortion due to tape saturation becomes significant) the d.c. current through the meter is  $95\mu\text{A}$ .

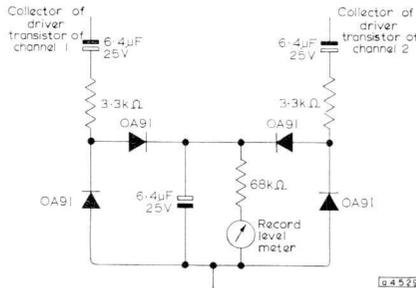


Fig. 59—Recording level indicator for stereo operation

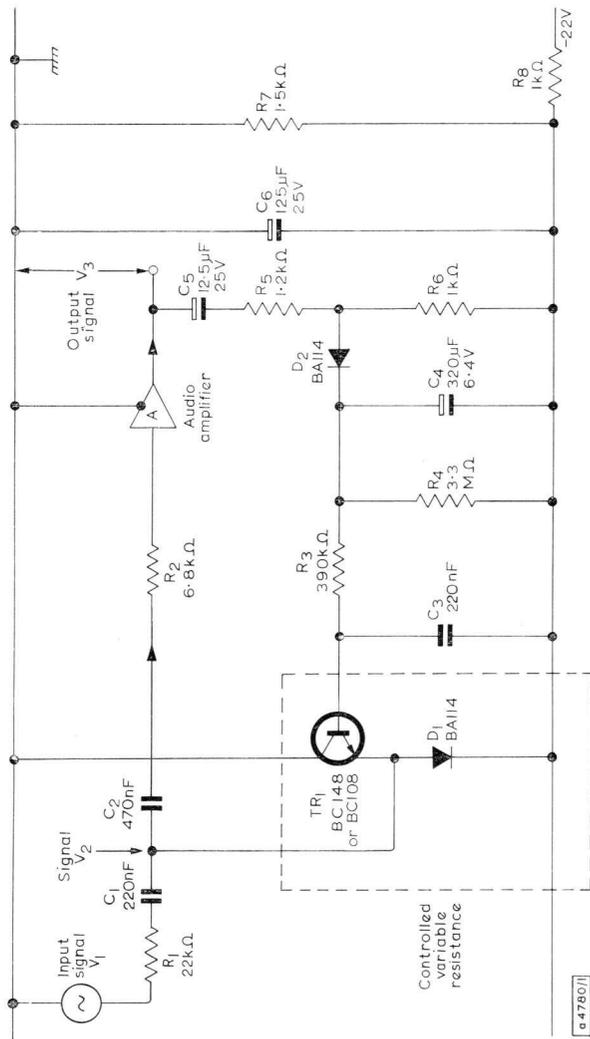


Fig. 60—Automatic gain control circuit

## A.G.C. CIRCUIT FOR TAPE RECORDERS

When recording on tape, the current in the recording head must not exceed the value at which tape saturation occurs if severe distortion is to be avoided. This can be prevented by monitoring the current by means of a meter or magic eye, and manually adjusting the recording level. Another method is to use a circuit that electronically reduces the gain of the amplifier when the optimum recording level is exceeded.

To ensure that the distortion is recorded for only a short time, the gain control must respond very rapidly to the overload signal. When the gain has been reduced, however, the recovery time must be long, for otherwise volume compression will result, and loud and soft passages of music will be recorded with equal loudness.

A gain control circuit that uses a minimum of components and can produce an attenuation of 40dB within 150 milliseconds is shown in Fig. 60. The recovery rate does not exceed 6dB per minute. With a faster recovery rate, the same circuit arrangement is suitable as a volume compressor in other applications.

### Circuit Description

Gain control is achieved by means of an attenuator containing a diode. Controlling the direct current through the diode controls its slope resistance, and, consequently, the amount of attenuation.

The severe harmonic distortion caused by the exponential characteristic of one diode can be reduced by using two diodes in a reverse-parallel arrangement. In the circuit in Fig. 60, the base-emitter junction of a transistor is used as one of the diodes. Because the transistor is needed as a d.c. amplifier, this arrangement saves the expense of one diode.

Part of the amplifier output is rectified and used to provide the gain control signal. The time constants of the rectifier circuit are such as to give the high rate of attenuation and the long recovery time.

In Fig. 60 unit A is the audio amplifier and  $R_2$  represents its input resistance, which should be about  $7k\Omega$ .

The variable attenuator comprises  $R_1$ ,  $C_1$ ,  $D_1$  and part of the transistor  $TR_1$ . Because  $C_3$  is a short circuit to a.c. signals, the base-emitter junction of the transistor is, in effect, in reverse-parallel with  $D_1$  for all a.c. signals.

Resistors  $R_5$  and  $R_6$  form a fixed attenuator by means of which a constant fraction of the output is fed back to the control circuit. The feedback voltage is rectified by  $D_2$ , charges  $C_4$ , and is applied through  $R_3$  to the base of  $TR_1$ . Hence, the voltage across  $C_4$  controls the current through  $TR_1$  and  $D_1$ .

With an input signal well below that which causes tape saturation, the voltage across  $C_4$  is low. Therefore, the transistor current is also low and

the slope resistances of it and the diode are high. Consequently, the shunting effect that the diode and transistor have on the input to the amplifier is negligible.

As the input signal is increased, the voltage across  $C_4$  and the current through  $TR_1$ , will also increase. Eventually, the transistor current will reach a value which produces a significant reduction in the slope resistance of  $D_1$ . The voltage drop across  $R_1$  will be increased and there will be an appreciable attenuation of the signal to the amplifier. This occurs when the amplifier has an output of approximately 2V r.m.s.

A further increase in the input produces another rise in the voltage across  $C_4$ . The consequent increase in transistor current now produces a rapid reduction in the diode slope resistance. The shunting effect of the transistor and diode on the input to the amplifier is greatly increased, and  $V_2$  is much less than  $V_1$ .

Once attenuation has started, voltages  $V_2$  and  $V_3$  remain practically constant. Over the full range of attenuation, 40dB, they increase slightly because of slight increases in  $V_{BE}$ , the forward voltage of  $D_1$ , at higher currents (of the order of  $300\mu A$ ), and the base current through  $R_3$ .

The attack time is largely determined by the time constant of  $C_4$  and the source impedance of the charging circuit, which is  $R_5$  in parallel with  $R_6$ . For an attack time of about 200ms, the source impedance should be approximately  $600\Omega$ .

The recovery time is determined by the time constant of  $C_4$  and its discharge circuit— $R_4$  in parallel with  $R_3$  and the slope resistances of  $TR_1$  and  $D_1$ . Over a wide range of the attenuation,  $R_3$  is much larger than the slope resistances of the diode and transistor. The rate of discharge of  $C_4$  is then controlled by the value of  $R_3$ , and, consequently, the rate of change of attenuation is constant. At very low transistor currents, the slope resistances of the diode and the transistor greatly exceed  $R_3$ , and the rate of discharge of  $C_4$  via the transistor is very low. This tends to make the rate of change of attenuation also very low. Under these conditions, however,  $R_4$  provides an alternative discharge path. Hence, the rate of change of attenuation has a low limit that is determined by the value of  $R_4$ . When  $R_3$  is large with respect to the slope resistances of the diode and the transistor, the effect of  $R_4$  is negligible.

The transistor is a BC148 or BC108 n-p-n planar type, which, with its low leakage current and high gain, makes this simple arrangement possible. The silicon diodes also are used because of their low leakage currents.

In Fig. 60, the gain is controlled by attenuating the signal before it reaches the audio amplifier. This has the disadvantage that, when the signal is attenuated, the noise originating in the first transistor of the



This is shown in Fig. 62 by the input/output characteristics of the circuit with high-gain and low-gain transistors. When a low-gain transistor is used, an attenuation of 40dB is accompanied by an increase of 7dB in the output; with a high-gain transistor, the corresponding increase in output is 4.5dB.

The change of attenuation with time is shown in Fig. 63. This diagram shows that the rate of change of attenuation is substantially constant over much of the range. It does not exceed 6dB per minute and is almost independent of the gain of the transistor.

The variation of total harmonic distortion of  $V_2$  with the amount of attenuation for various values of  $V_2$  is given in Fig. 64. These curves show that  $V_2$  should not exceed 4mV r.m.s. if the total harmonic distortion is not to exceed 2%.

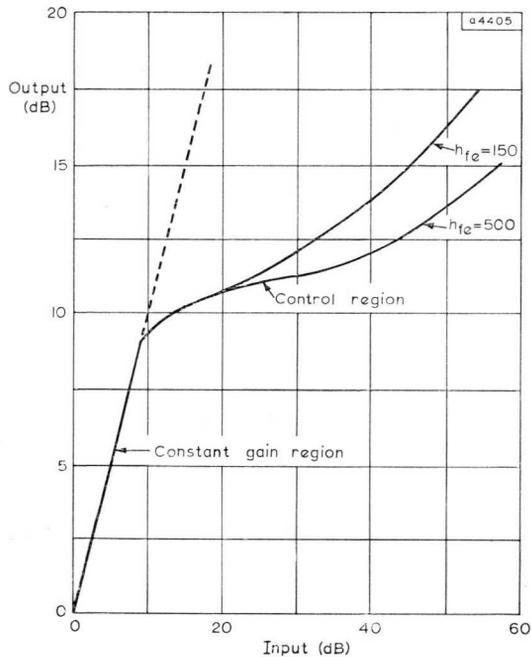


Fig. 62—Variation of output with input for high-gain and low-gain transistors

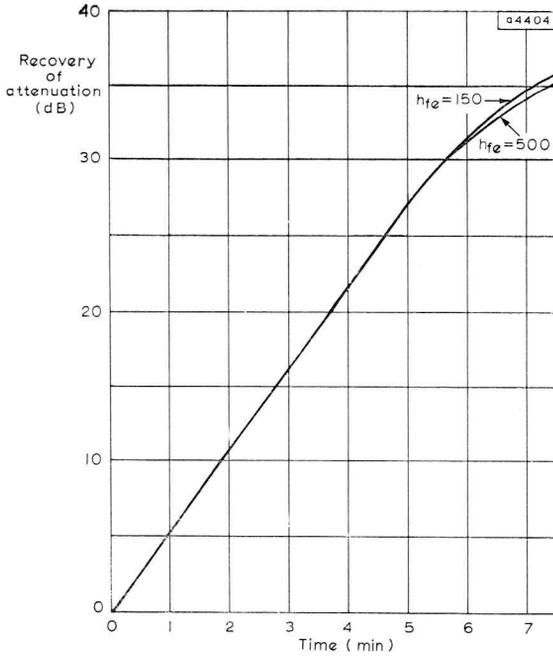


Fig. 63—Decrease of attenuation with time for high-gain and low-gain transistors

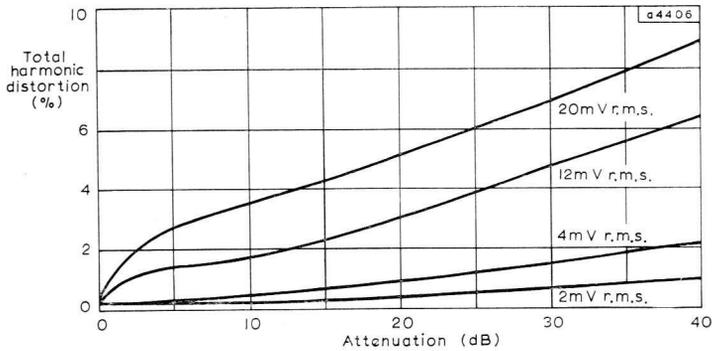


Fig. 64—Variation of total harmonic distortion of  $V_2$  with amount of attenuation, for various values of  $V_2$

## COMPONENT LISTS FOR CIRCUITS IN CHAPTER 5

### 4W Tape Recorder (page 70)

#### Heads

Record/playback head	Marriot X/RPS/36
Erase head	Marriot X/ES/11

#### Transistors and Diodes

Circuit reference	Mullard type
TR <sub>1</sub>	BC149 or BC109
TR <sub>2</sub>	BC148 or BC108
TR <sub>3</sub>	BC148 or BC108
TR <sub>4</sub>	AC128
TR <sub>5</sub>	AD161
TR <sub>6</sub>	AD162
D <sub>1</sub>	OA91
D <sub>2</sub>	OA91
Full-wave bridge rectifier	BY164

#### Resistors

Tolerance:  $\pm 5\%$  except R<sub>33</sub> and R<sub>34</sub>, which may be  $\pm 10\%$  components

Power rating:  $\frac{1}{8}$ W except R<sub>26</sub>, which should be a  $\frac{1}{2}$ W component, R<sub>33</sub> and R<sub>34</sub>, which should be  $\frac{1}{4}$ W components

Circuit reference	Value	Circuit reference	Value
R <sub>1</sub>	chosen to	R <sub>20</sub>	27 $\Omega$
R <sub>2</sub>	suit input	R <sub>21</sub>	2.2k $\Omega$
R <sub>3</sub>	330k $\Omega$	R <sub>22</sub>	2.7k $\Omega$
R <sub>4</sub>	100k $\Omega$	R <sub>23</sub>	presets
R <sub>5</sub>	220k $\Omega$		potentiometer
R <sub>6</sub>	68k $\Omega$	R <sub>24</sub>	39k $\Omega$
R <sub>7</sub>	68k $\Omega$	R <sub>25</sub>	18 $\Omega$
R <sub>8</sub>	22k $\Omega$	R <sub>26</sub>	560 $\Omega$
R <sub>9</sub>	47k $\Omega$	R <sub>27</sub>	220k $\Omega$
R <sub>10</sub>	82k $\Omega$	R <sub>28</sub>	thermistors
R <sub>11</sub>	180k $\Omega$		type VA1077
R <sub>12</sub>	12k $\Omega$	R <sub>29</sub>	5.6k $\Omega$
R <sub>13</sub>	820 $\Omega$	R <sub>30</sub>	68 $\Omega$
R <sub>14</sub>	logarithmic potentiometer	R <sub>31</sub>	68 $\Omega$
		R <sub>32</sub>	5.6k $\Omega$
R <sub>15</sub>	68k $\Omega$	R <sub>33</sub>	1 $\Omega$
R <sub>16</sub>	150k $\Omega$	R <sub>34</sub>	1 $\Omega$
R <sub>17</sub>	68k $\Omega$	R <sub>35</sub>	15 $\Omega$
R <sub>18</sub>	3.3k $\Omega$	R <sub>36</sub>	18k $\Omega$
R <sub>19</sub>	2.7k $\Omega$		

## Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	6·8nF	polyester	C296AC/A6K8
C <sub>2</sub>	6·4μF	electrolytic 25V	C426AR/F6·4
C <sub>3</sub>	6·4μF	electrolytic 25V	C426AR/F6·4
C <sub>4</sub>	820pF	polystyrene	C295AC/820E
C <sub>5</sub>	1·5nF	polyester	C296AC/A1K5
C <sub>6</sub>	390pF	polystyrene	
C <sub>7</sub>	3·3nF	polyester	C296AC/A3K3
C <sub>8</sub>	3·3nF	polyester	C296AC/A3K3
C <sub>9</sub>	160μF	electrolytic 2·5V	C426AR/A160
C <sub>10</sub>	220nF	polyester	C296AA/A220K
C <sub>11</sub>	250μF	electrolytic 25V	C437AR/F250
C <sub>12</sub>	6·4μF	electrolytic 25V	C426AR/F6·4
C <sub>13</sub>	2·5μF	electrolytic 16V	C426AR/H2·5
C <sub>14</sub>	125μF	electrolytic 16V	C426AR/E125
C <sub>15</sub>	1nF	polyester	C296AC/A1K
C <sub>16</sub>	6·4μF	electrolytic 25V	C426AR/F6·4
C <sub>17</sub>	320μF	electrolytic 2·5V	C426AR/A320
C <sub>18</sub>	150nF	polyester	C296AA/A150K
C <sub>19</sub>	150pF	ceramic plate	C333CH/C150E
C <sub>20</sub>	33nF	polyester	C296AA/A33K
C <sub>21</sub>	68nF	polyester	C296AA/A68K
C <sub>22</sub>	68nF	polyester	C296AA/A68K
C <sub>23</sub>	640μF	electrolytic 16V	C437AR/E640
C <sub>24</sub>	6·4μF	electrolytic 25V	C426AR/F6·4
C <sub>25</sub>	640μF	electrolytic 25V	C437AR/F640

## Mains Transformer

The transformer used in this circuit may be obtained from the following manufacturers under the type numbers given:

Colne Electric Limited, Rickmansworth, Herts	20042
Drake Transformers Limited, Billericay, Essex	351-245
Gardners Transformers Limited, Christchurch, Hants	GR 97182
Parmeko Limited, Aylestone Park, Leicester	P 3203

## Heatsinks

Each output transistor should be mounted on a 1·5mm (16 gauge) bright aluminium heatsink with an area of 26cm<sup>2</sup>. The driver transistor TR<sub>4</sub> should be mounted by means of a heat clip onto a 1·5mm bright aluminium heatsink with an area of 13cm<sup>2</sup>.

## Tape Pre-amplifier (page 76)

As for the tape recorder amplifier (page 86) except:

### Transistors

TR <sub>5</sub>	AC176
TR <sub>6</sub>	AC128

### Resistors

R <sub>23</sub>	omitted
R <sub>28</sub>	omitted
R <sub>33</sub>	2·2Ω
R <sub>34</sub>	2·2Ω

### Capacitors

C <sub>23</sub>	omitted
-----------------	---------

## A.G.C. Circuit (page 80)

### Transistor and Diode

Circuit reference	Mullard type
TR <sub>1</sub>	BC148 or BC108
D <sub>1</sub>	BA114

### Resistors

Tolerance:  $\pm 5\%$  except R<sub>4</sub>, which may be a  $\pm 10\%$  component

Power rating:  $\frac{1}{8}$ W

Circuit reference	Value
R <sub>1</sub>	22kΩ
R <sub>2</sub>	see text
R <sub>3</sub>	390kΩ
R <sub>4</sub>	3·3MΩ
R <sub>5</sub>	1·2kΩ
R <sub>6</sub>	1kΩ
R <sub>7</sub>	1·5kΩ
R <sub>8</sub>	1kΩ

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	220nF	polyester	C296AA/A220K
C <sub>2</sub>	470nF	polyester	C296AA/A470K
C <sub>3</sub>	220nF	polyester	C296AA/A220K
C <sub>4</sub>	320μF	electrolytic 6·4V	C426AR/C320
C <sub>5</sub>	12·5μF	electrolytic 25V	C426AR/F12·5
C <sub>6</sub>	125μF	electrolytic 25V	C426AR/E125

## CHAPTER 6

# CAR RADIOS

The chapter is divided into two sections comprising:

1. Two a.f. amplifiers, a 5W class A amplifier and a 6W class B amplifier, suitable for use in a car radio;
2. R.F. and i.f. stages for a car radio.

Attention is again drawn to the difficulties associated with the construction and alignment of r.f. and i.f. stages, as stated earlier. Access to specialised equipment is essential to those wishing to build these circuits.

Component lists for the circuits are given at the end of the chapter.

## A.F. STAGES

### 5W CLASS A AMPLIFIER

The circuit of a 5W class A audio amplifier for use in a car radio is given in Fig. 65. It contains two BC148 or BC108 transistors and one BD121 transistor, and is designed to operate from a nominal 14V supply.

#### Circuit Description

Direct coupling is used between stages, and the base-emitter voltage of TR<sub>1</sub> serves as a reference for the emitter voltage of TR<sub>3</sub>. Consequently, the emitter voltage of TR<sub>1</sub> controls the direct current through TR<sub>3</sub> and determines its operating point.

Variable resistor R<sub>11</sub> is used to set the quiescent current—900mA—of the output stage. The loudspeaker is driven by means of a centre-tapped choke which incorporates a small winding to provide feedback to the first stage. The choke has an inductance of 30mH and a d.c. resistance of 1Ω. The voltage ratio of choke to secondary is 13:1. Resistor R<sub>10</sub> and capacitor C<sub>5</sub> limit the frequency response of the feedback loop and amplifier.

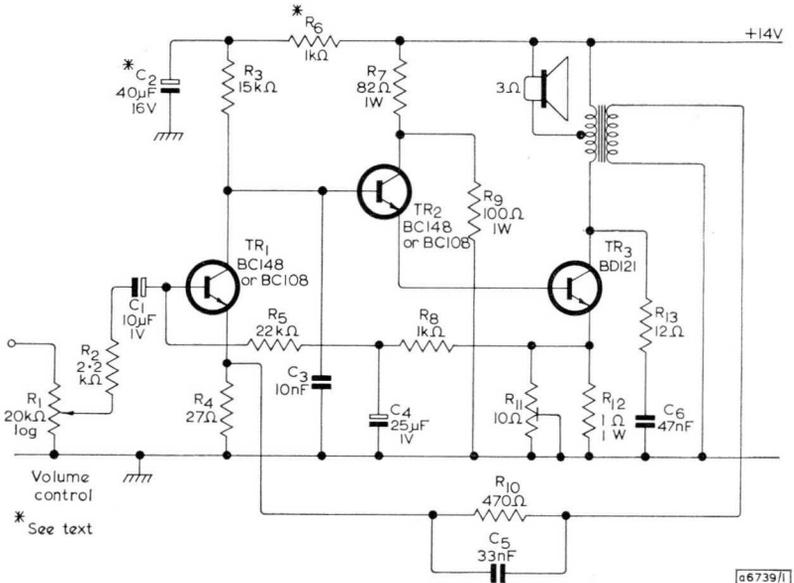


Fig. 65—5W class A audio amplifier circuit for use in a car radio

Resistor  $R_{13}$  and capacitor  $C_6$  are included to ensure that the load remains resistive, and hence the circuit stable, at high frequencies. As low-frequency stability depends upon the source impedance, a  $2.2k\Omega$  resistor,  $R_2$ , is connected in series with the wiper of the volume control  $R_1$ .

Decoupling between resistors  $R_3$  and  $R_7$  is effected by resistor  $R_6$  and capacitor  $C_2$ . The values given for  $R_6$  and  $C_2$  in the circuit diagram may have to be modified as they depend upon the decoupling at the supply input. The voltage drop across  $R_6$  should not exceed 1V; if it does, the value of  $R_3$  must be reduced.

### Performance

Output power with symmetrical clipping	5W r.m.s.
Sensitivity (input for 5W output with volume control set for maximum volume)	43mV
Frequency response ( $-3dB$ points)	50Hz to 10kHz
Input resistance (including $2.2k\Omega$ resistor but excluding volume control)	$13k\Omega$
Negative feedback	12dB
Distortion at 5W output (see Fig. 66)	$2.5\%$

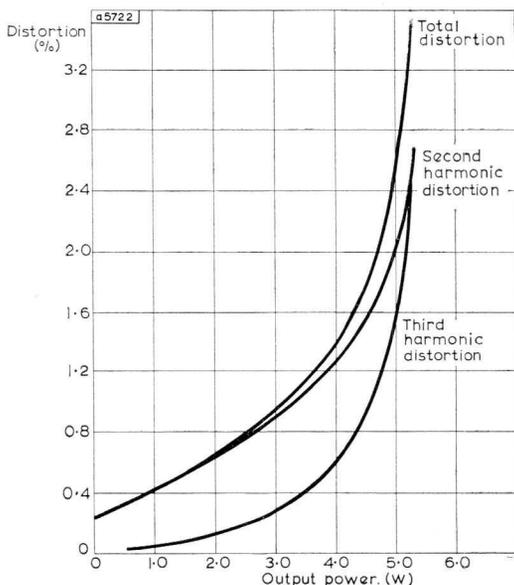


Fig. 66—Variation of harmonic distortion with output power

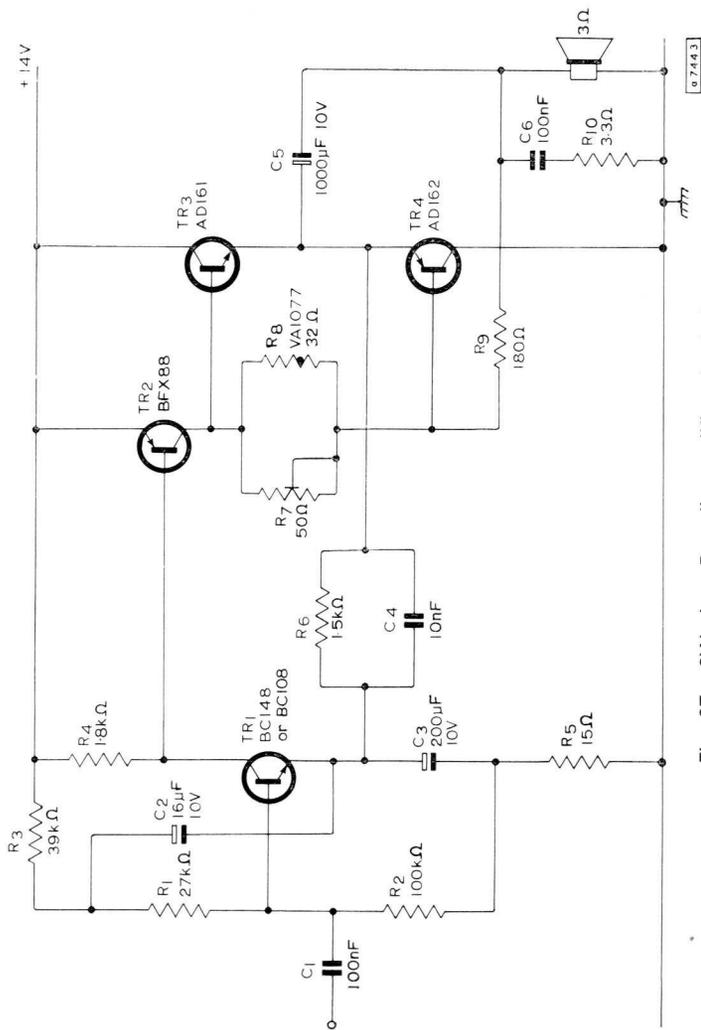


Fig. 67—6W class B audio amplifier circuit for use in a car radio

## 6W CLASS B AMPLIFIER

The circuit of a 6W class B audio amplifier for use in a car radio is shown in Fig. 67. The amplifier contains an AD161/AD162 complementary output pair, a BFX88 driver transistor, and a BC148 or BC108 transistor as the first-stage amplifier.

### Circuit Description

The amplifier is a conventional four-transistor circuit with one exception: the decoupling capacitor  $C_2$  in the input stage is returned to the emitter of transistor  $TR_1$  instead of to chassis. The purpose of this is two-fold: firstly, to neutralise the effect of ripple on the h.t. line, and secondly, to bootstrap the base resistor, thereby increasing the input resistance.

### Performance

Output power	6W r.m.s.
Sensitivity for full output	52mV
Frequency response at 3W ( $-3$ dB points)	74Hz to 10.6kHz
Input resistance at 1kHz	100k $\Omega$
Feedback	20dB
Distortion at 6W output (see Fig. 68)	1.2%
Quiescent current in output stage only	30mA
Total current at 6W output	700mA

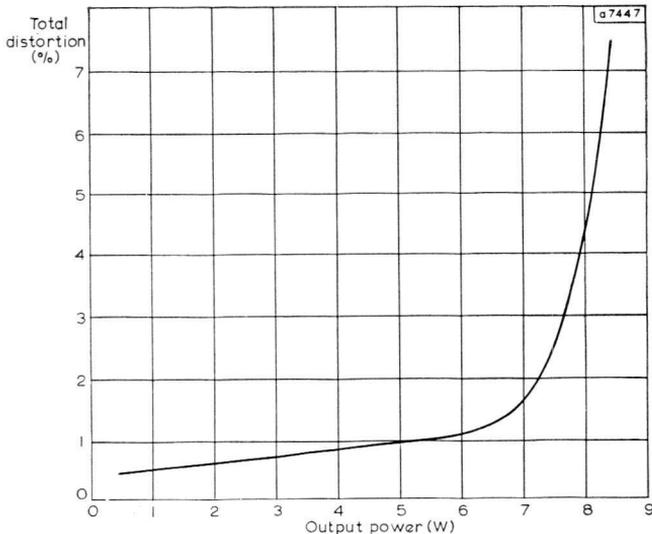


Fig. 68—Variation of total harmonic distortion with output power

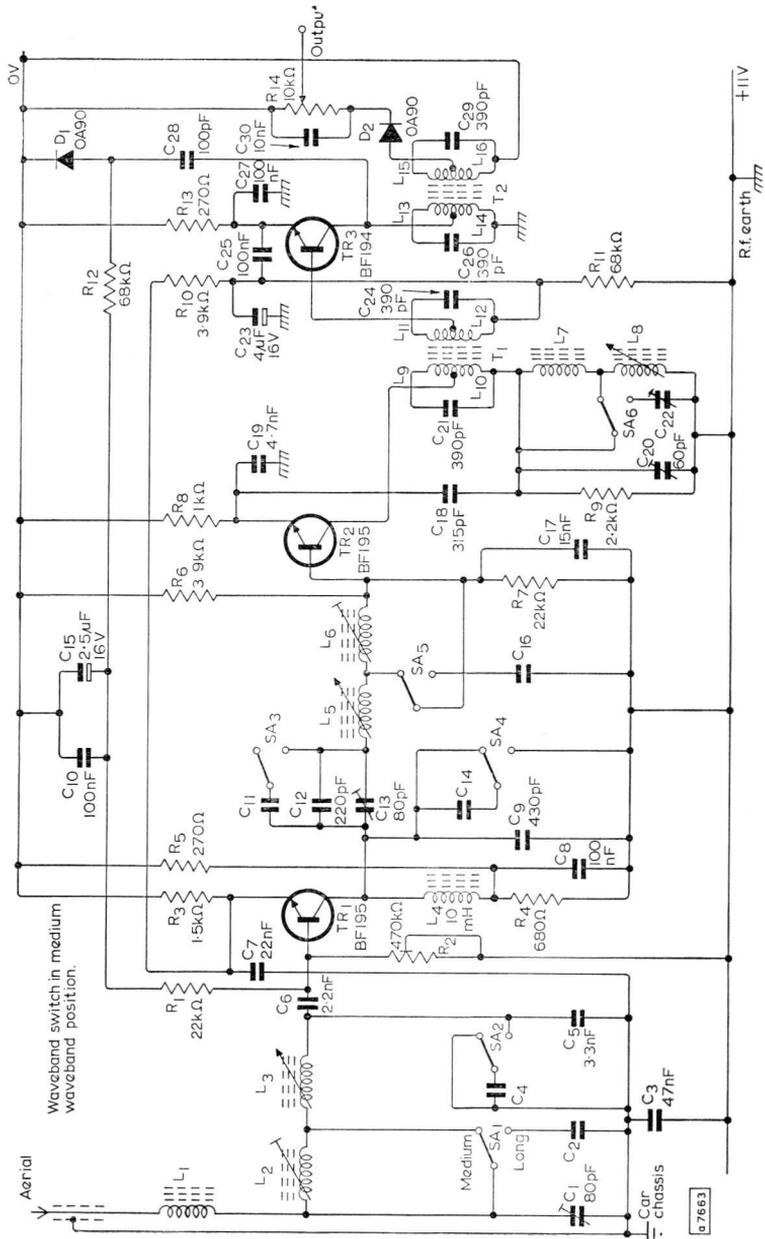


Fig. 69—R.F. and i.f. stages of a car radio receiver

## R.F. AND I.F. STAGES

The r.f. and i.f. stages of a medium- and long-wave car radio are shown in Fig. 69. The circuit is designed to operate from an 11V supply and uses two BF195 transistors and one BF194 transistor.

### Circuit Description

#### *R.F. Amplifier and Self-oscillating Mixer Stages*

The design of the r.f. amplifier stage is necessarily one of compromise between factors such as gain, noise performance, signal handling and avoidance of mixer blocking.

The wide range of a.g.c. required of a car radio can be satisfactorily met by applying full control to the r.f. amplifier. The maximum signal handling can be achieved by ensuring that the base of the r.f. amplifier is ultimately reverse-biased by the a.g.c. circuit.

A serious limitation encountered when using an r.f. amplifier in front of a self-oscillating mixer is r.f. blocking of the oscillator. If the receiver is tuned rapidly to a strong carrier (for example, by a push button), a very large signal can appear at the mixer base before the a.g.c. voltage has time to build up. Consequently the oscillator may be prevented from operating, and the receiver will be blocked. In this design, it was found necessary to limit the maximum input to the mixer stage (a) by the choice of tapping ratio between the r.f. amplifier collector and the mixer base, and (b) by reducing the r.f. amplifier collector voltage. These requirements limit the r.f. gain to a value considerably lower than could otherwise be achieved with the BF195.

A conventional car-radio mixer is used, comprising a capacitively-tapped Colpitts oscillator, and using a BF195 transistor. The gain of the stage is limited by the oscillator voltage developed across the primary of the first i.f. transformer  $T_1$  on the long waveband.

#### *I.F. Stage*

The increase in stage gain, theoretically possible when transistors with low feedback capacitance are used, is obtained only if the stage gain is not determined by the a.g.c. line damping, which limits the collector loading of the i.f. stage. In the past, the limitation in loading has necessitated a rather high value of base source impedance. This has the disadvantage of giving considerable spreads and reduced selectivity, which can be overcome only by some sacrifice in gain. With the BF194, however, it is possible to realise this increase in gain quite simply, by using a high value of preset potentiometer ( $R_2$ ) as one of the bias resistors of the r.f. amplifier. This allows a high value of collector load to be used in the i.f. stage.

The temperature effects with silicon planar transistors are small, and

virtually the only requirement for stabilisation is that the spreads in quiescent current should be small.

### Detector

The a.f. amplifiers recommended for use with this circuit have input impedances greater than  $10k\Omega$ . A high value of detector load resistance ( $10k\Omega$  potentiometer  $R_{14}$ ) can therefore be used. This allows the diode to work at a higher voltage level, and results in increased diode efficiency and about 2 to 3dB improvement in sensitivity.

### Performance

Sensitivity for 7mV output at detector, at 1MHz with 30% modulation	1.4 $\mu$ V
Signal-to-noise ratio with 15pF/60pF aerial:	
1.4 $\mu$ V aerial e.m.f.	5dB
10 $\mu$ V aerial e.m.f.	20dB
A.G.C. range for 10dB change in output (see Fig. 70)	90dB
Maximum signal handling*	
30% modulation	2V
80% modulation	1V
Oscillator drive voltage, for medium waveband:	
oscillator frequency = 2.11MHz	100mV
oscillator frequency = 1.01MHz	120mV

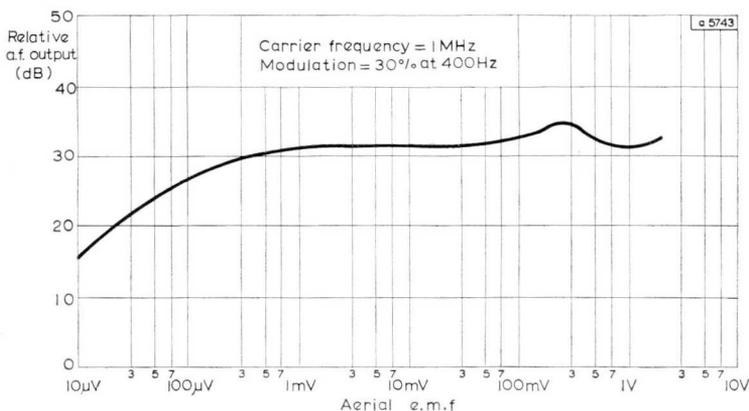


Fig. 70—Automatic gain control characteristic

\*No mixer blocking occurs at any signal level

## COMPONENT LISTS FOR CIRCUITS IN CHAPTER 6

### 5W Class A Amplifier (page 90)

#### Transistors

Circuit reference	Mullard type
TR <sub>1</sub>	BC148 or BC108
TR <sub>2</sub>	BC148 or BC108
TR <sub>3</sub>	BD121

#### Resistors

Circuit reference	Value	Tolerance (%)	Power rating (W)
R <sub>1</sub> logarithmic potentiometer	20k $\Omega$		
R <sub>2</sub>	2.2k $\Omega$	$\pm 20$	$\frac{1}{8}$
R <sub>3</sub>	15k $\Omega$	$\pm 20$	$\frac{1}{8}$
R <sub>4</sub>	27 $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>5</sub>	22k $\Omega$	$\pm 20$	$\frac{1}{8}$
R <sub>6</sub>	1k $\Omega$	$\pm 20$	$\frac{1}{8}$
R <sub>7</sub>	82 $\Omega$	$\pm 10$	1
R <sub>8</sub>	1k $\Omega$	$\pm 20$	$\frac{1}{8}$
R <sub>9</sub>	100 $\Omega$	$\pm 10$	1
R <sub>10</sub>	470 $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>11</sub> preset potentiometer	10 $\Omega$		
R <sub>12</sub>	1 $\Omega$	$\pm 20$	1
R <sub>13</sub>	12 $\Omega$	$\pm 20$	$\frac{1}{8}$

#### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	10 $\mu$ F	electrolytic 1V	C426AR/E10
C <sub>2</sub>	40 $\mu$ F	electrolytic 16V	C426AR/E40
C <sub>3</sub>	10nF	polyester	C296AA/A10K
C <sub>4</sub>	25 $\mu$ F	electrolytic 1V	C426AR/C25
C <sub>5</sub>	33nF	polyester	C296AA/A33K
C <sub>6</sub>	47nF	polyester	C296AA/A47K

#### Heatsinks

The values of R<sub>7</sub> and R<sub>9</sub> ensure that the maximum permissible junction temperature of transistor TR<sub>2</sub> is not exceeded and so no heat clip is required. The output transistor, however, has a maximum dissipation of 11W; therefore at an ambient temperature of 60°C, a 1.5mm (16 gauge) bright aluminium heatsink with an area of 50cm<sup>2</sup> is required.

## 6W Class B Amplifier (page 94)

### Transistors

Circuit reference	Mullard type
TR <sub>1</sub>	BC148 or BC108
TR <sub>2</sub>	BFX88
TR <sub>3</sub>	AD161
TR <sub>4</sub>	AD162

### Resistors

Circuit reference	Value	Tolerance (%)	Power rating (W)
R <sub>1</sub>	27k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>2</sub>	100k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>3</sub>	39k $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>4</sub>	1.8k $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>5</sub>	15 $\Omega$	$\pm 5$	$\frac{1}{8}$
R <sub>6</sub>	1.5k $\Omega$	$\pm 10$	$\frac{1}{8}$
R <sub>7</sub> preset potentiometer	50 $\Omega$		
R <sub>8</sub> thermistor type VA1077	32 $\Omega$		
R <sub>9</sub>	180 $\Omega$	$\pm 10$	$\frac{1}{2}$
R <sub>10</sub>	3.3 $\Omega$	$\pm 10$	$\frac{1}{8}$

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	100nF	polyester	C296AA/A100K
C <sub>2</sub>	16 $\mu$ F	electrolytic 10V	C426AR/D16
C <sub>3</sub>	200 $\mu$ F	electrolytic 10V	C426AR/D200
C <sub>4</sub>	10nF	polyester	C296AA/A10K
C <sub>5</sub>	1000 $\mu$ F	electrolytic 10V	C437AR/D1000
C <sub>6</sub>	100nF	polyester	C296AA/A100K

### Heatsinks

The driver dissipation is only 350mW, so no heatsink is required for this transistor. If mica washers are used, each output transistor should be mounted on a 1.5mm (16 gauge) bright aluminium heatsink with an area of 16cm<sup>2</sup>.

## R.F. and I.F. Stages (page 94)

### Transformers

Both i.f. transformers are double-tuned and critically coupled; they are wound on 4.8mm diameter formers, with ferrite slugs and frames.

First i.f. transformer— $T_1$

$L_9 + L_{10}$  80 + 30 turns of  $6 \times 46$  s.w.g. litz wire;

\* $Z_{do} = 50k\Omega$ ,  $Q_o = 140$

$L_{11} + L_{12}$  5 + 105 turns of  $6 \times 46$  s.w.g. litz wire;

$Z_{do} = 235\Omega$ ,  $Q_o = 150$

Second i.f. transformer— $T_2$

$L_{13} + L_{14}$  60 + 50 turns of  $6 \times 64$  s.w.g. litz wire;

$Z_{do} = 35k\Omega$ ,  $Q_o = 150$

$L_{15} + L_{16}$  35 + 75 turns of  $6 \times 64$  s.w.g. litz wire;

$Z_{do} = 10k\Omega$ ,  $Q_o = 150$

Coils for which no details are given are part of the permeability tuner.

### Transistors and Diodes

Circuit reference	Mullard type
TR <sub>1</sub>	BF195
TR <sub>2</sub>	BF195
TR <sub>3</sub>	BF194
D <sub>1</sub>	OA90
D <sub>2</sub>	OA90

### Resistors

Tolerance:  $\pm 5\%$

Power rating:  $\frac{1}{8}W$

Circuit reference	Value
R <sub>1</sub>	22k $\Omega$
R <sub>2</sub> carbon trimming potentiometer	470k $\Omega$
R <sub>3</sub>	1.5k $\Omega$
R <sub>4</sub>	680 $\Omega$
R <sub>5</sub>	270 $\Omega$
R <sub>6</sub>	3.9k $\Omega$
R <sub>7</sub>	22k $\Omega$
R <sub>8</sub>	1k $\Omega$
R <sub>9</sub>	2.2k $\Omega$
R <sub>10</sub>	3.9k $\Omega$
R <sub>11</sub>	68k $\Omega$
R <sub>12</sub>	68k $\Omega$
R <sub>13</sub>	270 $\Omega$
R <sub>14</sub> logarithmic carbon potentiometer	10k $\Omega$

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\* $Z_{do}$  = coil impedance with the other coil open-circuited.

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	80pF	trimmer	
C <sub>3</sub>	47nF	polyester	C296AA/A47K
C <sub>5</sub>	3.3nF	polyester	C296AC/A3K3
C <sub>6</sub>	2.2nF	polyester	C296AC/A2K2
C <sub>7</sub>	22nF	polyester	C296AA/A22K
C <sub>8</sub>	100nF	polyester	C296AA/A100K
C <sub>9</sub>	430pF	polystyrene	
C <sub>10</sub>	100nF	polyester	C296AA/A100K
C <sub>12</sub>	220pF	polystyrene	
C <sub>13</sub>	80pF	trimmer	
C <sub>15</sub>	2.5μF	electrolytic 16V	C426AR/H2.5
C <sub>17</sub>	15nF	polyester	C296AA/A15K
C <sub>18</sub>	315pF	polystyrene	
C <sub>19</sub>	4.7nF	polyester	C296AC/A4K7
C <sub>20</sub>	60pF	trimmer	808 01011
C <sub>21</sub>	390pF	polystyrene	
C <sub>23</sub>	4μF	electrolytic 16V	C426AR/G4
C <sub>24</sub>	390pF	polystyrene	
C <sub>25</sub>	100nF	polyester	C296AA/A100K
C <sub>26</sub>	390pF	polystyrene	
C <sub>27</sub>	100nF	polyester	C296AA/A100K
C <sub>28</sub>	100pF	ceramic plate	C333CH/C100E
C <sub>29</sub>	390pF	polystyrene	
C <sub>30</sub>	10nF	polyester	C296AA/A10K

Capacitors for which no values are given are part of the permeability tuner.

## CHAPTER 7

# HIGH-QUALITY AUDIO EQUIPMENT

In this chapter audio amplifiers with output powers of 10W and 25W are described, together with a pre-amplifier suitable for use with either amplifier. The chapter includes auxiliary audio amplifiers, control circuits and filters.

In the construction of high-quality equipment attention must be paid to component layout; the recommendations made in this chapter should be carefully followed.

Components lists for the circuits are given at the end of the chapter.

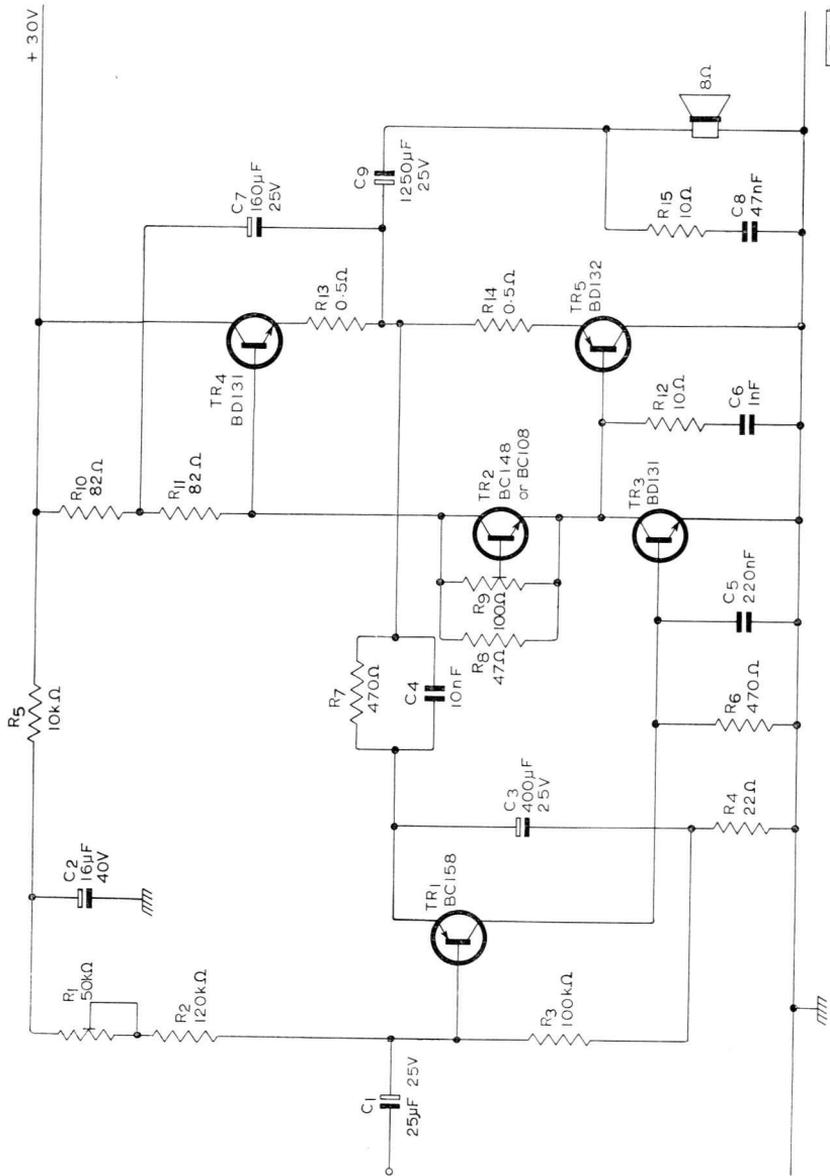


Fig. 71—10W high-quality audio amplifier circuit

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## 10W AUDIO AMPLIFIER

The circuit for a 10W high-quality audio amplifier is shown in Fig. 71. The use of a complementary pair of output transistors gives a much simpler circuit than the quasi-complementary circuit usually employed in class B hi-fi amplifiers. In addition, the greater symmetry of the circuit gives lower distortion, particularly in the crossover region.

### Circuit Description

The circuit uses a BD131/BD132 complementary pair to deliver an output power of 10W at a distortion level of less than 0.1%. The familiar four-transistor, directly-coupled configuration is used, but an additional transistor is included to stabilise the quiescent current of the output transistors. Preset potentiometer  $R_1$  sets the mid-point voltage for symmetrical clipping.

### Power Supply

Fig. 72 shows a suitable power supply. The supply requirements are:

Total quiescent current for one channel	120mA
Full load current for one channel (at 30V)	600mA
Supply voltage	30V
Maximum supply voltage	40V

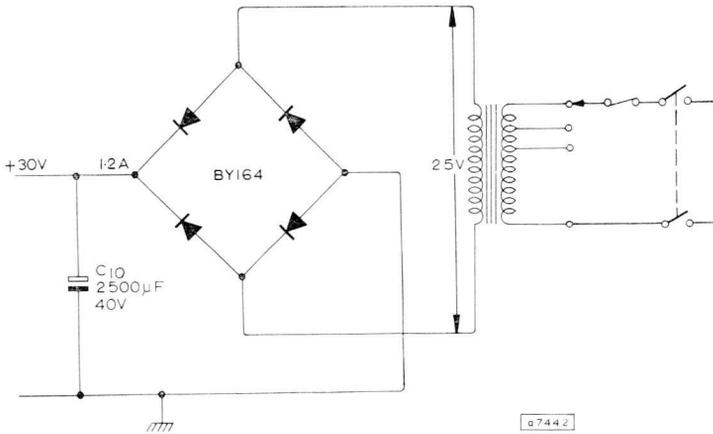


Fig. 72—Power supply circuit for 10W amplifier

## Performance

Output power (with 30V supply)	10W r.m.s.
Sensitivity for full output	430mV
Frequency response at 2W output (-3dB points)	20Hz to 35kHz
Input resistance	90k $\Omega$
Distortion at 10W output (see Fig. 73)	< 0.1%
Quiescent current of output transistors	15mA

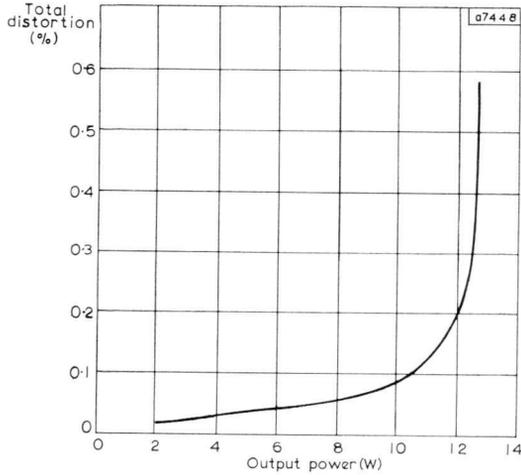


Fig. 73—Variation of total harmonic distortion with output power

## 25W AUDIO AMPLIFIER

The circuit of a 25W high-quality amplifier suitable for use as one channel of a stereo system is shown in Fig. 74. In this circuit, two matched BDY20 output transistors are driven by a matched complementary pair consisting of one BFX29 and one BFX84. Diodes  $D_1$ ,  $D_2$  and  $D_3$  are included to ensure that distortion in the crossover region—that is, at low output powers—is very low.

### Circuit Description

The voltage at the mid-point between the output transistors is set by means of the preset potentiometer  $R_1$  to give symmetrical clipping. Transistor  $TR_3$  provides bias for the output stage as well as thermal and voltage compensation. The quiescent current of the output stage is set to 35 to 40mA, or that of the whole power amplifier to 45 to 50mA, by means of  $R_9$ .

High-frequency stabilisation, necessitated by the high value of feedback, is effected by  $C_4$ ,  $C_5$ ,  $C_6$ ,  $C_9$ ,  $R_{14}$  and  $R_{23}$ .

### Power Supply

The power supply requirements are:

Total quiescent current for one channel only	45 to 50mA
Supply voltage	50V
Maximum supply voltage under quiescent conditions	60V
Total current taken from the supply for one channel only:	
for 25W output into $8\Omega$ load	0.8A
for 25W output into $4\Omega$ load	1.1A

For short-circuit protection, a 1.5A fuse is required in the supply to each channel.

The circuit for a simple power supply is shown in Fig. 75.

### Performance

Output power ( $8\Omega$ load, 50V supply)	25W r.m.s.
Sensitivity for 25W output	200mV
Frequency response ( $-3\text{dB}$ points)	10Hz to 30kHz
Input resistance	200k $\Omega$
Distortion at 25W output (see Fig. 76)	0.2%

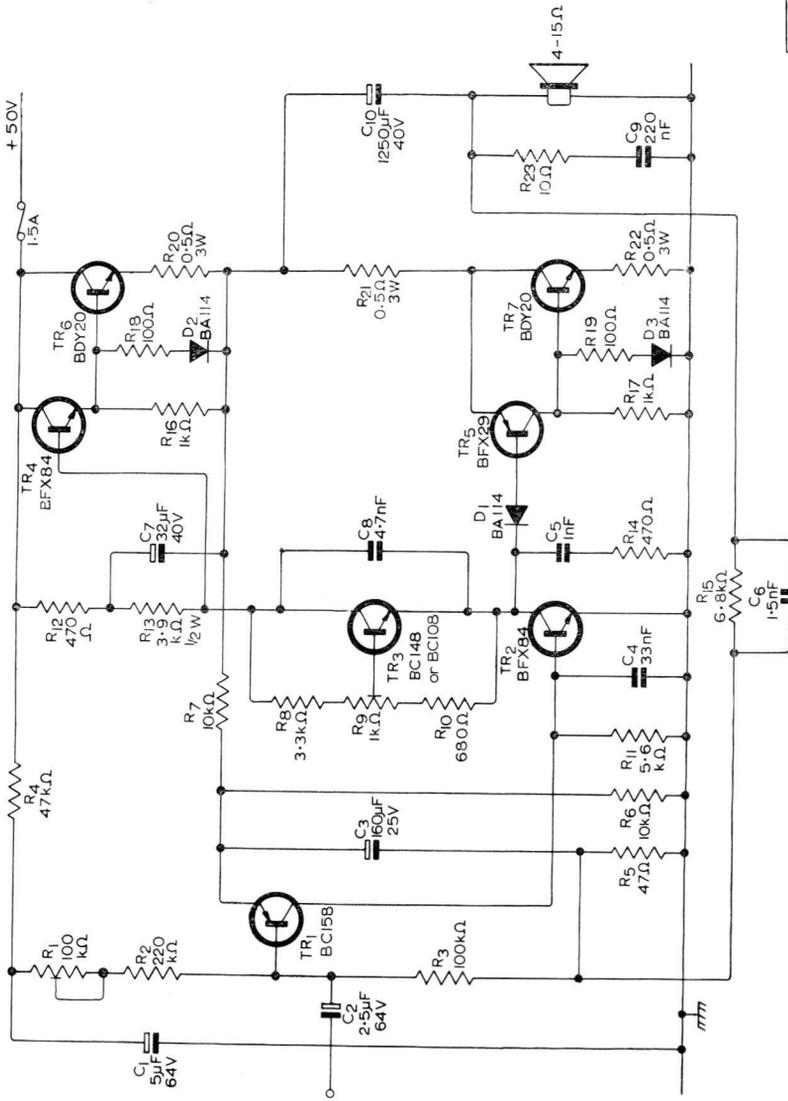


Fig. 74—25W high-quality audio amplifier circuit

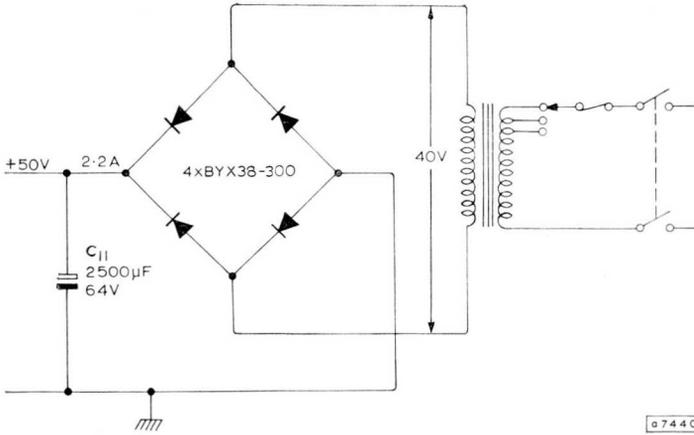


Fig. 75—Power supply circuit for 25W amplifier

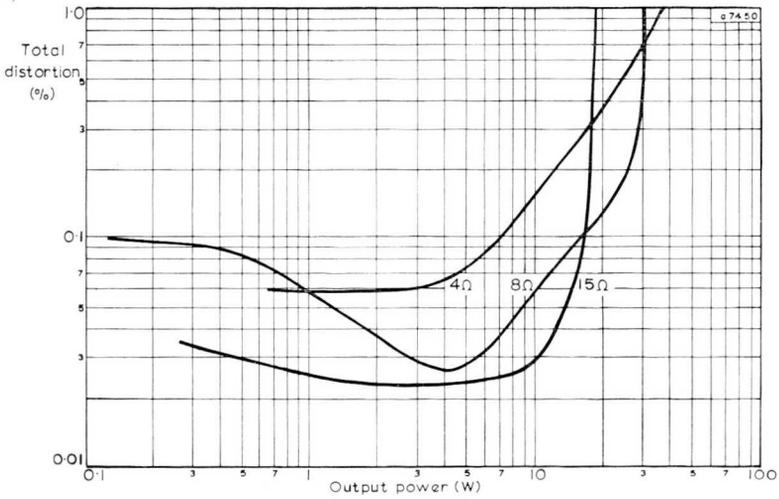
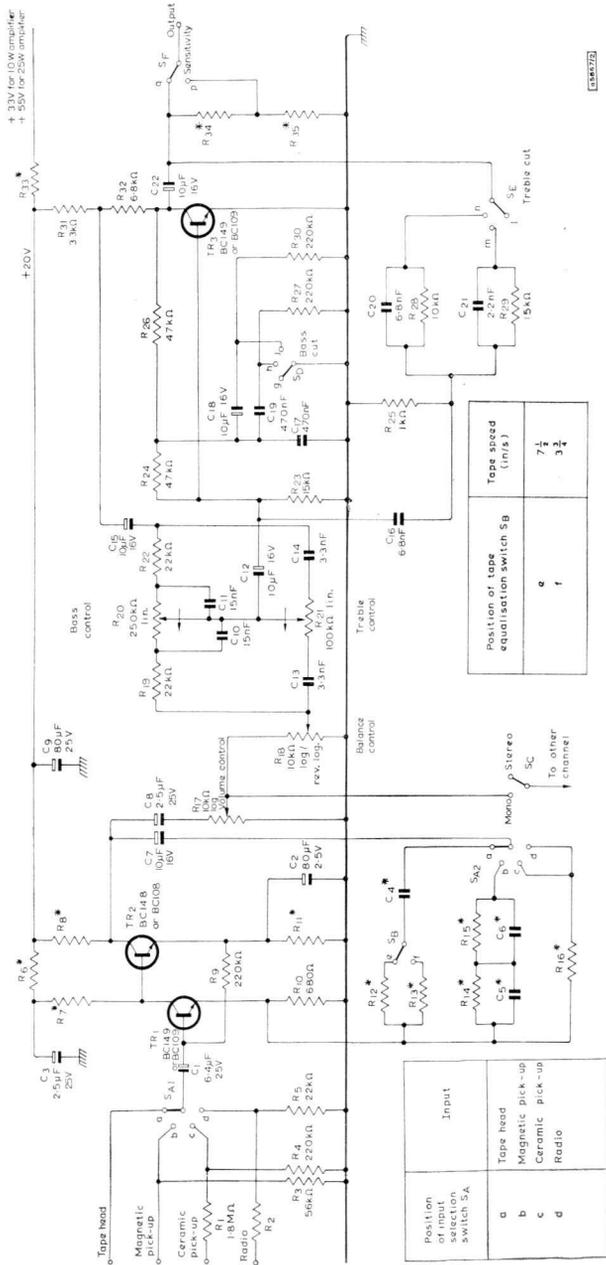


Fig. 76—Variation of total harmonic distortion with output power for three load impedances



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Fig. 77—Pre-amplifier circuit for use with 10W and 25W amplifiers  
\*The values of these components depend on the power amplifier to be used: see components list. Switch S<sub>F</sub> is omitted in a pre-amplifier to be used with a 10W amplifier

## PRE-AMPLIFIER FOR USE WITH THE 10W AND 25W AUDIO AMPLIFIERS

A pre-amplifier for use with the 10W and 25W audio amplifiers is shown in Fig. 77.

### Circuit Description

Transistors  $TR_1$  and  $TR_2$  form a directly coupled pair, the base voltage of  $TR_1$  being derived from the emitter of  $TR_2$ . Equalisation for tape head, magnetic pick-up, ceramic pick-up and radio inputs is obtained by feedback from the collector of  $TR_2$  to the emitter of  $TR_1$ . The equalisation characteristics are shown in Figs. 78 and 79.

No value is given for  $R_2$ , the input resistor for the radio position, because this must be chosen to suit the available signal. The sensitivity at the base of  $TR_1$  is 7.5mV for 200mV output.

Transistor  $TR_3$  is used in a feedback tone control circuit which gives a voltage gain of three times. A circuit with linear potentiometers has been used because more boost can be obtained, and also because of the difficulty in obtaining and matching reverse-logarithmic potentiometers. A BC149 or BC109 is used because a low-noise device is required in the first stage after the volume control. The tone control characteristics are shown in Fig. 80.

The working point of  $TR_3$  is fixed by  $R_{23}$ ,  $R_{24}$  and  $R_{26}$ , a.c. feedback being removed by decoupling capacitors,  $C_{17}$ ,  $C_{18}$  or  $C_{19}$ . By switching these capacitors, bass cut is obtained, and the effect on the pre-amplifier and 25W power amplifier combined is shown in Fig. 81. Networks can also be switched in by  $S_E$  to give treble cut as shown in Fig. 82.

Resistors  $R_{34}$ ,  $R_{35}$  and Switch  $S_F$  are required in the pre-amplifier for use with the 25W amplifier only. When a high-sensitivity speaker is used with the 25W circuit in quiet listening conditions, the noise originating in  $TR_3$  is perceptible even when a low-noise transistor is used. Since the full sensitivity will not be required under these conditions, a switched attenuator is used at the output of the pre-amplifier, reducing the sensitivity and noise by 12dB.

### Performance

Sensitivity at 1kHz for 200mV (25W version) or  
400mV (10W version) output:

ceramic pick-up	170mV
magnetic pick-up	4mV
tape head with tape speed of $7\frac{1}{2}$ in/s	6.5mV
Total distortion for 200mV output with volume control at maximum	< 0.02%

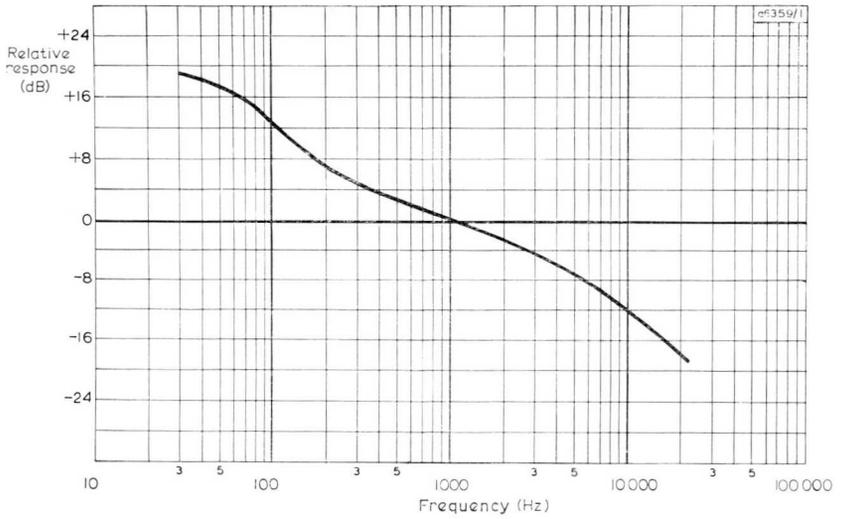


Fig. 78—Equalisation of pre-amplifier with magnetic pick-up input

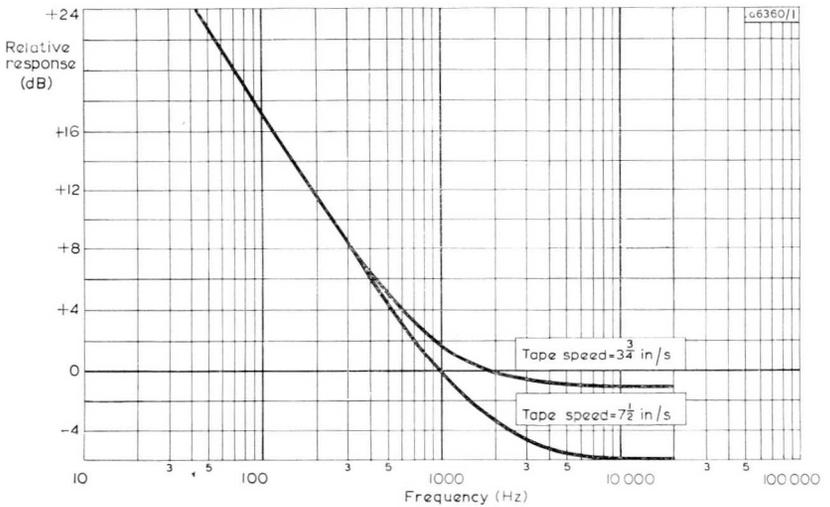


Fig. 79—Equalisation of pre-amplifier with tape head input

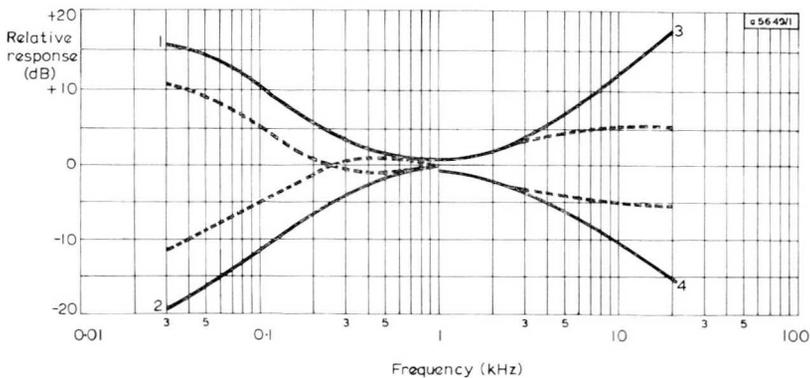


Fig. 80—Tone control characteristics of pre-amplifier

Curve 1: maximum bass boost, treble flat

Curve 2: maximum bass cut, treble flat

Curve 3: maximum treble boost, bass flat

Curve 4: maximum treble cut; bass flat

The dotted curves represent intermediate positions of the controls

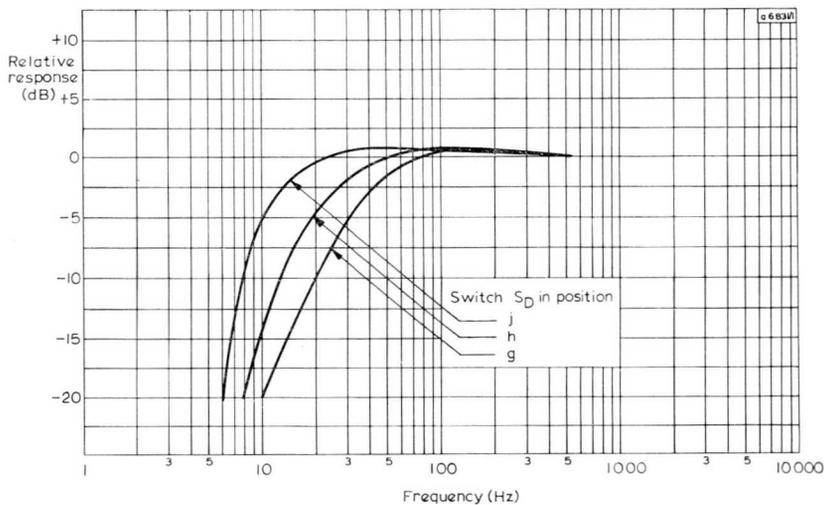


Fig. 81—Low-frequency response of pre-amplifier and 25W amplifier

**Performance (continued)**

Total distortion with volume control at minimum,  
measured at the volume control

see Fig. 83

Signal-to-noise ratio for 200mV output, for all inputs > 60dB

Total current:

25W version

2mA

10W version

3mA

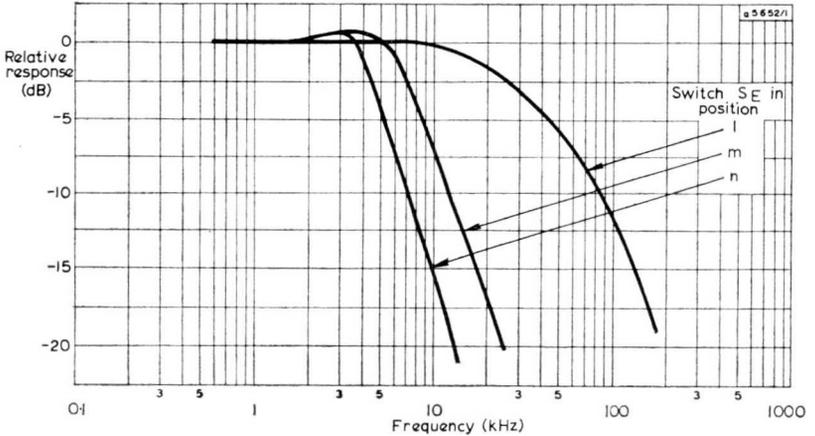


Fig. 82—High-frequency response of pre-amplifier and 25W amplifier

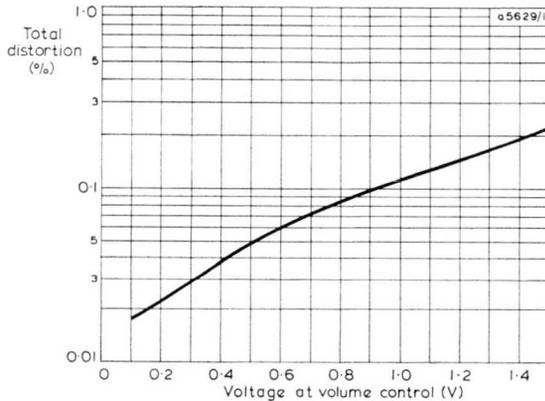


Fig. 83—Total pre-amplifier distortion (measured at the volume control) plotted against the voltage at the volume control

## LAYOUT OF HIGH-QUALITY AUDIO CIRCUITRY

The circuits described in this chapter are capable of high-quality reproduction, but only if they are carefully laid out and constructed. The relative positions of input, output and power supply, and the earthing and screening arrangements are of particular importance, and it is suggested that layouts should be designed with reference to the code of good practice outlined here.

### General Layout

It should be remembered that the input sensitivity of an amplifier is typically 3mV at 1kHz, on the magnetic pick-up position, and the output voltage is of the order of 20V, implying a voltage gain approaching  $10^4$ . It is therefore essential to keep the output separated and screened from the input. The magnetic field from the mains transformer may cause hum, so the transformer should be as remote as possible from the input (this is dealt with more fully below).

### Earthing

Currents of several amps magnitude circulate in the power supply and output stages. It is important that no wiring carrying these currents is included in the input circuit, otherwise hum or instability, due to the small but significant resistance of the wires, will result. The paths of currents in the output stage and power supply are shown in Fig. 84.

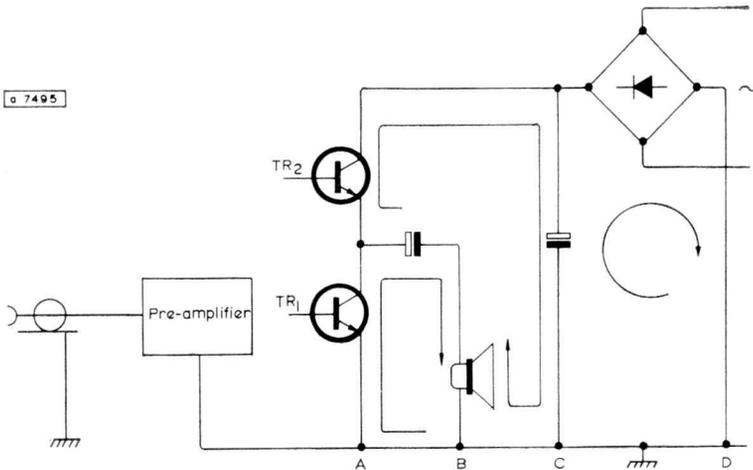


Fig. 84—Current paths in power supply and output stage

Between points A and B there is a voltage due to  $TR_1$ ; between B and C a voltage due to  $TR_2$ ; and between C and D a voltage due to the power supply. The input can be earthed at A, but not at B, C, or D. In practice it is usual to combine A, B, C and D in one common earthing point.

The earthing arrangement for stereo amplifiers is considerably more complex than for mono, since the single power supply and common earth for the two signal inputs make it more difficult to avoid earth loops. The arrangement recommended for the 25W amplifier is shown in Fig. 85.

Point E is the common earthing point. The voltage across the wire AE is effectively in series with the input to the power amplifier. This does not cause any trouble provided the wire is short, because the sensitivity at the input of the power amplifier is 200mV and the output-stage current is taken to the earth point separately.

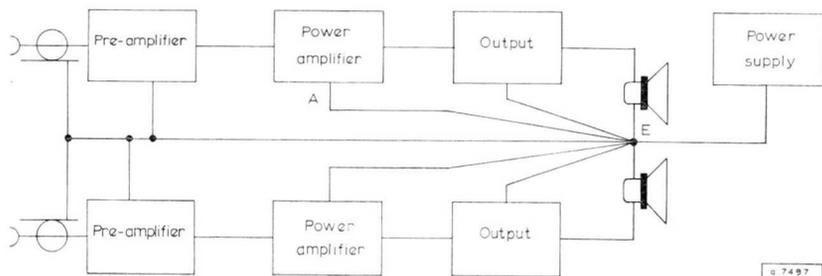


Fig. 85—Earthing arrangement for a stereo amplifier

### Magnetic Fields

The principal source of magnetic fields in an amplifier is the mains transformer. Hum due to this cause will be at a frequency of 150Hz because the hysteresis of the core results in the magnetic field being predominantly third harmonic. The magnetic field will induce a voltage in any circuit loop.

The input loop of a pre-amplifier is shown in Fig. 86. The area of this loop should be minimised, and it may also be necessary to screen the mains transformer by making the parts of the chassis surrounding it from mild steel rather than aluminium.

The magnetic field associated with the currents in the output stage may occasionally cause trouble. Again, the remedy is to minimise the area of the circuit loops in the output stage by, for example, running emitter and collector leads close together, in order to minimise radiation.

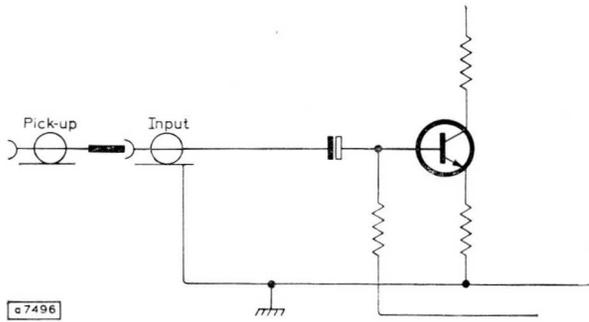


Fig. 86—Input loop of a pre-amplifier

### Hum

There are many possible causes of hum and only the more probable are indicated here. A clue to the cause of the hum may often be obtained by determining its frequency.

50Hz hum may be due to stray pick-up caused by poor screening, earth loops or television break-through. The last is recognisable by the distinctive buzz of the field sync pulses, and also by the fact that it is usually accompanied by the sound channel.

100Hz hum originates in the power supply and is often indicative of poor decoupling in the h.t. line or incorrect connection of the earth leads (see Page 114).

150Hz hum comes from the magnetic field of the transformer and has already been discussed.

### Resistor Noise

Every resistor has inherent thermal noise which could only be eliminated by refrigerating the component. However, certain resistors, notably carbon composition types, give an excess noise which is proportional to the voltage across them. Although this excess noise does not usually contribute significantly to the noise in the transistor circuit it is advisable to use high-stability resistors for the collector load and base bias resistors of the input stage.

## AUXILIARY HIGH-QUALITY CIRCUITS

In the design of the auxiliary a.f. amplifiers, control circuits and filters which follow, use has been made of the technique, common in audio engineering, of having a high input impedance and a low output impedance. All the circuits can therefore be connected together irrespective of impedance. This means that a uniform supply voltage is necessary for all the circuits, and a value of 18V has been chosen. The supply voltage can vary by  $\pm 15\%$  without any appreciable change in the performance of the circuits.

## AUXILIARY HIGH-QUALITY AMPLIFIERS

The auxiliary amplifiers described in this section are derived from the basic voltage amplifier shown in Fig. 87. To achieve stabilisation against temperature variations, two d.c. feedback loops are used: one from the emitter of the second transistor to the base of the first, and the other from the collector of the second transistor to the emitter of the first. The values of the components for circuits with voltage gains  $A_v$  of 10, 20, 30 and 40dB are shown in Table 2. The voltages in the circuit, and the input and output impedance values  $Z_{in}$  and  $Z_{out}$ , are shown in Table 3.

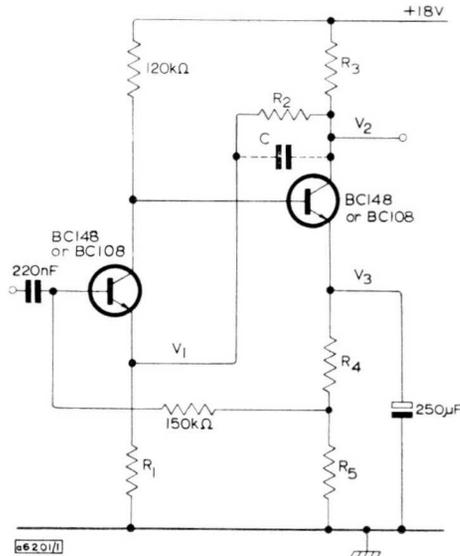


Fig. 87—Simple audio amplifier circuit.  
Component values are given in Table 2

**TABLE 2**  
**Component Values**

Circuit reference	$A_v = 10\text{dB}$	$A_v = 20\text{dB}$	$A_v = 30\text{dB}$	$A_v = 40\text{dB}$
R <sub>1</sub>	4.7k $\Omega$	1.5k $\Omega$	1.5k $\Omega$	1k $\Omega$
R <sub>2</sub>	12k $\Omega$	15k $\Omega$	56k $\Omega$	180k $\Omega$
R <sub>3</sub>	1.8k $\Omega$	2.2k $\Omega$	2.2k $\Omega$	2.2k $\Omega$
R <sub>4</sub>	470 $\Omega$	560 $\Omega$	330 $\Omega$	680 $\Omega$
R <sub>5</sub>	1.2k $\Omega$	470 $\Omega$	270 $\Omega$	220 $\Omega$
C	—	—	—	10pF

**TABLE 3**  
**Voltages and Impedances**

Voltage or impedance	$A_v = 10\text{dB}$	$A_v = 20\text{dB}$	$A_v = 30\text{dB}$	$A_v = 40\text{dB}$
V <sub>1</sub>	3.4V	0.97V	0.4V	0.15V
V <sub>2</sub>	10.8V	9.3V	9.3V	9.7 V
V <sub>3</sub>	5.6V	3.55V	2.3V	3.4V
Z <sub>in</sub>	145k $\Omega$	140k $\Omega$	135k $\Omega$	110k $\Omega$
Z <sub>out</sub>	63 $\Omega$	140 $\Omega$	260 $\Omega$	700 $\Omega$

Figs. 88 to 91 show for the four circuits the total distortion as a function of the output voltage at three frequencies, and the noise voltage at the output as a function of the generator resistance at the input. The total distortion for all four amplifiers remains below 0.1% for output voltages up to 1V at 1kHz, and below 1% for output voltages up to 3V. The noise voltage referred to the input in all four amplifiers is less than 1 $\mu$ V. The frequency response (-3dB points) of all amplifiers is from 20Hz to 20kHz.

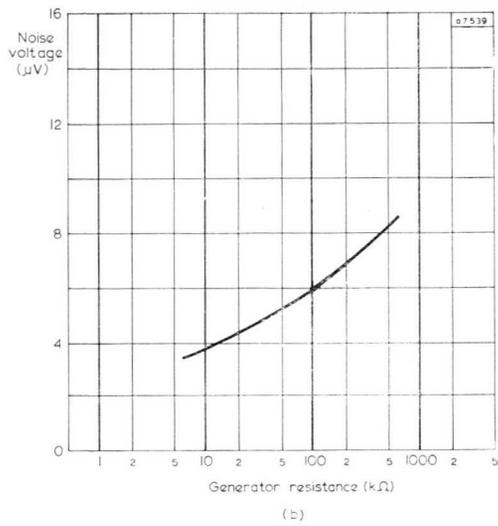
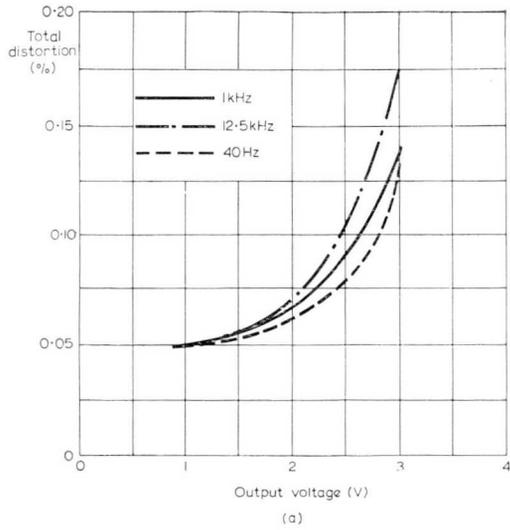


Fig. 88—Total distortion and noise voltage at output of 10dB amplifier

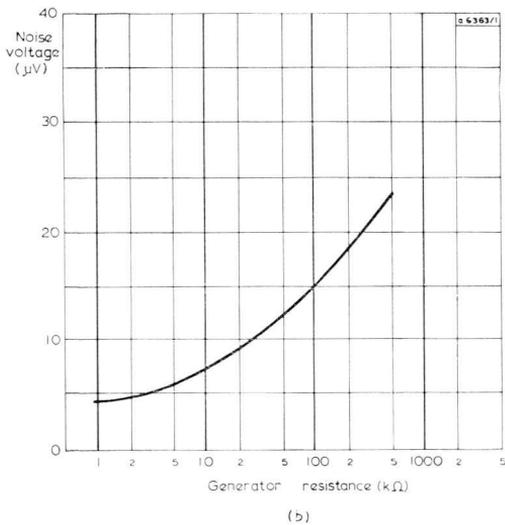
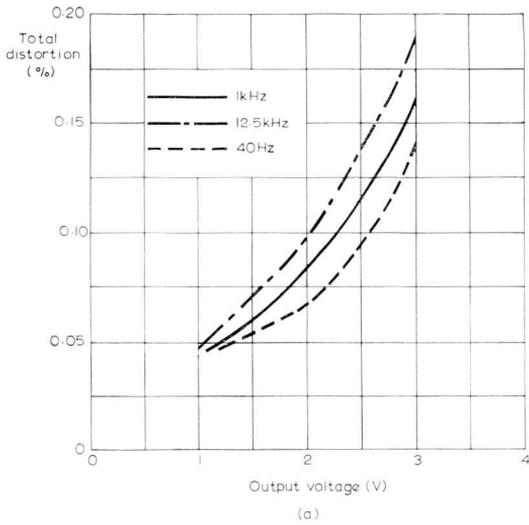


Fig. 89—Total distortion and noise voltage at output of 20dB amplifier

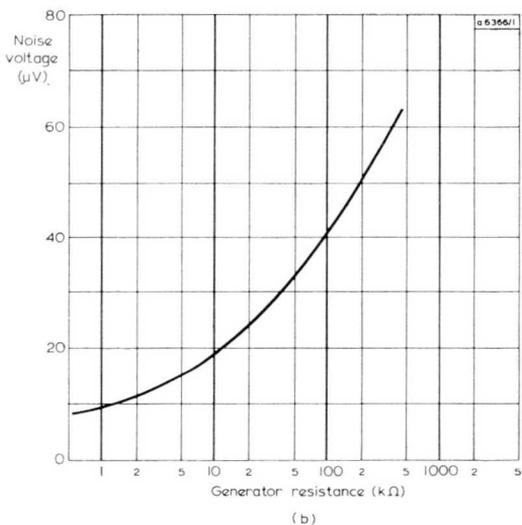
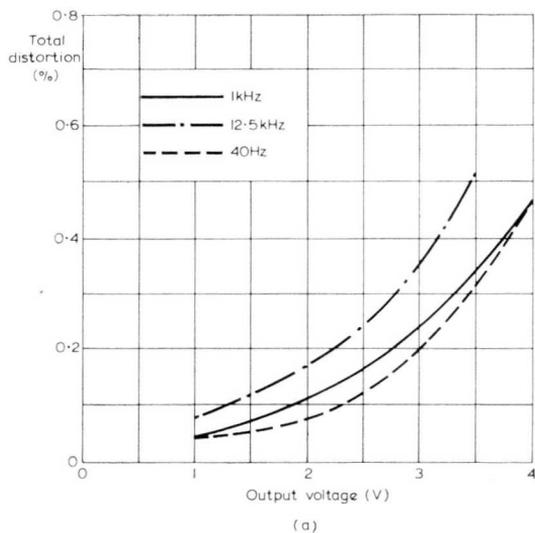


Fig. 90—Total distortion and noise voltage at output of 30dB amplifier

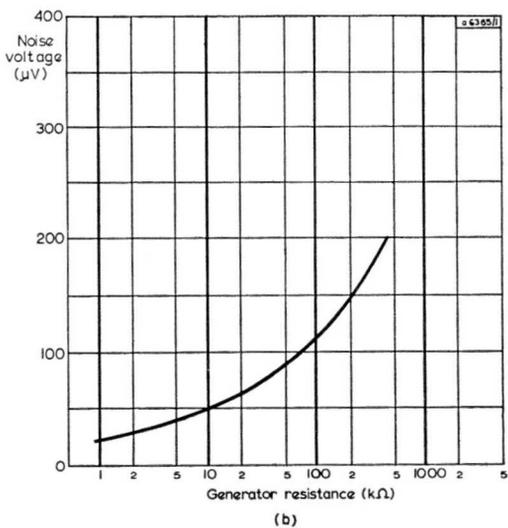
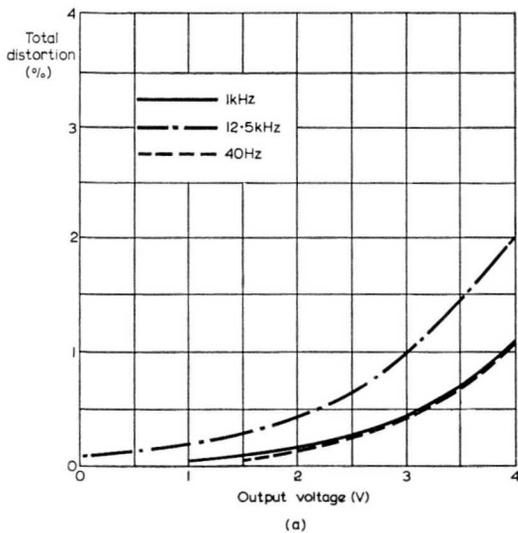


Fig. 91—Total distortion and noise voltage at output of 40dB amplifier

## Buffer Amplifier

The circuit of a two-stage buffer amplifier is shown in Fig. 92. The first stage works in the common-emitter configuration with a large amount of feedback, while the second stage is an emitter follower. This ensures a high input impedance of  $3.6\text{M}\Omega$ , and a low output impedance of  $250\Omega$ . The voltage gain is unity, and the frequency response ( $-3\text{dB}$  points) is from  $20\text{Hz}$  to  $20\text{kHz}$ . Fig. 93 shows the total distortion and the noise voltage at the output. The distortion remains below  $0.5\%$  with output voltages up to  $2.5\text{V}$ .

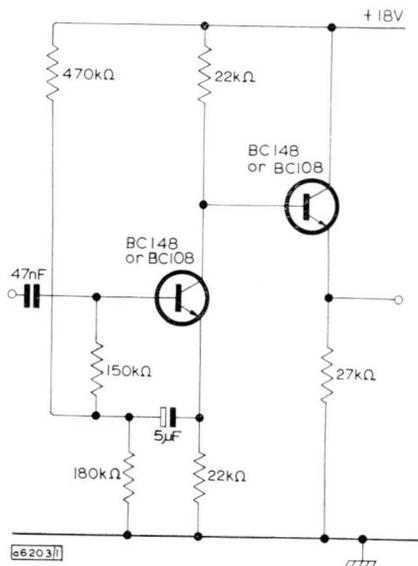


Fig. 92—Buffer amplifier circuit

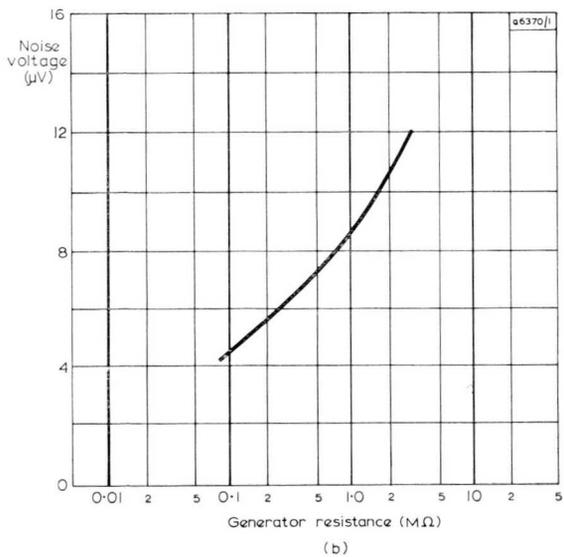
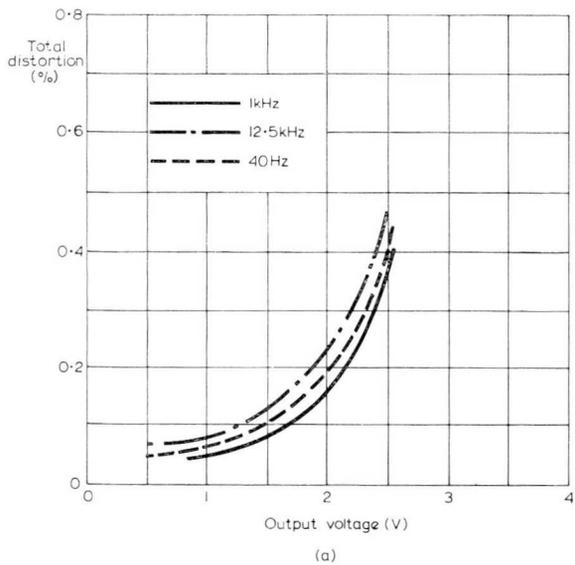


Fig. 93—Total distortion and noise voltage at output of buffer amplifier

## Microphone Amplifier

The circuit of a microphone amplifier with a voltage gain adjustable between 13 and 40dB by varying the feedback is shown in Fig. 94. The total distortion for the limiting values of the voltage gain is shown in Fig. 95. With an output voltage of 2V, the distortion is 0.75% for a gain of 40dB, and 0.15% for a gain of 13dB. The values of noise voltage correspond to those of the 10dB and 40dB amplifiers of Fig. 87. The input and output impedances, and the frequency response (-3dB points) are shown in Table 4.

**TABLE 4**  
**Impedances and Frequency Response**

Impedance or frequency	$A_v = 13\text{dB}$	$A_v = 40\text{dB}$
$Z_{in}$	145k $\Omega$	120k $\Omega$
$Z_{out}$	47 $\Omega$	120 $\Omega$
$f_{lower}$	< 20Hz	< 20Hz
$f_{upper}$	$\geq 20\text{kHz}$	$\geq 20\text{kHz}$

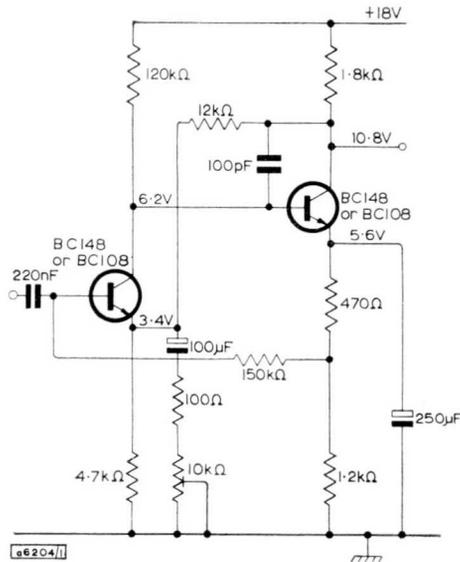


Fig. 94—Microphone amplifier circuit

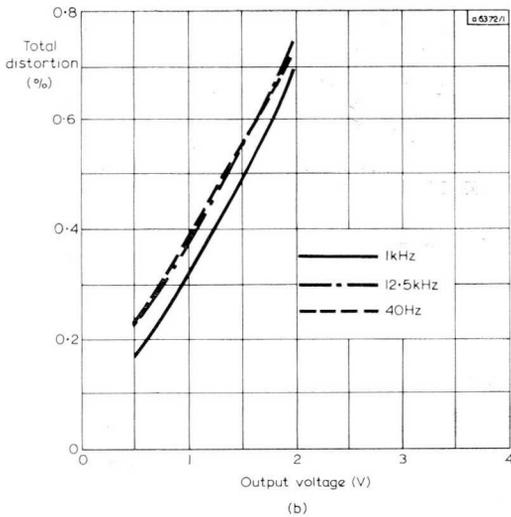
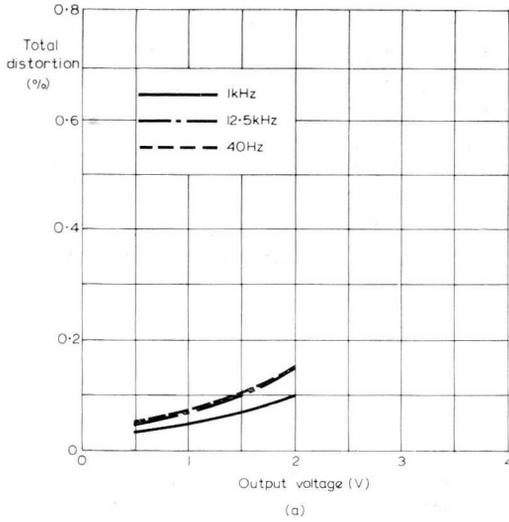


Fig. 95—Total distortion of microphone amplifier with voltage gain of (a) 13dB and (b) 40dB

### Mixer Amplifier

Fig. 96 shows the circuit of a mixer amplifier, with two inputs feeding two transistors with a common collector load resistor. An emitter follower stage ensures a low output impedance of  $70\Omega$ , and the input impedance is  $2.5M\Omega$ . For both inputs, the voltage gain is unity.

Fig. 97 shows the total distortion of the mixer amplifier with a signal on one input and the other input short-circuited. The distortion is  $0.5\%$  for an output voltage of  $2V$ , and falls to  $0.1\%$  for outputs less than  $0.5V$ . For distortion of  $0.5\%$ , the voltage of each input must not exceed  $1V$ , otherwise with full modulation of both inputs there will be overloading.

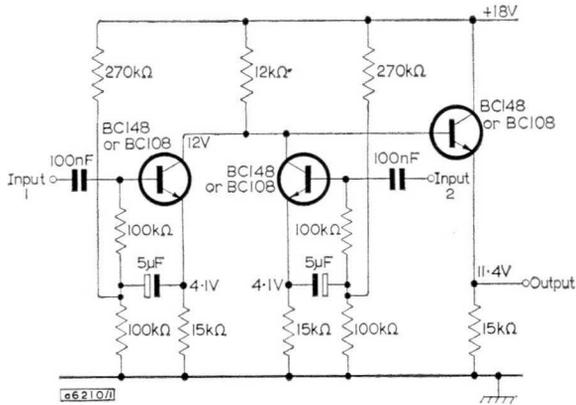


Fig. 96—Mixer amplifier circuit with two inputs

### Amplifier with High Voltage Output

The circuit of an amplifier with a voltage gain of  $20dB$  and designed for a maximum output voltage of  $10V$  is shown in Fig. 98. To achieve this high output voltage, it is necessary for the supply voltage to be  $45V$  instead of the standard  $18V$ . The total distortion at  $1kHz$  and maximum output voltage is  $0.11\%$  (Fig. 99). The frequency response ( $-3dB$  points) is from  $20Hz$  to  $20kHz$ , and the input and output impedances are  $140k\Omega$  and  $200\Omega$  respectively.

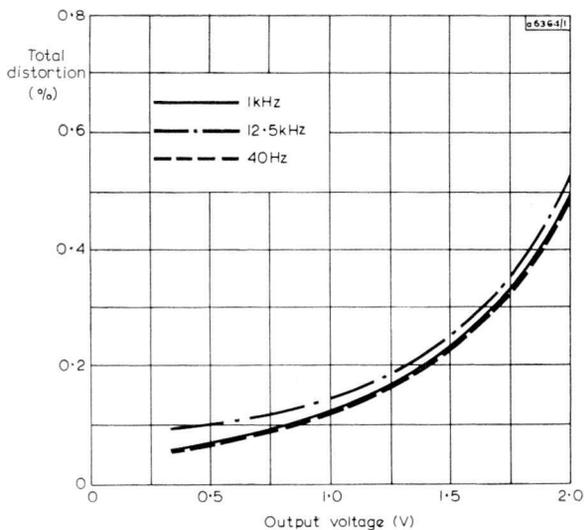


Fig. 97—Total distortion of mixer amplifier

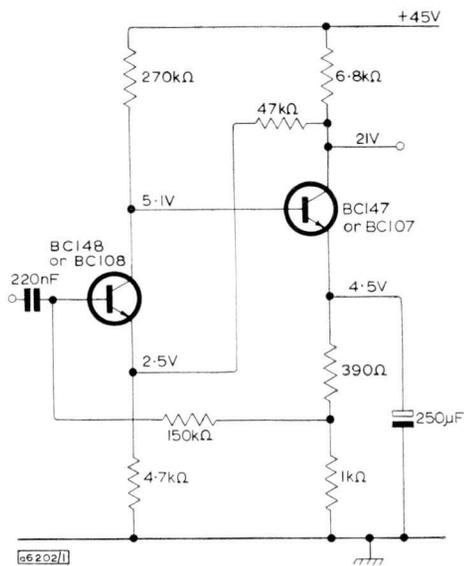


Fig. 98—Amplifier with high voltage output

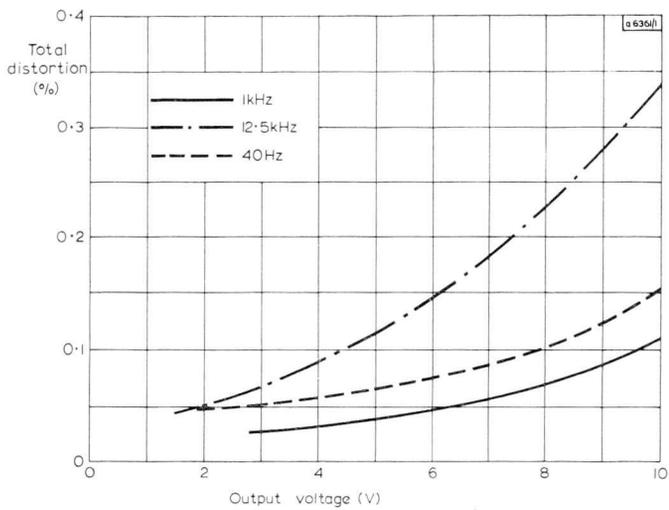


Fig. 99—Total distortion of amplifier shown in Fig. 98

# AUXILIARY HIGH-QUALITY CONTROL CIRCUITS

## Balance Control

The balance control of Fig. 100 makes it possible in stereophonic systems to vary the voltage gain in both channels by 6dB in opposite directions. The controlling variable resistor is inserted in the feedback circuit. The average gain is 23.4dB, and Fig. 101 shows the total distortion for minimum and maximum gain. The differences are slight because of the large amount of feedback applied. The noise voltage corresponds to that of the 20dB amplifier of Fig. 87. The frequency response (-3dB points) is from 20Hz to 20kHz, while the input and output impedances are 140kΩ and 85Ω respectively.

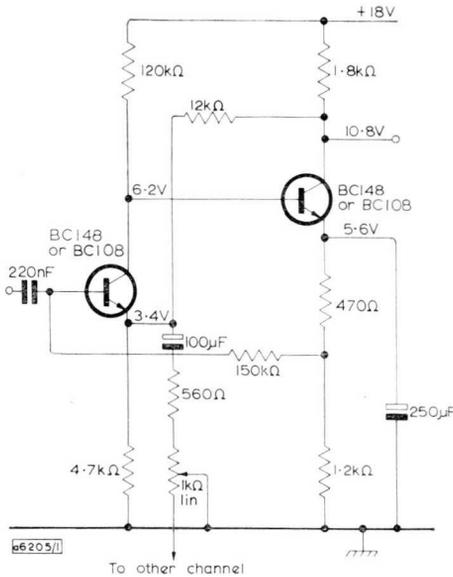


Fig. 100—Balance control circuit (only one channel shown)

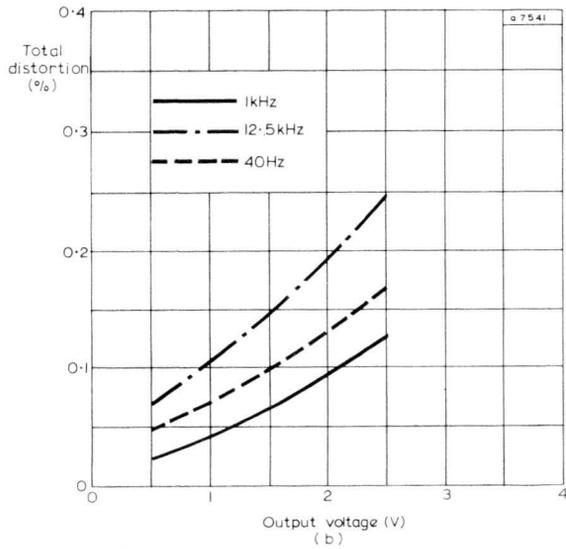
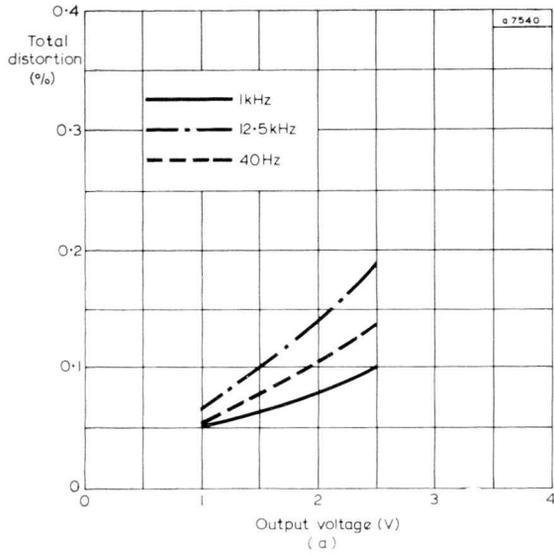


Fig. 101—Total distortion of balance control for (a) minimum and (b) maximum gain

### Active Tone Control

The active tone control circuit of Fig. 102, unlike the well-known frequency-dependent voltage-divider circuits, operates with a frequency-dependent feedback network between the collector and base of the transistor. The tone control characteristics are shown in Fig. 103. The range of control extends from  $-22$  to  $+19.5$  dB at 30Hz, and from  $-19$  to  $+19.5$  dB at 20kHz. The flat frequency response is obtained when the variable resistors are in the physically central position. The voltage gain is then 0.91. Fig. 104 shows the total distortion as a function of output voltage for frequencies of 40Hz, 1kHz, and 12.5kHz, measured with the controls in the flat position. For small input voltages (less than 250mV), the total distortion remains below 0.1%, and for an output voltage of 2V it rises to 0.85% at 12.5kHz. The input and output impedances at 1kHz are 40k $\Omega$  and 180 $\Omega$  respectively.

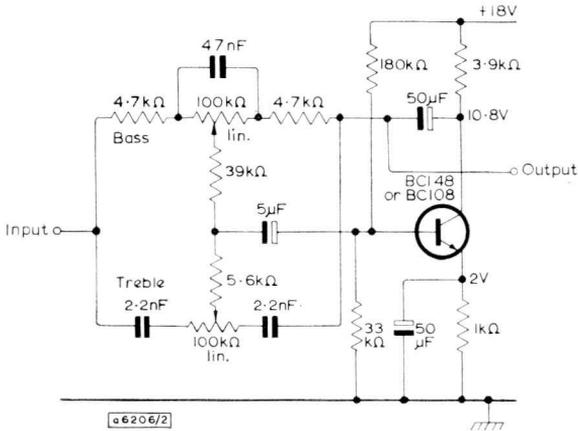


Fig. 102—Active tone control circuit

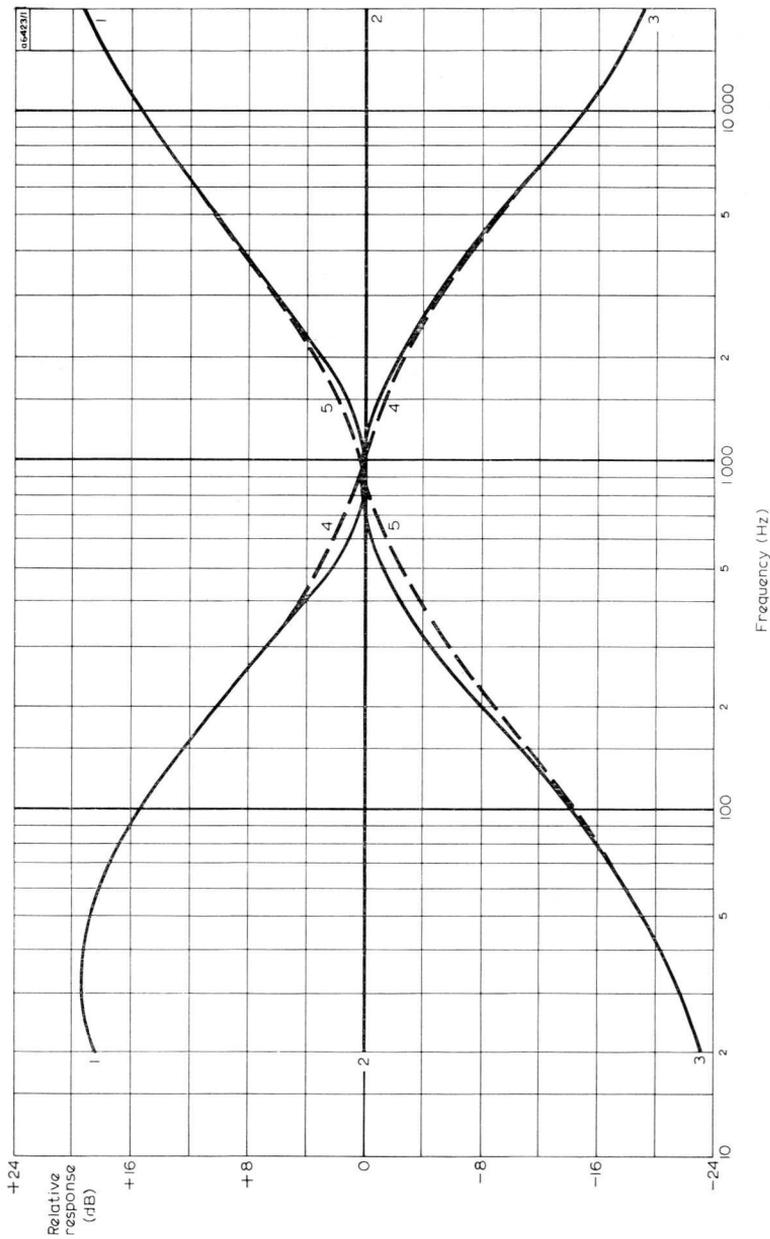


Fig. 103—Characteristics of active tone control circuit

Curve 1: maximum bass boost, maximum treble boost    Curve 2: linear frequency response (controls flat)  
 Curve 3: maximum bass cut, maximum treble cut    Curve 4: maximum bass boost, maximum treble cut  
 Curve 5: maximum bass cut, maximum treble boost

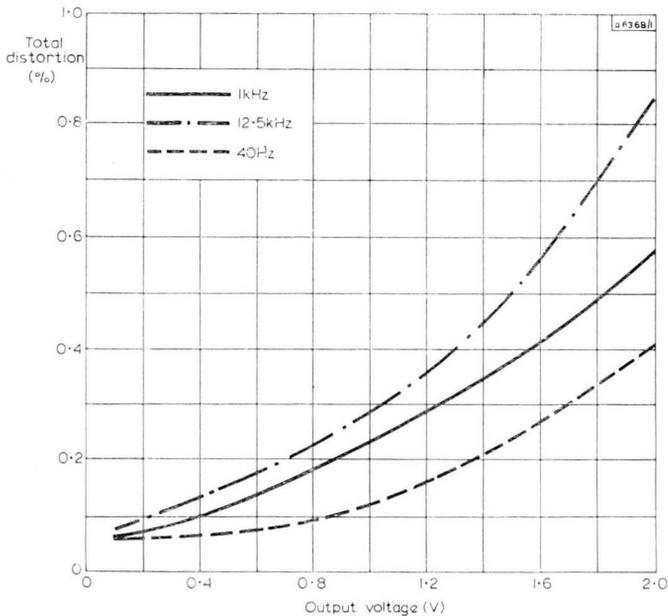


Fig. 104—Total distortion of active tone control

### Sound Source Width Control

Fig. 105 shows a circuit by which the width of the sound source in a stereophonic system can be varied continuously. For this, part of the signal voltage of one channel is added to the second channel. The width control can be adjusted continuously between in-phase crosstalk of 100% (corresponding to mono operation) and anti-phase crosstalk of 24%. Greater anti-phase crosstalk is not necessary since the sound impression will 'fall apart' for greater values. A 5k $\Omega$  preset potentiometer is used to balance the two channels. The voltage gain of the circuit is 0.5. Input and output impedances are 750k $\Omega$  and 47 $\Omega$  respectively, and the frequency response (-3dB points) is from 20Hz to 20kHz.

Fig. 106 shows the total distortion of the circuit as a function of output voltage for three frequencies.

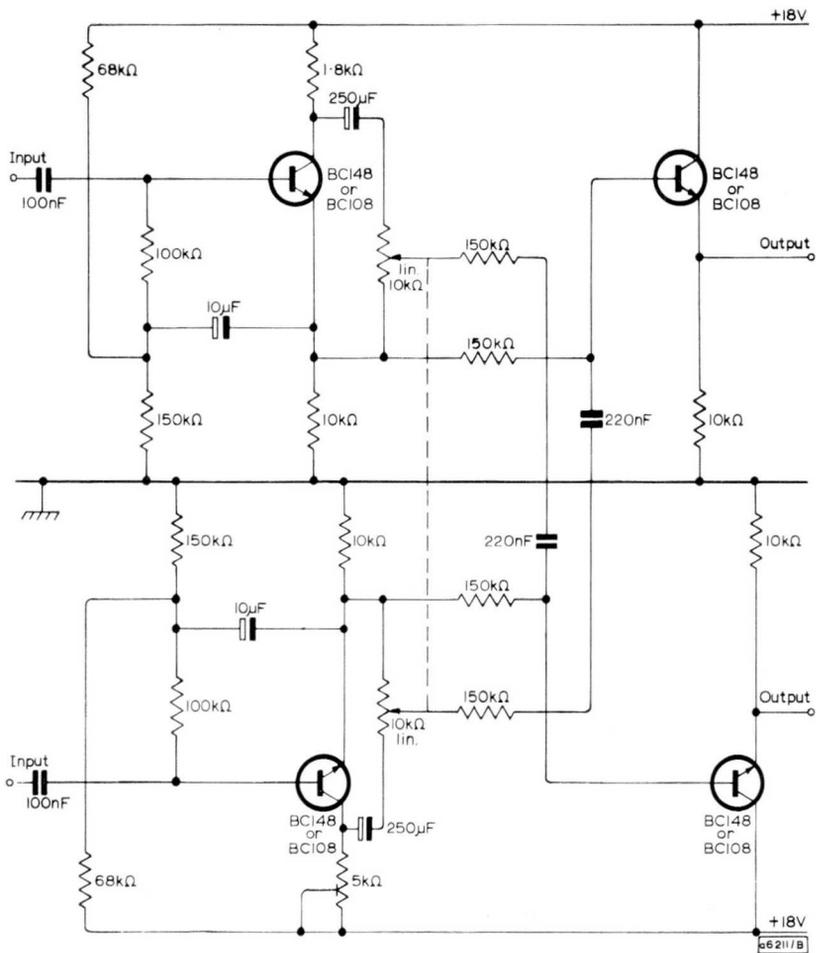


Fig. 105—Sound source width control circuit

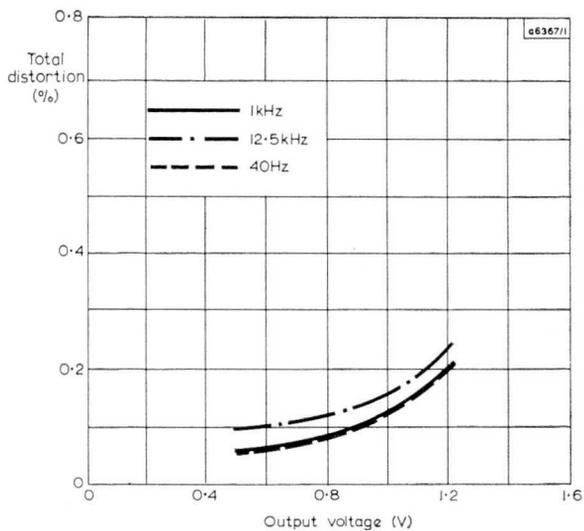


Fig. 106—Total distortion of sound source width control.

## AUXILIARY HIGH-QUALITY FILTERS

### Low-pass/High-pass Filter

The circuit of a low-pass/high-pass filter is shown in Fig. 107. It consists of two RC networks connected in series with a buffer amplifier, the circuit of which is given in Fig. 92. The adjustable frequency characteristics are shown in Fig. 108. The following frequency limits can be selected:

lower frequency 40, 80, 160, and 270Hz;

upper frequency 11, 9, 4.5, and 3.2kHz.

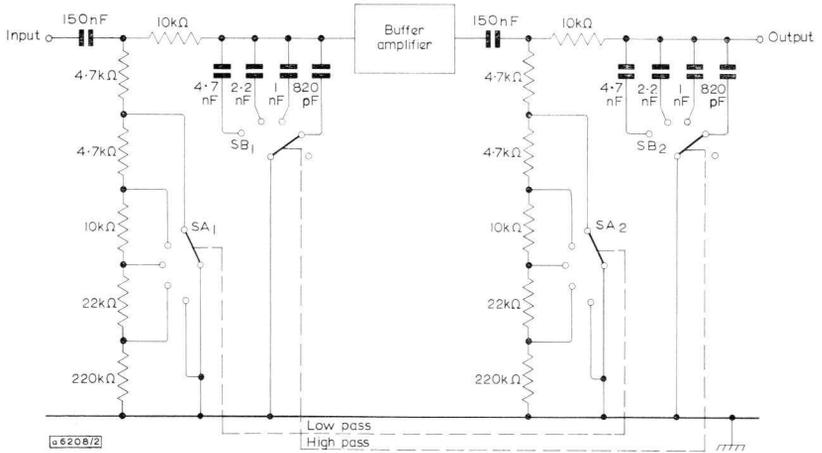


Fig. 107—Low-pass/high-pass filter circuit

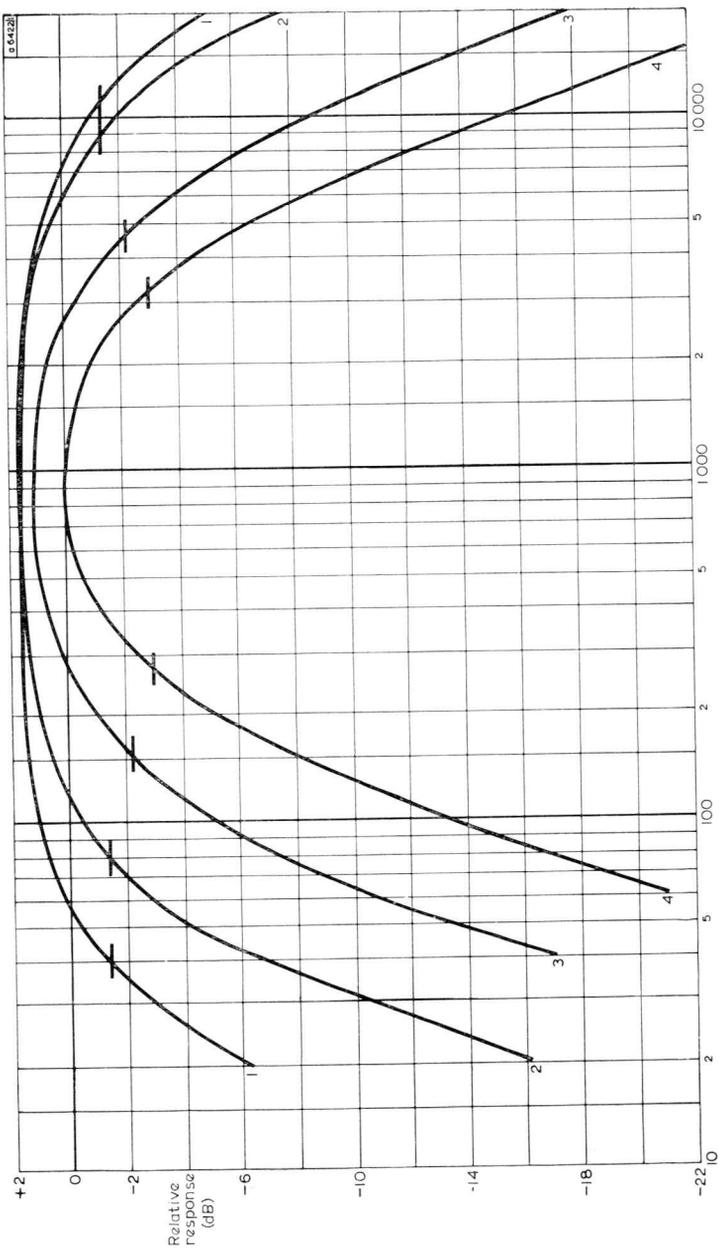


Fig. 108—Frequency characteristics of low-pass/high-pass filter

Curve 1:  $f_{c1} = 40\text{Hz}$ ,  $f_{c2} = 11\text{kHz}$

Curve 2:  $f_{c1} = 80\text{Hz}$ ,  $f_{c2} = 9\text{kHz}$

Curve 3:  $f_{c1} = 160\text{Hz}$ ,  $f_{c2} = 4.5\text{kHz}$

Curve 4:  $f_{c1} = 270\text{Hz}$ ,  $f_{c2} = 3.2\text{kHz}$

( $f_{c1}$  = lower cut-off frequency;  $f_{c2}$  = upper cut-off frequency)

## Noise and Rumble Filter

The circuit of a noise and rumble filter is shown in Fig. 109. Bass and treble cut are produced by an RC network connected between two emitter followers, and a feedback loop from the output to the input through a second RC network. In this way, a high slope of about 13dB per octave is achieved. The frequency limit of the rumble filter is fixed at 45Hz, and the noise filter can be switched to limits of 16, 12, and 7kHz. The resulting frequency characteristics are shown in Fig. 110. The voltage gain is 0.95, and the total distortion at 1kHz and an output voltage of 2V is 0.35%, falling to less than 0.1% at 1V. The input and output impedances are 1.7M $\Omega$  and 450 $\Omega$  respectively.

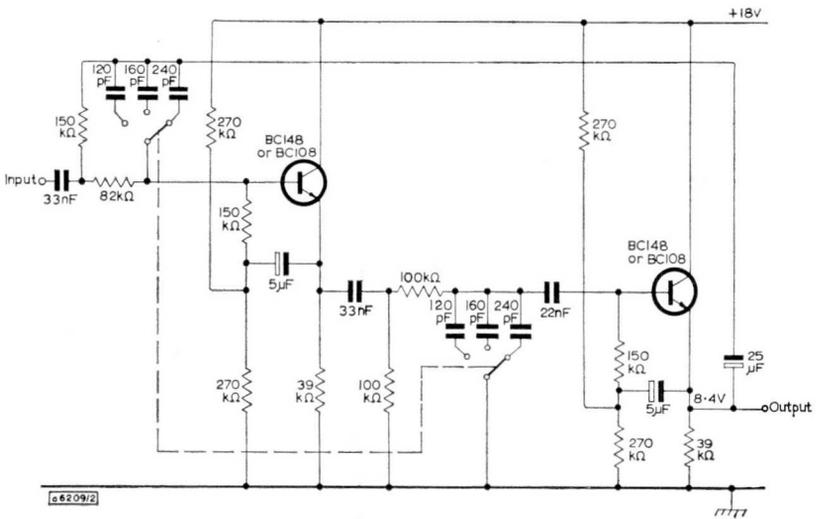


Fig. 109—Noise and rumble filter circuit

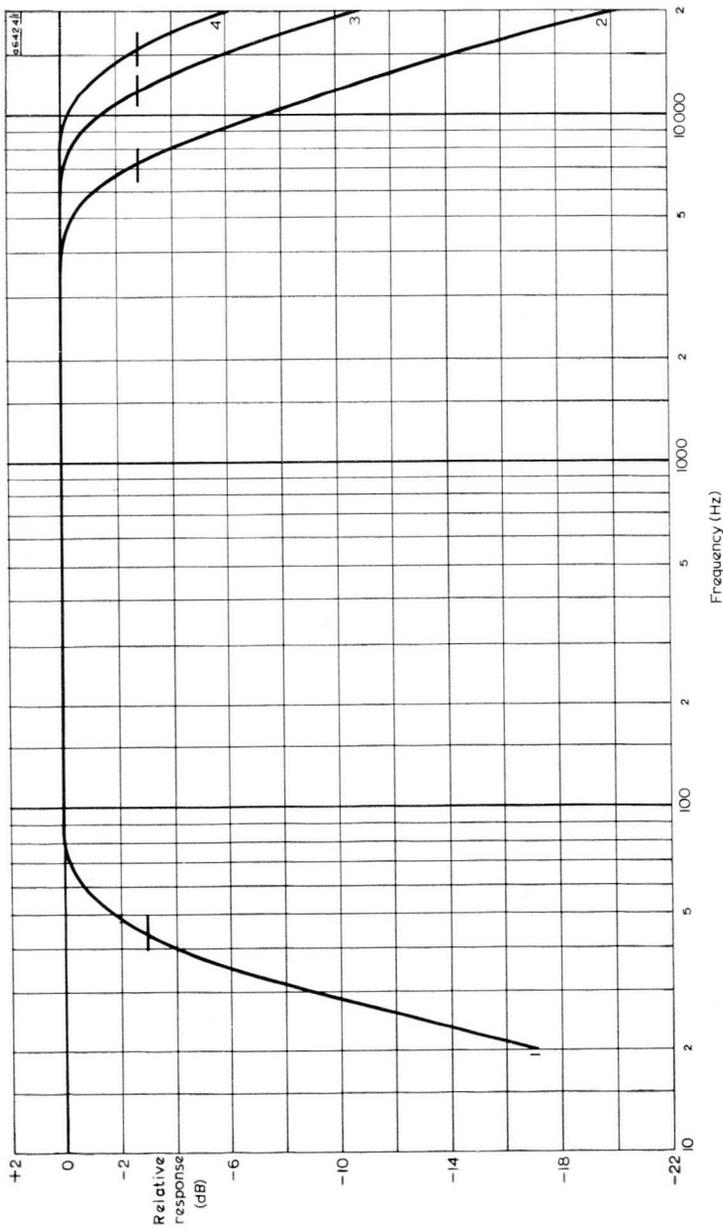


Fig. 110—Frequency characteristics of noise and rumble filter  
 For all curves  $f_{c1} = 45\text{Hz}$   
 Curve 2:  $f_{c2} = 7\text{kHz}$   
 Curve 3:  $f_{c2} = 12\text{kHz}$   
 Curve 4:  $f_{c2} = 16\text{kHz}$

## COMPONENTS FOR CIRCUITS IN CHAPTER 7

### 10W Audio Amplifier (page 102)

#### Transistors and Rectifier

Circuit reference	Mullard type	Circuit reference	Mullard type
TR <sub>1</sub>	BC158	TR <sub>4</sub>	BD131
TR <sub>2</sub>	BC148 or BC108	TR <sub>5</sub>	BD132
TR <sub>3</sub>	BD131	Full-wave bridge rectifier BY164	

#### Resistors

Tolerance:  $\pm 10\%$  except R<sub>2</sub> and R<sub>3</sub>, which should be  $\pm 5\%$  components  
 Power rating:  $\frac{1}{3}$ W except R<sub>10</sub>, which should be a 2W component, R<sub>11</sub>, R<sub>13</sub> and R<sub>14</sub>, which should be 1W components

Circuit reference	Value	Circuit reference	Value
R <sub>1</sub> preset potentiometer	50k $\Omega$	R <sub>9</sub> preset potentiometer	100 $\Omega$
R <sub>2</sub>	120k $\Omega$	R <sub>10</sub>	82 $\Omega$
R <sub>3</sub>	100k $\Omega$	R <sub>11</sub>	82 $\Omega$
R <sub>4</sub>	22 $\Omega$	R <sub>12</sub>	10 $\Omega$
R <sub>5</sub>	10k $\Omega$	R <sub>13</sub>	0.5 $\Omega$
R <sub>6</sub>	470 $\Omega$	R <sub>14</sub>	0.5 $\Omega$
R <sub>7</sub>	470 $\Omega$	R <sub>15</sub>	10 $\Omega$
R <sub>8</sub>	47 $\Omega$		

Resistors R<sub>2</sub>, R<sub>3</sub>, R<sub>5</sub> and R<sub>6</sub> should be high-stability components.

#### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	25 $\mu$ F	electrolytic 25V	C426AR/F25
C <sub>2</sub>	16 $\mu$ F	electrolytic 40V	C426AR/G16
C <sub>3</sub>	400 $\mu$ F	electrolytic 25V	C437AR/F400
C <sub>4</sub>	10nF	polyester	C296AA/A10K
C <sub>5</sub>	220nF	polyester	C296AA/A220K
C <sub>6</sub>	1nF	polyester	C296AC/A1K
C <sub>7</sub>	160 $\mu$ F	electrolytic 25V	C437AR/F160
C <sub>8</sub>	47nF	polyester	C296AA/A47K
C <sub>9</sub>	1250 $\mu$ F	electrolytic 25V	C431BR/F1250
C <sub>10</sub>	2500 $\mu$ F	electrolytic 40V	C431BR/G2500

#### Mains Transformer

The transformer used in this circuit may be obtained from the following manufacturers under the type numbers given:

Colne Electric Limited, Rickmansworth, Herts	20043
Drake Transformers Limited, Billericay, Essex	294-140
Gardners Transformers Limited, Christchurch, Hants	GR 97183
Parmeko Limited, Aylestone Park, Leicester	P 3204

### Heatsinks

The dissipation in the driver transistor may reach 1W and a 1.5mm (16 gauge) bright aluminium heatsink with an area of 10cm<sup>2</sup> should be used for this transistor. Each output transistor should be mounted on a 1.5mm bright aluminium heatsink with an area of 15cm<sup>2</sup>.

## 25W Audio Amplifier (page 74)

### Transistors and Diodes

Circuit reference	Mullard type
TR <sub>1</sub>	BC158
TR <sub>2</sub>	BFX84
TR <sub>3</sub>	BC148 or BC108
TR <sub>4</sub>	BFX84
TR <sub>5</sub>	BFX29
TR <sub>6</sub>	BDY20
TR <sub>7</sub>	BDY20
D <sub>1</sub>	BA114
D <sub>2</sub>	BA114
D <sub>3</sub>	BA114
Bridge rectifier	4 × BYX38-300

### Resistors

Tolerance:  $\pm 10\%$  except R<sub>2</sub> and R<sub>3</sub>, which should be  $\pm 5\%$  components.  
Power rating:  $\frac{1}{8}$ W except R<sub>13</sub>, which should be a  $\frac{1}{2}$ W component, R<sub>20</sub>, R<sub>21</sub> and R<sub>22</sub>, which should be 3W components.

Circuit reference	Value	Circuit reference	Value
R <sub>1</sub> preset potentiometer	100k $\Omega$	R <sub>13</sub>	3.9k $\Omega$
R <sub>2</sub>	220k $\Omega$	R <sub>14</sub>	470 $\Omega$
R <sub>3</sub>	100k $\Omega$	R <sub>15</sub>	6.8k $\Omega$
R <sub>4</sub>	47k $\Omega$	R <sub>16</sub>	1k $\Omega$
R <sub>5</sub>	47 $\Omega$	R <sub>17</sub>	1k $\Omega$
R <sub>6</sub>	10k $\Omega$	R <sub>18</sub>	100 $\Omega$
R <sub>7</sub>	10k $\Omega$	R <sub>19</sub>	100 $\Omega$
R <sub>8</sub>	3.3k $\Omega$	R <sub>20</sub>	0.5 $\Omega$
R <sub>9</sub> preset potentiometer	1k $\Omega$	R <sub>21</sub>	0.5 $\Omega$
R <sub>10</sub>	680 $\Omega$	R <sub>22</sub>	0.5 $\Omega$
R <sub>11</sub>	5.6k $\Omega$	R <sub>23</sub>	10 $\Omega$
R <sub>12</sub>	470 $\Omega$		

Resistors R<sub>2</sub>, R<sub>3</sub>, R<sub>4</sub> and R<sub>11</sub> should be high-stability components.

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	5 $\mu$ F	electrolytic 64V	C426AR/H5
C <sub>2</sub>	2.5 $\mu$ F	electrolytic 64V	C426AR/H2.5
C <sub>3</sub>	160 $\mu$ F	electrolytic 25V	C437AR/F160
C <sub>4</sub>	33nF	polyester	C296AA/A33K
C <sub>5</sub>	1nF	polyester	C296AC/A1K
C <sub>6</sub>	1.5nF	polyester	C296AC/A1K5
C <sub>7</sub>	32 $\mu$ F	electrolytic 40V	C426AR/G32
C <sub>8</sub>	4.7nF	polyester	C296AC/A4K7
C <sub>9</sub>	220nF	polyester	C296AA/A220K
C <sub>10</sub>	1250 $\mu$ F	electrolytic 40V	C431BR/G1250
C <sub>11</sub>	2500 $\mu$ F	electrolytic 64V	C431BR/H2500

### Mains Transformer

The transformer used in this circuit may be obtained from the following manufacturers under the type numbers given:

Colne Electric Limited, Rickmansworth, Herts	20044
Drake Transformers Limited, Billericay, Essex	786-174
Gardners Transformers Limited, Christchurch, Hants	GR 97184
Parmeko Limited, Aylestone Park, Leicester	P 3205

### Heatsinks

With a 4 $\Omega$  load, the dissipation in each output transistor can be 18W. The maximum permissible junction temperature of the BDY20 is 200°C and the thermal resistance between junction and mounting base is 1.5degC/W. Therefore, with a mounting which has a thermal resistance of 0.5degC/W, and a maximum ambient temperature of 45°C, the thermal resistance of the heatsink must not exceed 6.5degC/W. This can be achieved with 80cm<sup>2</sup> of 2mm (14 gauge) bright aluminium or 50cm<sup>2</sup> of 2mm blackened aluminium for each transistor. As the dissipation of each driver transistor may be 1W, the driver transistors should be mounted on small heatsinks, such as the Redpoint 5F heatsink.

### Pre-amplifier (page 109)

#### Transistors

Circuit reference	Mullard type
TR <sub>1</sub>	BC149 or BC109
TR <sub>2</sub>	BC148 or BC108
TR <sub>3</sub>	BC149 or BC109

### Resistors

Tolerance:  $\pm 10\%$

Power rating:  $\frac{1}{8}W$

Circuit reference	Value	
	10W circuit	25W circuit
R <sub>1</sub>		1·8M $\Omega$
R <sub>2</sub>		see text
R <sub>3</sub>		56k $\Omega$
R <sub>4</sub>		220k $\Omega$
R <sub>5</sub>		22k $\Omega$
R <sub>6</sub>	100k $\Omega$	220k $\Omega$
R <sub>7</sub>	100k $\Omega$	220k $\Omega$
R <sub>8</sub>	12k $\Omega$	18k $\Omega$
R <sub>9</sub>		220k $\Omega$
R <sub>10</sub>		680 $\Omega$
R <sub>11</sub>	560 $\Omega$	820 $\Omega$
R <sub>12</sub>	6·8k $\Omega$	3·3k $\Omega$
R <sub>13</sub>	12k $\Omega$	6·8k $\Omega$
R <sub>14</sub>	22k $\Omega$	10k $\Omega$
R <sub>15</sub>	560k $\Omega$	150k $\Omega$
R <sub>16</sub>	10k $\Omega$	4·7k $\Omega$
R <sub>17</sub>	logarithmic potentiometer	10k $\Omega$
R <sub>18</sub>	logarithmic/reverse logarithmic potentiometer	10k $\Omega$
R <sub>19</sub>		22k $\Omega$
R <sub>20</sub>	linear potentiometer	250k $\Omega$
R <sub>21</sub>	linear potentiometer	100k $\Omega$
R <sub>22</sub>		22k $\Omega$
R <sub>23</sub>		15k $\Omega$
R <sub>24</sub>		47k $\Omega$
R <sub>25</sub>		1k $\Omega$
R <sub>26</sub>		47k $\Omega$
R <sub>27</sub>		220k $\Omega$
R <sub>28</sub>		10k $\Omega$
R <sub>29</sub>		15k $\Omega$
R <sub>30</sub>		220k $\Omega$
R <sub>31</sub>		3·3k $\Omega$
R <sub>32</sub>		6·8k $\Omega$
R <sub>33</sub>	3·9k $\Omega$	18k $\Omega$
R <sub>34</sub>	—	15k $\Omega$
R <sub>35</sub>	—	4·7k $\Omega$

Resistors R<sub>6</sub>, R<sub>7</sub>, R<sub>8</sub> and R<sub>9</sub> should be high-stability components.

## Capacitors

Circuit reference	Value		Description	Mullard type	
	10W circuit	25W circuit		10W circuit	25W circuit
C <sub>1</sub>		6.4 $\mu$ F	electrolytic 25V		C426AR/F6.4
C <sub>2</sub>		80 $\mu$ F	electrolytic 2.5V		C426AR/A80
C <sub>3</sub>		2.5 $\mu$ F	electrolytic 25V		C426AR/H2.5
C <sub>4</sub>	10nF	22nF	metallised foil	C281AB/A10K	C281AB/A22K
C <sub>5</sub>	3.3nF	6.8nF	polyester	C296AC/A3K3	C296AC/A6K8
C <sub>6</sub>	10nF	22nF	metallised foil	C281AB/A10K	C281AB/A22K
C <sub>7</sub>		10 $\mu$ F	electrolytic 16V		C426AR/E10
C <sub>8</sub>		2.5 $\mu$ F	electrolytic 25V		C426AR/H2.5
C <sub>9</sub>		80 $\mu$ F	electrolytic 25V		C426AR/F80
C <sub>10</sub>		15nF	metallised foil		C281AB/A15K
C <sub>11</sub>		15nF	metallised foil		C281AB/A15K
C <sub>12</sub>		10 $\mu$ F	electrolytic 16V		C426AR/E10
C <sub>13</sub>		3.3nF	polyester		C296AC/A3K3
C <sub>14</sub>		3.3nF	polyester		C296AC/A3K3
C <sub>15</sub>		10 $\mu$ F	electrolytic 16V		C426AR/E10
C <sub>16</sub>		6.8nF	polyester		C296AC/A6K8
C <sub>17</sub>		470nF	metallised foil		C281AB/A470K
C <sub>18</sub>		10 $\mu$ F	electrolytic 16V		C426AR/E10
C <sub>19</sub>		470nF	metallised foil		C281AB/A470K
C <sub>20</sub>		6.8nF	polyester		C296AC/A6K8
C <sub>21</sub>		2.2nF	polyester		C296AC/A2K2
C <sub>22</sub>		10 $\mu$ F	electrolytic 16V		C426AR/E10

## CHAPTER 8

# HIGH-QUALITY F.M. TUNERS

Two f.m. tuners are described, the first using a BF200 silicon planar transistor in the r.f. stage and the second using a BFW10 field-effect transistor. The tuners may be used with the f.m. stages of the i.f. amplifier described in Chapter 4 (page 52).

A comparison of the two tuners will reveal that the circuits give very similar performances. However, it should be noted that the f.e.t. tuner achieves this performance at the expense of a relatively high supply voltage and high operating current in the r.f. stage. In addition, the field-effect transistor must be selected for a value of  $I_{DSS}$  (drain current at zero source-gate voltage) of 8 to 20mA.

The chapter also includes a stereo decoder circuit for reception of stereophonic broadcasts.

The difficulties associated with the construction and lining-up of r.f. and i.f. amplifiers must again be stressed. Only those constructors with previous experience in this type of circuitry and with access to specialised equipment should consider building the circuits described in this chapter.

Component lists for the circuits are given at the end of the chapter.

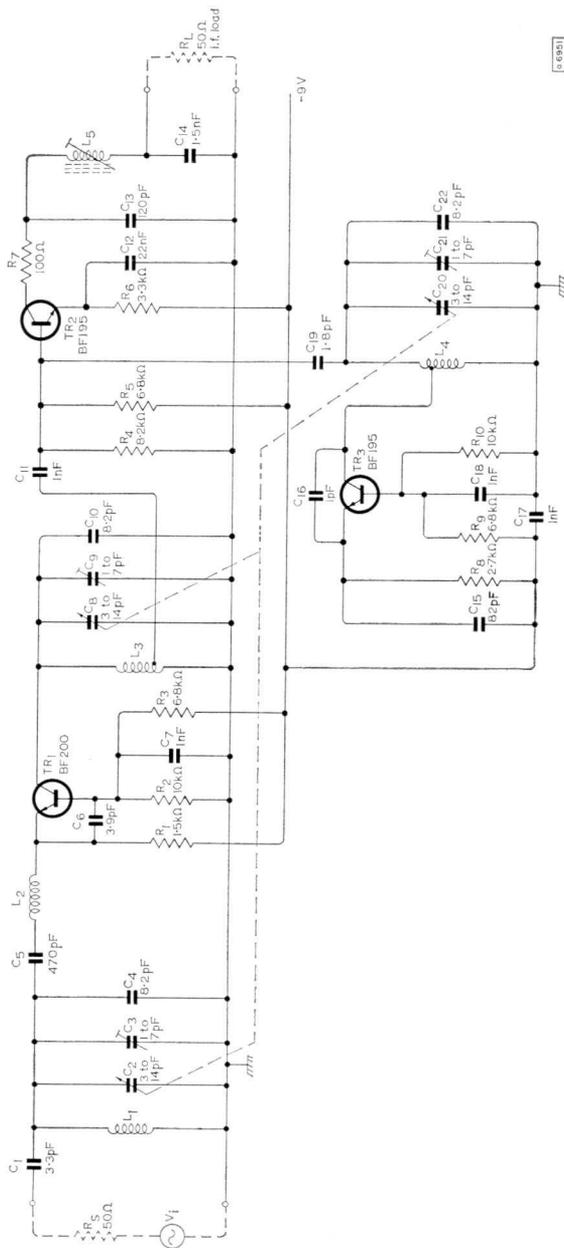


Fig. 111—Three-ganged, capacitively-tuned f.m. tuner circuit

## F.M. TUNER USING BF200 SILICON PLANAR TRANSISTOR

High-quality f.m. reception calls for a tuner having a low noise factor and excellent signal-handling ability. These objectives can be achieved by exploiting the inherently good signal-handling capability of the BF200 in a circuit configuration favouring optimum noise performance.

This high-performance tuner uses a tuned aerial circuit matched to the r.f. transistor by a fixed inductance. By this means it is possible to retain the benefits of a low-loss selective aerial circuit, which can be approximately power matched, and, through an impedance transform, to allow the transistor to be matched for optimum noise performance. The transistor is then required to handle less signal for a given noise performance.

### Circuit Description

The complete circuit of a three-ganged capacitively-tuned f.m. tuner is given in Fig. 111.

#### *R.F. Stage*

The BF200 transistor,  $TR_1$ , operates in the common-base configuration at a collector current of 2mA. The optimum source impedance for minimum noise is equivalent to the parallel combination of  $125\Omega$  resistance and  $500\Omega$  inductance, giving a typical noise factor of 2dB.

The emitter resistor  $R_1$ , inductance  $L_2$  and capacitor  $C_6$  cause some additional losses which result in a typical noise factor for the tuner of about 4.5dB. Capacitor  $C_6$  prevents parasitic oscillation at very high frequencies and must be mounted between the base and emitter leads of the BF200 and as closely as possible to them.

The low feedback capacitance of the BF200 allows the collector to be connected to the top of the tuned interstage circuit. The collector output damping of the BF200 is negligible.

The transducer gain of the r.f. stage is about 16dB at a 3dB bandwidth of the loaded interstage circuit of 1MHz. The value of  $Q_0$  of this tuned circuit is 200.

#### *Mixer Stage*

The mixer transistor,  $TR_2$ , is a Lockfit transistor, type BF195, and operates in the common-emitter configuration at a collector current of 1mA. At this current and with a source impedance of about  $100\Omega$ , the contribution of the mixer stage to the total noise factor is small—approximately 0.5dB.

By keeping the oscillator signal at the base of  $TR_2$  to as low a value as possible—about 50mV—harmonics of the oscillator frequency at the input to the mixer are virtually eliminated, while sufficient conversion gain is maintained.

Because the base of TR<sub>2</sub> has an inductive tap on the interstage circuit, no additional 10.7MHz i.f. series filter is necessary between the base and the emitter. To prevent i.f. parasitic oscillations, a 100Ω resistor, R<sub>7</sub>, is connected in series with the collector.

The value of Q<sub>0</sub> of the i.f. tuned circuit is about 150 and the value of Q<sub>L</sub> is 50. The mixer gain is about 18dB.

### *Oscillator Stage*

The oscillator transistor, TR<sub>3</sub>, is also a BF195, and operates in the common-base configuration at a current of 1mA. The coupling between the top of the oscillator coil and the base of the mixer is obtained via capacitor C<sub>19</sub>. The low value of this capacitance—1.8pF—guarantees that large aerial signals have practically no effect on the oscillator circuit. The oscillator frequency is below the aerial frequency.

### **Performance**

In obtaining the performance data given in this section, the aerial and i.f. trimmer capacitors were adjusted at each frequency to give no padding error at the measuring point.

### *Transducer Gain*

Transducer gain is defined as the ratio of the power delivered to the load to the power supplied into the stage if it were power-matched to the source, that is if the input impedance were equal to the source impedance.

$$\text{Transducer gain} = \frac{V_O^2}{R_L} \cdot \frac{4R_S}{V_S^2}$$

where V<sub>O</sub> = voltage developed across load

R<sub>L</sub> = load impedance

R<sub>S</sub> = source impedance of generator

V<sub>S</sub> = e.m.f. of generator

The values of transducer gain at three tuning frequencies are given in Table 5. A curve of transducer gain at a tuning frequency of 98MHz plotted against supply voltage is given in Fig. 112.

**TABLE 5**  
**Measured Values of Transducer Gain**

Tuning Frequency (MHz)	Transducer Gain (dB)
90	32
98	35
105	35

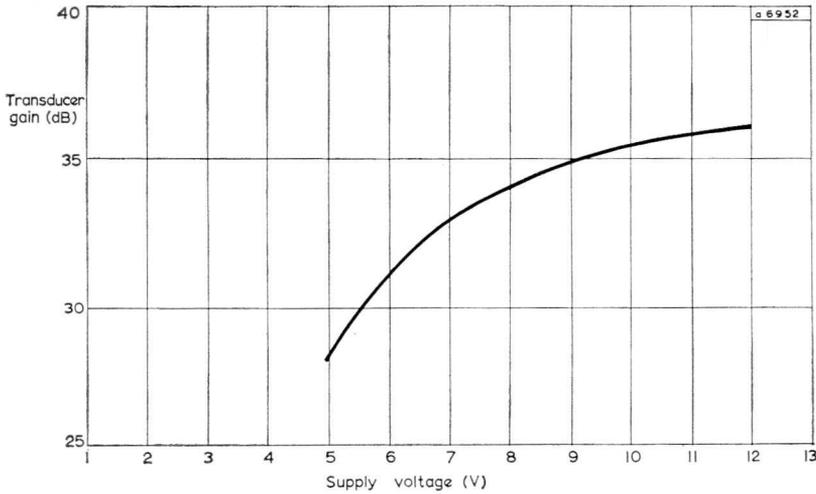


Fig. 112—Variation of transducer gain with supply voltage at a tuning frequency of 98MHz

*Noise Factor*

The values of noise factor at three tuning frequencies are given in Table 6.

**TABLE 6**  
**Measured Values of Noise Factor**

Tuning Frequency (MHz)	Noise Factor (dB)
90	4.7
98	4.5
105	4.3

*Repeat-spot Suppression*

Repeat spots are caused by harmonics of the oscillator signal mixing with those of a strong aerial signal resulting in a signal having the intermediate frequency. For example, if an unwanted aerial signal of 88MHz is present, its second harmonic (176MHz) mixes with the second harmonic (165.3MHz) of an oscillator signal of 82.65MHz to give 10.7MHz—the intermediate frequency. The 82.65MHz oscillator signal corresponds to an aerial signal of 93.35MHz and so the 88MHz aerial signal will be received when the dial is set to 93.35MHz.

Repeat-spot suppression is sometimes known as half i.f. rejection. The values of repeat-spot suppression are given for two input levels at each of three tuning frequencies in Table 7. The value of  $R_S$  is  $50\Omega$  throughout. A graph of repeat-spot suppression against input voltage at a tuning frequency of 98MHz is given in Fig. 113. From this graph it can be seen that the repeat-spot suppression improves by 1dB for a decrease in signal of 2dB.

**TABLE 7**  
**Measured Values of Repeat-spot Suppression**

Tuning Frequency (MHz)	Input Voltage ( $\mu$ V)	Repeat-spot Suppression (dB)
90	40	73
90	1	89
98	40	71
98	1	87
105	40	70
105	1	86

*Double-beat Suppression*

Double beats occur if two strong aerial signals have frequencies or harmonics which combine with the oscillator signal, or its harmonics, to give the intermediate frequency. For example, if two strong unwanted aerial signals with frequencies of 94MHz and 96.7MHz are present, and the dial is set to 100.7MHz, the audio signals associated with the two strong signals will be heard superimposed upon each other. This is because the dial setting of 100.7MHz corresponds to an oscillator frequency of 90MHz and the second harmonic of this oscillator signal (180MHz) combines with the two strong unwanted aerial signals ( $94+96.7-180$ ) to give 10.7MHz—the intermediate frequency.

The values of double-beat suppression given in Table 8 were measured with two identical interference signals at 95 and 97.5MHz. Double-beat reception is possible at the tuning frequencies 92.5, 100 and 101.6MHz and at these frequencies, measurements of double-beat suppression for a required signal level of  $40\mu$ V are given. The value of  $R_S$  is  $50\Omega$ . A graph of double-beat suppression against input voltage is given in Fig. 114.

**TABLE 8**  
**Measured Values of Double-beat Suppression**

Tuning Frequency (MHz)	Double-beat Suppression (dB)
92.5	63
100	66
101.6	65

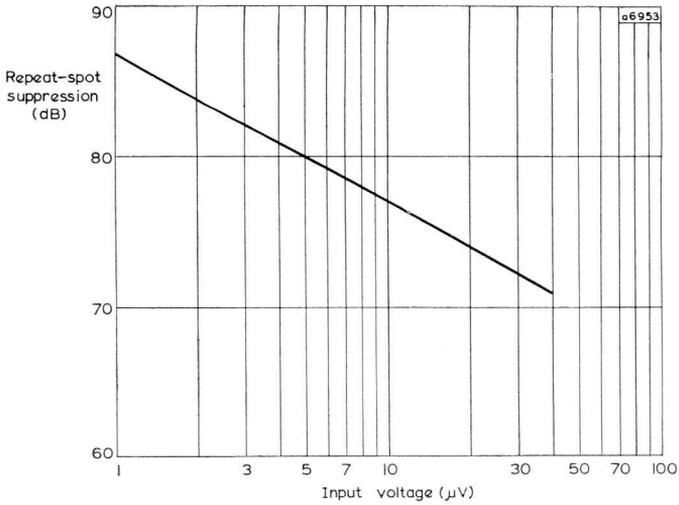


Fig. 113—Variation of repeat-spot suppression with input voltage at a tuning frequency of 98MHz

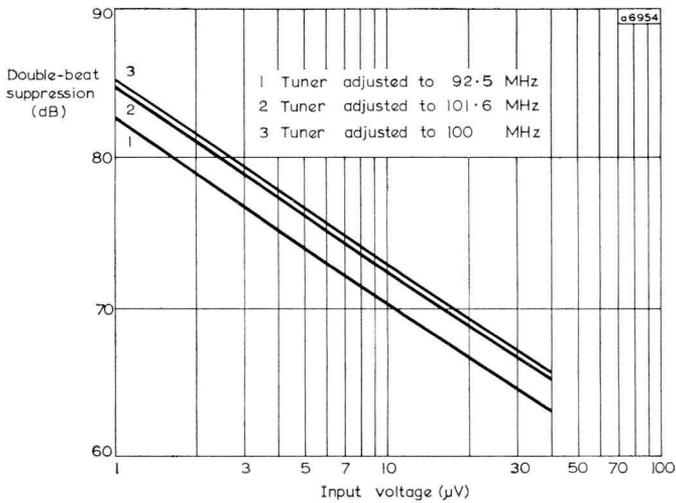


Fig. 114—Variation of double-beat suppression with input voltage

### Continuous-beat Suppression

Continuous-beats occur when two strong aerial signals have frequencies, or harmonics, which combine to give the intermediate frequency. If continuous beats occur, they occur regardless of the dial setting. For example, if two strong aerial signals are present with frequencies of 90MHz and 95.35MHz, their second harmonics (180MHz and 190.7MHz respectively) combine to produce 10.7MHz—the intermediate frequency.

The continuous-beat suppression, measured at a tuning frequency of 98MHz, is 67dB at input voltage levels of 40 $\mu$ V for both signals.

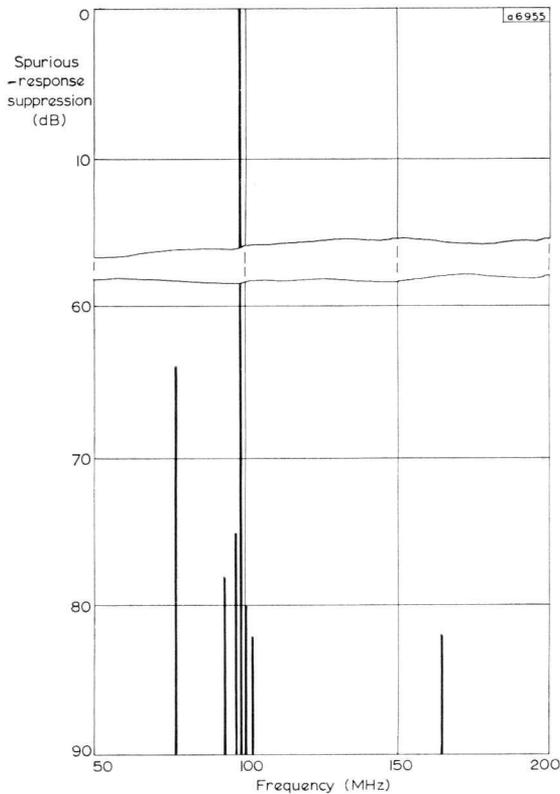


Fig. 115—Histogram of spurious-response suppression

### *Spurious-response Suppression*

The one-signal spurious-response suppression is given in histogram form in Fig. 115. The tuner frequency is 98MHz and the reference level of the required input signal is  $8\mu\text{V}$ . The spikes in Fig. 115 show that at a certain input frequency, an i.f. output signal occurs. The input signal level at this frequency must be many times higher to obtain the same i.f. output signal as for a wanted input signal of  $8\mu\text{V}$ . The ratio of the required interference input signal level and the required input signal of  $8\mu\text{V}$  is given as spurious-response suppression. This ratio is indicated by the top level of the spikes in Fig. 115.

### *Image Rejection*

The image rejection is determined by the selectivity of the aerial at a frequency different from the tuned frequency, and by interstage circuit quality factors. In the tuner described, the image-rejection frequency is  $2 \times 10^{-7}\text{MHz}$  below the tuning frequency. The values of image rejection at three tuning frequencies are given in Table 9.

**TABLE 9**  
**Measured Values of Image Rejection**

Tuning Frequency (MHz)	Image Rejection (dB)
90	63
98	64
105	63

### *I.F. Rejection*

The values of i.f. rejection at three tuning frequencies are given in Table 10.

**TABLE 10**  
**Measured Values of I.F. Rejection**

Tuning Frequency (MHz)	I.F. Rejection (dB)
90	64
98	63
105	61

### *Signal Handling*

When the value of  $R_S$  is  $50\Omega$ , signals of more than 1V can be handled. The shift of the oscillator frequency is not more than 20kHz for signals up to 1V.

### *Oscillator Voltage on Mixer*

The oscillator voltage at the base of the mixer is kept low. The values of oscillator voltage at three tuning frequencies are given in Table 11.

**TABLE 11**  
**Measured Values of Oscillator Voltage at Base of Mixer**

Tuning Frequency (MHz)	Oscillator Voltage (mV)
90	35
98	50
105	60

### *Frequency Shift of Oscillator*

The oscillator frequency shift due to supply voltage variations is about 20kHz per 2V supply voltage variation.

### *Oscillator Radiation*

When the value of  $R_s$  is  $50\Omega$ , the oscillator radiation at the input terminals of the tuner is  $300\mu V$ .

## F.M. TUNER USING BFW10 FIELD-EFFECT TRANSISTOR

The circuit for a high-quality, two-ganged, capacitively-tuned f.m. tuner is shown in Fig. 116. The tuner uses a BFW10 field-effect transistor in the r.f. input stage, and BF195 transistors in the mixer and oscillator stages. Because it has a square-law input characteristic, the field-effect transistor is particularly useful in this circuit, where a high degree of spurious-response suppression is required. The low noise factor and high input impedance of the device are also advantageous in this type of circuit.

### Circuit Description

#### *R.F. Stage*

The BFW10 field-effect transistor operates at a typical drain current of 10mA and typical drain-source voltage of 6V. The optimum source impedance for minimum noise is equivalent to the parallel combination of 910 $\Omega$  resistance and 370 $\Omega$  inductance, giving a typical noise factor of 2.5dB.

The aerial input circuit is transformer-coupled to the input of the field-effect transistor, the unloaded quality factor,  $Q_0$ , of the aerial transformer being about 80 at a secondary inductance of 330nH.

The transducer gain of the r.f. stage is about 8.5dB at 100MHz. The value of  $Q_0$  for the interstage circuit is 200.

The d.c. stabilisation is obtained by a voltage divider for the gate electrode and a source resistance of value 680 $\Omega$ . A limitation of this design is that the minimum value of  $I_{DSS}$  for the field-effect transistor is 8mA because the gate of the transistor may not be positive with respect to the source.

#### *Mixer and Oscillator Stages*

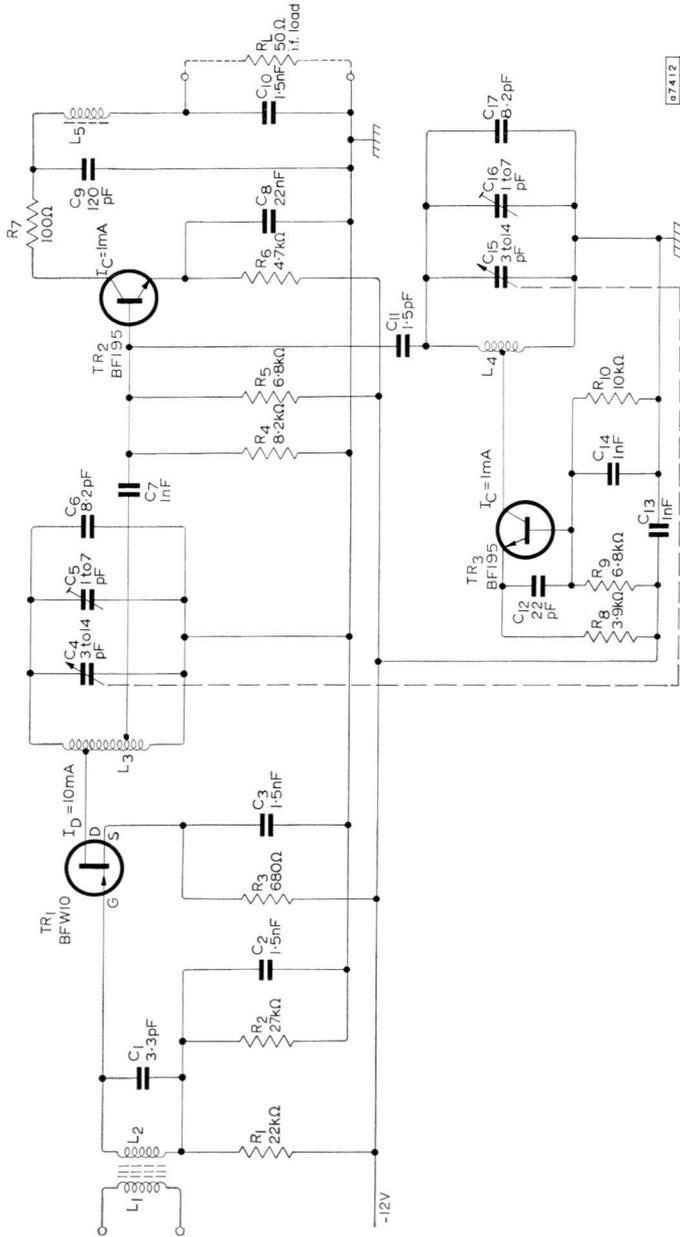
Comparison of the circuit diagram of this tuner with that of the planar-transistor version shown on page 146 will show that the mixer and oscillator stages of the two circuits are almost identical. The description given on pages 147 and 148 applies equally to this tuner.

### Performance

For definitions of terms transducer gain, repeat-spot suppression, double-beat suppression, continuous-beat suppression, spurious-response suppression and image rejection, see pages 148 to 153.

#### *Transducer Gain*

The values of transducer gain measured at three tuning frequencies are given in Table 12. In Fig. 117 the transducer gain at a tuning frequency of 98MHz is plotted as a function of supply voltage.



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Fig. 116—Two-ganged, capacitively-tuned f.m. tuner circuit

**TABLE 12**  
**Measured Values of Transducer Gain**

Tuning Frequency (MHz)	Transducer Gain (dB)
90	26
98	30
106	29

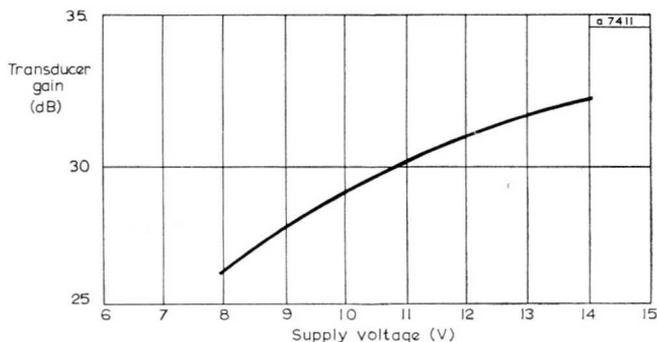


Fig. 117—Variation of transducer gain with supply voltage  
at a tuning frequency of 98MHz

*Noise Factor*

The values of noise factor measured at three tuning frequencies are given in Table 13.

**TABLE 13**  
**Measured Values of Noise Factor**

Tuning Frequency (MHz)	Noise Factor (dB)
90	6.9
98	4.2
106	4.1

In this circuit, the noise contribution of the mixer stage rises when the power gain of the r.f. stage decreases. Because of the selectivity of the aerial input circuit, the power gain of the r.f. stage at 90MHz is 3dB below that at 98MHz, hence the increase in noise factor at the lower frequency.

*Repeat-spot Suppression*

The values of repeat-spot suppression at three tuning frequencies and an aerial signal level of 100 $\mu$ V are given in Table 14.

**TABLE 14**  
**Measured Values of Repeat-spot Suppression**

Tuning Frequency (MHz)	Repeat-spot Suppression (dB)
90	68
98	61
106	58

For an aerial signal level of  $1\mu\text{V}$  the repeat-spot suppression would be about 80dB.

*Double-beat Suppression*

The values of double-beat suppression at three tuning frequencies are given in Table 15.

**TABLE 15**  
**Measured Value of Double-beat Suppression**

Tuning Frequency (MHz)	Double-beat Suppression (dB)
92.5	60
100	57
101.6	59

*Continuous-beat Suppression*

The values of continuous-beat suppression at three tuning frequencies with both aerial signals at a level of  $100\mu\text{V}$  are given in Table 16.

**TABLE 16**  
**Measured Values of Continuous-beat Suppression**

Tuning Frequency (MHz)	Continuous-beat Suppression (dB)
90	65
98	60
106	56

*Spurious-response Suppression*

The one-signal spurious-response suppression is given in histogram form in Fig. 118. The tuning frequency is 98MHz. The reference level of the required input signal is  $20\mu\text{V}$ .

*Image Rejection*

The values of image rejection at three tuning frequencies is given in Table 17.

**TABLE 17**  
**Measured Values of Image Rejection**

Tuning Frequency (MHz)	Image Rejection (dB)
90	42
98	43
106	38

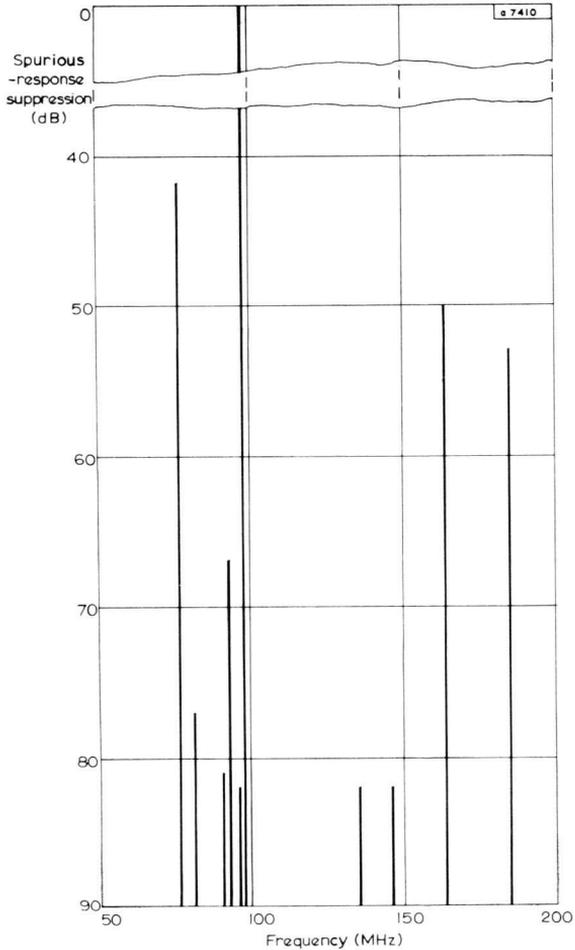


Fig. 118—Histogram of spurious-response suppression

### *I.F. Rejection*

The values of i.f. rejection at three tuning frequencies are given in Table 18.

**TABLE 18**  
**Measured Value of I.F. Rejection**

Tuning Frequency (MHz)	I.F. Rejection (dB)
90	76
98	76
106	75

### *Signal Handling*

With a value of source impedance of  $300\Omega$ , signals of more than 1V can be handled. The shift of oscillator frequency is not more than 20kHz for signals up to 1V.

### *Oscillator Voltage on Mixer*

The oscillator voltages at the base of the mixer at three tuning frequencies are given in Table 19.

**TABLE 19**  
**Oscillator Voltage at Base of Mixer**

Tuning Frequency (MHz)	Oscillator Voltage (mV)
90	40
98	60
106	80

### *Frequency Shift of Oscillator*

The frequency shift of the oscillator due to a supply voltage variation of 1V is less than 20kHz. The lower limit of supply voltage for oscillator operation is 4V.

## **STEREO DECODER**

### **Stereo Transmissions**

Stereophonic programmes are regularly broadcast on the v.h.f. transmissions of BBC Radio Three. For these transmissions to be received stereophonically, certain equipment in addition to the normal v.h.f. receiver is required. This additional equipment consists of two separate audio amplifiers and loudspeakers to amplify the left- and right-hand channels and some means of separating—or decoding—the channels.

The system the BBC, in common with other European broadcasting authorities, uses is the pilot-tone (Zenith-G.E.) system, with a  $50\mu\text{s}$  pre-emphasis time-constant instead of the  $75\mu\text{s}$  used in the U.S.A. In this system, the left- and right-hand channels are encoded at the transmitter by a multiplexing process and transmitted on a single wavelength. The channels are decoded after detection in the receiver. The system is compatible; that is, listeners with unadapted v.h.f. receivers can receive an acceptable monophonic representation of the stereophonic broadcast.

The sum of the left- and right-hand channels provides a satisfactory monophonic signal which can be transmitted and received in the normal way. For stereophonic reception, however, additional information is necessary to enable the stereo receiver to separate the left- and right-hand signals. In the Zenith-G.E. system, this extra information consists of a 'difference' signal—left minus right—which is transmitted as the upper and lower sidebands of a 38kHz subcarrier. The 38kHz subcarrier is itself totally suppressed.

To ensure synchronisation between the decoder in the receiver and the encoder at the transmitter, a low-level synchronising signal, or pilot tone, is also transmitted. The frequency of the pilot tone is 19kHz.

### **Circuit Description**

The circuit diagram of a decoder is shown in Fig. 119. The pilot tone is extracted from the multiplex input by means of a 19kHz circuit immediately following the discriminator output. The pilot tone is then amplified by the first transistor and applied to the base of the second transistor. The second transistor is biased to operate in class B; that is, only the positive half-cycles of the amplified pilot tone are amplified. The distorted waveform resulting from this type of amplification is very rich in second harmonic content, and this second harmonic (38kHz) is extracted by means of a tuned circuit at the collector of the second transistor. The peak-to-peak amplitude of the 38kHz signal, between the collector end of the coil and the tap on the coil, is limited to approximately twice the supply voltage; hence its amplitude is constant regardless of input level once a certain value has been exceeded.

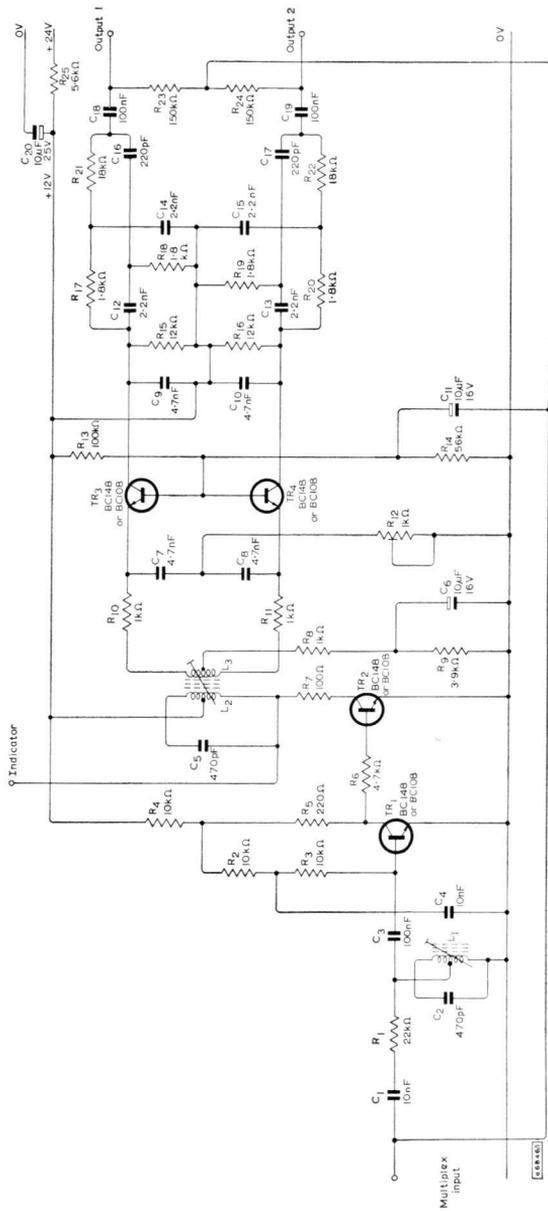


Fig. 119—Stereo decoder circuit

A centre-tapped secondary winding applies antiphase switching signals to the emitters of two transistors and the complete multiplex information is applied to their bases. With this arrangement, synchronous detection to obtain the 'difference' signal, along with 'matrixing' of the 'sum' and 'difference' signals, occurs and the two separated left- and right-hand signals appear—one at each collector. With a simple decoder operating on the principle described, only a limited separation is obtainable, so arrangements have been made in the design of the circuit shown in Fig. 119 to improve the separation. This is done by deliberately introducing a controlled amount of crosstalk into the two outputs in antiphase to the inherent crosstalk, thereby cancelling the crosstalk.

Conventional de-emphasis occurs in the collector circuits of the two switching transistors but this is insufficient to remove the 38kHz waveform from the output. As the 38kHz waveform is of sufficient amplitude to constitute a nuisance, in that it may give rise to distortion in any following audio amplifier or to beating with the oscillator frequency of a tape recorder, it is removed by passing each output through a parallel-T filter tuned to 38kHz. This does have a slight adverse effect on the de-emphasis but it is kept within acceptable limits.

In the absence of the 38kHz switching waveform at the emitters of the two switching transistors, they are biased to operate in class A and any signal applied to their bases is reproduced at their collectors. The circuit is therefore compatible, requiring no switching between mono and stereo operation.

The input impedance of the decoder is approximately 15k $\Omega$  and the decoder may be fed directly from a semiconductor discriminator capable of providing a loaded output with a peak-to-peak amplitude of approximately 750mV. It may also be fed from a typical valve discriminator, in which case the discriminator output should be attenuated by means of a series resistor shunted by a capacitor. Typical values for the resistor and capacitor are 3.3k $\Omega$  to 33k $\Omega$  and a few hundred picofarads. Such an arrangement not only provides the correct input level at all multiplex frequencies but also reduces the discriminator loading to an acceptable value.

Each of the audio amplifiers into which the outputs of the decoder are fed must have an input impedance of not less than 50k $\Omega$ .

### **Stereo Indicator**

A stereo indicator gives a visual indication when a stereo transmission is in progress. It is also essential in the alignment of the decoder if only a limited amount of test equipment is available. A stereo indicator circuit using a single transistor is shown in Fig. 120.

This stereo indicator circuit operates by detecting the 38kHz signal generated when the 19kHz pilot tone is passed through the frequency-doubling circuit in the decoder. This 38kHz signal is fed through a limiting resistor and blocking capacitor to a shunt rectifier. The voltage derived from this shunt rectifier is applied to the base of a transistor. The transistor remains cut off when the signal is absent and is turned on when it is present. Therefore, the bulb in the collector circuit glows when a stereophonic broadcast is in progress but remains extinguished when a monophonic transmission is being received.

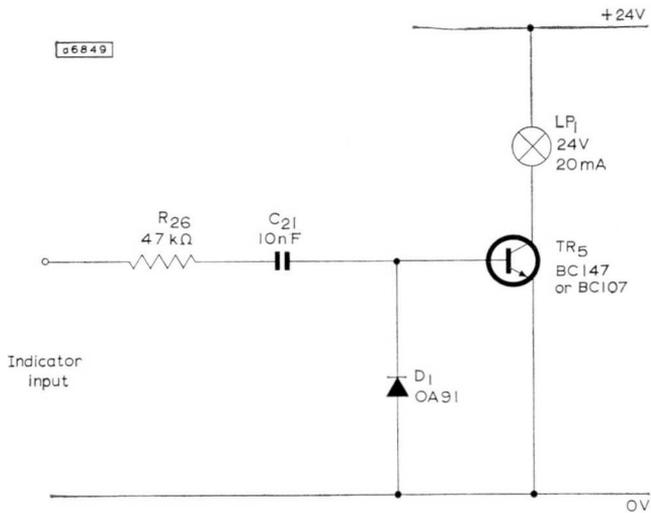


Fig. 120—Stereo indicator circuit

### Alignment of the Decoder

To assist those people who do not have access to a wide range of accurate test equipment, a simple alignment procedure using the BBC transmissions has been devised. Tones are transmitted by the BBC outside normal listening hours to enable the channels to be identified and to assist in alignment. Details of the broadcasts are given in Appendix 2. For the initial alignment, however, any stereo broadcast can be used. The alignment procedure is as follows.

First, remove the de-emphasis component network from the discriminator output.

Connect a potentiometer with a value of at least  $50k\Omega$  across the discriminator output and connect the decoder input to the potentiometer slider. With the potentiometer set for maximum output, tune the receiver to a stereo broadcast on Radio Three.

Adjust the 19kHz and 38kHz coil slugs to give maximum output at the 'Indicator' terminal (maximum brightness of the indicator lamp). Adjust the input potentiometer setting until the indicator lamp just glows, then adjust the coil slugs again to give maximum brightness. Keep repeating this procedure until adjusting the cores either way results in the lamp getting dimmer. The two coils are now aligned. If tolerances in coil manufacture result in difficulty being experienced in this adjustment, especially of the 38kHz coil, because the slugs are at one end of their travel, replace the 470pF capacitor across the coil by a 390pF capacitor.

When the coils are aligned, connect the discriminator output directly to the decoder input and discard the input potentiometer.

Adjust the preset potentiometer in the decoder circuit to its mid-position. The decoder should give a reasonable degree of separation, but further adjustment using the test-tone transmissions is necessary, as follows.

Connect the two outputs to two audio amplifiers and identify the left- and right-hand channels. When the left-hand channel only is being transmitted, disconnect the left-hand amplifier and turn the 38kHz slug anti-clockwise (when viewed from the top) until the output from the right-hand loudspeaker is a minimum. Anti-clockwise rotation is necessary because a false minimum is encountered if the slug is rotated clockwise.

Reconnect the left-hand amplifier.

When the right-hand channel only is being transmitted, disconnect the right-hand amplifier and adjust the preset potentiometer from its mid-point position to give minimum output from the left-hand loudspeaker.

Reconnect the right-hand amplifier.

The decoder is now correctly aligned.

## Performance

The channel separation of the decoder is shown graphically in Fig. 121. The signal-to-noise ratio is well above the acceptable level although the signal-to-noise ratio of a stereo broadcast is inherently slightly lower than that of a mono broadcast. For good stereo reproduction, the i.f. bandwidth of the tuner unit should be not less than 180kHz.

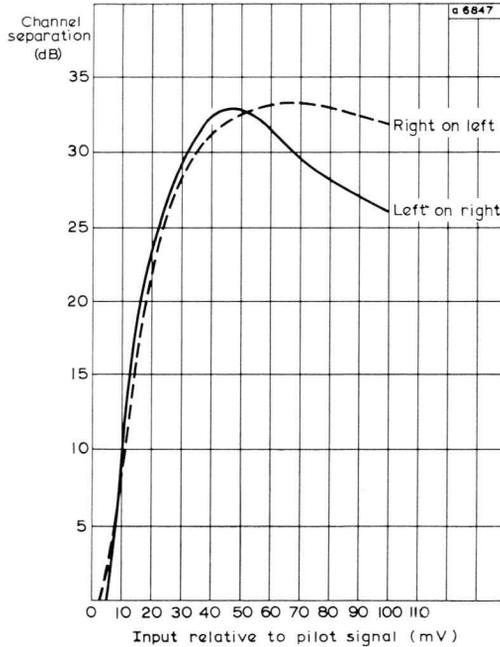


Fig. 121—Channel separation characteristics

### Aerial Requirements for Stereo Reception

One common cause of poor results from an f.m. stereo receiver is an inadequate aerial. Satisfactory stereo results cannot be expected unless a really good signal is fed into the tuner.

Unlike the other signals in the complex f.m. stereo signal, the 19kHz signal is of constant amplitude and does not vary with the modulation. Therefore, it is a measure of the signal strength fed to the f.m. tuner. Because its amplitude is much less than that of the other signals, the 19kHz signal is also nearer the noise level. When it is weak the separation between the two a.f. signals is unlikely to be great enough or constant, and the stereophonic effect will be lost.

The output circuit or i.f. filtering circuit of the ratio detector in an f.m. mono receiver requires an a.f. bandwidth of about 15kHz. In an f.m. stereo receiver, however, an a.f. bandwidth of 53kHz is required. Consequently, if all other factors are equal, the signal-to-noise ratio of a stereo receiver is not so good as that of a mono receiver. Therefore, before fitting a stereo decoder, it would be wise to check that the strength of the received

signal is sufficient to ensure that the deterioration in signal-to-noise ratio does not make good stereo reception an impossibility.

This check may be made by means of the simple circuits shown in Fig. 122. The circuit in Fig. 122(a) will produce an attenuation of about 12dB. If this is connected between the aerial feeder and the tuner aerial sockets when receiving mono, there should be little audible difference. Any increase in the background noise (hiss, clicks and pops) indicates that a more efficient aerial or a re-siting of the aerial is needed.

If the test is satisfactory, two of the circuit in Fig. 122(a) in series, or one of the circuit in Fig. 122(b), should be connected between the aerial feeder and the tuner aerial sockets. If again there is no marked increase in the background noise, the aerial is quite adequate for f.m. stereo. However, if there is a marked increase in the background noise, the aerial system may not be good enough for f.m. stereo. An aerial array or a new position for the aerial may be needed.

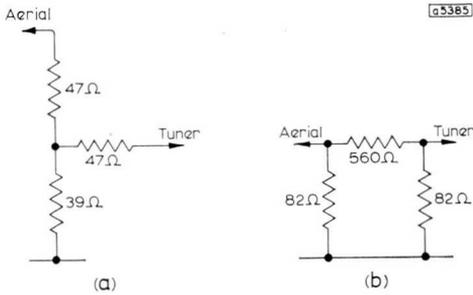


Fig. 122—Circuits for checking signal-to-noise ratio

## COMPONENT LISTS FOR CIRCUITS IN CHAPTER 8

### F.M. Tuner using BF200 Transistor (page 146)

#### Transistors

Circuit reference	Mullard type
TR <sub>1</sub>	BF200
TR <sub>2</sub>	BF195
TR <sub>3</sub>	BF195

#### Resistors

Tolerance:  $\pm 10\%$

Power rating:  $\frac{1}{8}W$

Circuit reference	Value	Circuit reference	Value
R <sub>1</sub>	1.5k $\Omega$	R <sub>6</sub>	3.3k $\Omega$
R <sub>2</sub>	10k $\Omega$	R <sub>7</sub>	100 $\Omega$
R <sub>3</sub>	6.8k $\Omega$	R <sub>8</sub>	2.7k $\Omega$
R <sub>4</sub>	8.2k $\Omega$	R <sub>9</sub>	6.8k $\Omega$
R <sub>5</sub>	6.8k $\Omega$	R <sub>10</sub>	10k $\Omega$

#### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	3.3pF	tubular ceramic	
C <sub>2</sub>	3 to 14pF	ganged tuning capacitor	
C <sub>8</sub>	3 to 14pF		
C <sub>20</sub>	3 to 14pF		
C <sub>3</sub>	1 to 7pF	trimmer	
C <sub>4</sub>	8.2pF	ceramic plate	C333CB/L8E2
C <sub>5</sub>	470pF	tubular ceramic	
C <sub>6</sub>	3.9pF	ceramic plate	C333CB/L3E9
C <sub>7</sub>	1nF	polystyrene	C295AC/1K
C <sub>9</sub>	1 to 7pF	trimmer	
C <sub>10</sub>	8.2pF	ceramic plate	C333CB/L8E2
C <sub>11</sub>	1nF	polystyrene	C295AC/1K
C <sub>12</sub>	22nF	metallised foil	C280AE/P22K
C <sub>13</sub>	120pF	ceramic plate	C333CH/C120E
C <sub>14</sub>	1.5nF	polystyrene	C295AA/1K5
C <sub>15</sub>	82pF	ceramic plate	C333CH/C82E
C <sub>16</sub>	1pF	tubular ceramic	
C <sub>17</sub>	1nF	polystyrene	C295AC/1K
C <sub>18</sub>	1nF	polystyrene	C295AC/1K
C <sub>19</sub>	1.8pF	tubular ceramic	
C <sub>21</sub>	1 to 7pF	trimmer	
C <sub>22</sub>	8.2pF	ceramic plate	C333CB/L8E2

### Coils

All the coils are wound with enamelled-copper wire and all except  $L_5$  are air-cored. The i.f. coil,  $L_5$ , follows normal design practice to match the input of the amplifier.

Circuit reference	$L_1$	$L_2$	$L_3$	$L_4$	$L_5$
$Q_0$	200		200	200	150
		150			
$Q_L$	50		100	—	—
No. of turns	4	22	4	$4\frac{1}{2}$	—
Wire diam. (mm)	1	0.2	1	1	—
Pitch (mm)	2	close	2	2	—
Inside diam. (mm)	8	4	8	8	—
No. of turns between tap and chassis end of coil	—	—	$\frac{3}{4}$	$3\frac{1}{2}$	—

### F.M. Tuner using BFW10 Field-effect Transistor (page 156)

#### Transistors

Circuit reference	Mullard type
$TR_1$	BFW10
$TR_2$	BF195
$TR_3$	BF195

#### Resistors

Tolerance:  $\pm 10\%$

Power rating:  $\frac{1}{8}W$

Circuit reference	Value
$R_1$	$22k\Omega$
$R_2$	$27k\Omega$
$R_3$	$680\Omega$
$R_4$	$8.2k\Omega$
$R_5$	$6.8k\Omega$
$R_6$	$4.7k\Omega$
$R_7$	$100\Omega$
$R_8$	$3.9k\Omega$
$R_9$	$6.8k\Omega$
$R_{10}$	$10k\Omega$

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	3·3pF	tubular ceramic	
C <sub>2</sub>	1·5nF	tubular ceramic	
C <sub>3</sub>	1·5nF	tubular ceramic	
C <sub>4</sub>	3 to 14pF	ganged tuning capacitor	
C <sub>15</sub>	3 to 14pF		
C <sub>5</sub>	1 to 7pF	trimmer	
C <sub>6</sub>	8·2pF	ceramic plate	C333CB/L8E2
C <sub>7</sub>	1nF	polystyrene	C295AC/1K
C <sub>8</sub>	22nF	metallised foil	C280AE/P22K
C <sub>9</sub>	120pF	ceramic plate	C333CH/C120E
C <sub>10</sub>	1·5nF	polystyrene	C295AA/1K5
C <sub>11</sub>	1·5pF	tubular ceramic	
C <sub>12</sub>	22pF	tubular ceramic	
C <sub>13</sub>	1nF	polystyrene	C295AC/1K
C <sub>14</sub>	1nF	polystyrene	C295AC/1K
C <sub>16</sub>	1 to 7pF	trimmer	
C <sub>17</sub>	8·2pF	ceramic plate	C333CB/L8E2

### Coils

All the coils are wound with enamelled-copper wire. L<sub>1</sub> and L<sub>2</sub> are wound on powdered iron; L<sub>3</sub> and L<sub>4</sub> are air-cored. The i.f. coil, L<sub>5</sub>, follows normal design practice to match the input of the amplifier.

Circuit reference	L <sub>1</sub>	L <sub>2</sub>	L <sub>3</sub>	L <sub>4</sub>	L <sub>5</sub>
Q <sub>O</sub>	80	80	200		150
Q <sub>L</sub>	4	4	100		
No. of turns	3	4	4	4½	
Wire diam. (mm)	0·15	0·15	1	1	
Pitch (mm)			2	2	
Inside diam. (mm)			8	8	
No. of turns between tap and chassis end of coil			drain 1 mixer ½	3½	

### Stereo Decoder and Indicator (pages 162 and 164)

#### Transistors and Diode

Circuit reference	Mullard type
TR <sub>1</sub>	BC148 or BC108
TR <sub>2</sub>	BC148 or BC108
TR <sub>3</sub>	BC148 or BC108
TR <sub>4</sub>	BC148 or BC108
TR <sub>5</sub>	BC147 or BC107
D <sub>1</sub>	OA91

## Resistors

Tolerance:  $\pm 10\%$  except  $R_{17}$  to  $R_{22}$  which should be  $\pm 5\%$  components.

Power rating:  $\frac{1}{8}$ W

Circuit reference	Value	Circuit reference	Value
$R_1$	22k $\Omega$	$R_{14}$	56k $\Omega$
$R_2$	10k $\Omega$	$R_{15}$	12k $\Omega$
$R_3$	10k $\Omega$	$R_{16}$	12k $\Omega$
$R_4$	10k $\Omega$	$R_{17}$	1.8k $\Omega$
$R_5$	220 $\Omega$	$R_{18}$	1.8k $\Omega$
$R_6$	4.7k $\Omega$	$R_{19}$	1.8k $\Omega$
$R_7$	100 $\Omega$	$R_{20}$	1.8k $\Omega$
$R_8$	1k $\Omega$	$R_{21}$	18k $\Omega$
$R_9$	3.9k $\Omega$	$R_{22}$	18k $\Omega$
$R_{10}$	1k $\Omega$	$R_{23}$	150k $\Omega$
$R_{11}$	1k $\Omega$	$R_{24}$	150k $\Omega$
$R_{12}$ preset potentiometer	1k $\Omega$	$R_{25}$	5.6k $\Omega$
$R_{13}$	100k $\Omega$	$R_{26}$	47k $\Omega$

## Capacitors

Circuit reference	Value	Description	Mullard type
$C_1$	10nF	metallised foil	C280AE/P10K
$C_2$	470pF	polystyrene or silvered-mica	
$C_3$	100nF	metallised foil	C280AE/P100K
$C_4$	10nF	metallised foil	C280AE/P10K
$C_5$	470pF	polystyrene or silvered-mica	
$C_6$	10 $\mu$ F	electrolytic 16V	C426AR/E10
$C_7$	4.7nF	polyester	C296AC/A4K7
$C_8$	4.7nF	polyester	C296AC/A4K7
$C_9$	4.7nF	polyester	C296AC/A4K7
$C_{10}$	4.7nF	polyester	C296AC/A4K7
$C_{11}$	10 $\mu$ F	electrolytic 16V	C426AR/E10
$C_{12}$	2.2nF	polystyrene	C295AA/2K2
$C_{13}$	2.2nF	polystyrene	C295AA/2K2
$C_{14}$	2.2nF	polystyrene	C295AA/2K2
$C_{15}$	2.2nF	polystyrene	C295AA/2K2
$C_{16}$	220pF	ceramic plate	C333CH/C220E
$C_{17}$	220pF	ceramic plate	C333CH/C220E
$C_{18}$	100nF	metallised foil	C280AE/P100K
$C_{19}$	100nF	metallised foil	C280AE/P100K
$C_{20}$	10 $\mu$ F	electrolytic 25V	C426AR/H10
$C_{21}$	10nF	metallised foil	C280AE/P10K

Capacitors  $C_2$  and  $C_5$  should be high-quality polystyrene or silvered-mica types.

Capacitors  $C_{12}$  to  $C_{17}$  should be  $\pm 5\%$  components.

## Coils

Circuit reference	Mullard type
L <sub>1</sub>	WF2949
L <sub>2</sub> /L <sub>3</sub>	WF2951

For coil details see Figs. 123 and 124.

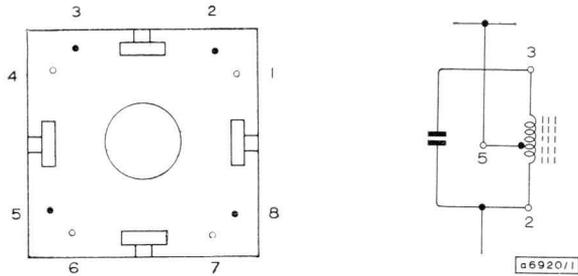


Fig. 123—19kHz coil, L<sub>1</sub> (Mullard type WF2949), viewed from underside.  
Pin 8 is the coil clamp and should be connected to earth

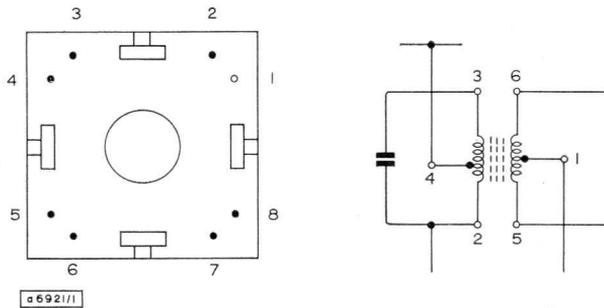


Fig. 124—38kHz coil, L<sub>2</sub>/L<sub>3</sub> (Mullard type WF2951), viewed from underside.  
Pin 8 is the coil clamp and should be connected to earth

## Stereo Indicator Bulb LPI

A 24V, 20mA indicator bulb is required, a suitable component being the Electronics Limited type SGF9/D/GN/24, available from Edinburgh Way, Harlow, Essex.

## CHAPTER 9

# TEST EQUIPMENT

Items of test equipment which will be found useful in commissioning and maintaining audio and radio circuitry include a voltmeter, ohmmeter, milliammeter, output power meter, a.f. signal generator, i.f. and r.f. signal generator with provision for modulation at audio frequencies, oscilloscope, transistor tester and stereo balance meter.

It is beyond the scope of this book to give designs for the complex equipment required for aligning and testing h.f. circuitry, and it is recommended that professionally built equipment should be obtained for this purpose.

### OSCILLOSCOPE

The reader is referred to the following sources for design information on a simple oscilloscope and auxiliary circuitry:

“The Wireless World Oscilloscope”, available from Wireless World, Dorset House, Stamford Street, London, S.E.1;

“Oscilloscope Trace Doubler” by W. Kemp, published in The Radio Constructor, Vol. 22, No. 4, Nov. 1968;

“Wide-band Oscilloscope Amplifier” by G. Sowersby, published in The Radio Constructor, Vol. 22, No. 5, Dec. 1968.

The last two are available from Data Publications Limited, 57 Maida Vale, London, N.9.

## VOLTMETER

It is essential that the voltmeter does not alter the conditions in the circuit when measurements are being made. The voltmeter should therefore have a resistance of at least  $20\text{k}\Omega/\text{V}$ . A voltage coverage of 2.5 to 100V d.c. is required. A valve voltmeter is very suitable for the measurements if precautions are taken to prevent earth-loop currents damaging the transistors.

The simplest approach to the testing of the directly-coupled amplifiers described in this book is to measure voltage levels throughout the circuit. A conventional four-transistor circuit is used here as an example, and the voltage levels resulting from various transistor failures are given in Table 20.

**TABLE 20**  
**Voltage Levels**

Transistor Fault	Voltage at point				General Performance
	A	B	C	D	
TR <sub>2</sub> o-c	high	no voltage	high	slightly higher than normal	no output
TR <sub>2</sub> s-c	low	twice normal voltage	low	slightly higher than normal	no output
TR <sub>3</sub> o-c	near-chassis	low	high	low	no output
TR <sub>4</sub> o-c	normal	normal	normal	normal	high distortion
TR <sub>3</sub> or TR <sub>4</sub> s-c	indeterminate				emitter resistors burn out

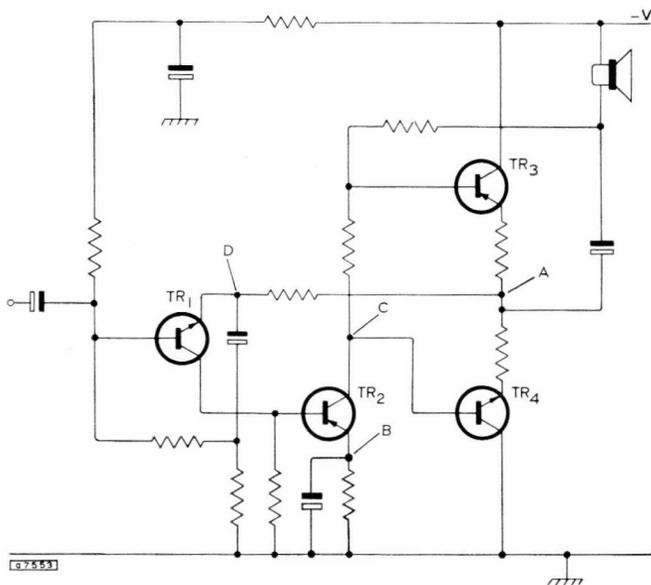


Fig. 125—Direct-coupled amplifier with voltage test points

## OHMMETER

The voltage at the output terminals of the ohmmeter should not exceed 1.5V otherwise there is a possibility of the transistors and miniature electrolytic capacitors in the circuit under test being damaged. In all cases when resistance measurements are made, the equipment should be switched off.

If only one component is suspect this can be isolated from the circuit by unsoldering the connection at one end and then testing with the ohmmeter. However, if components have to be checked while they are still in the circuit there are two methods available to prevent the 'diode elements' of the transistors affecting the measurements. In the first method the base connection of the transistor is unsoldered so that the transistor is effectively disconnected from the circuit. The resistance measurements may then be made, although allowance must be made for other resistors shunting the component under test. The second method uses the voltage of the ohmmeter to 'reverse bias' the diode elements of the transistor so that the transistor does not conduct.

The basic circuit of a series-connected ohmmeter is shown in Fig. 126 in which both the colour and the polarity of the output terminals are

shown. To provide the reverse bias for a p-n-p transistor, the positive ohmmeter terminal (coloured black) is connected to the base (n-type material) and the negative ohmmeter terminal (coloured red) connected to the emitter or collector (p-type material). The connections for measuring the values of the base bias resistors of a p-n-p transistor are shown in Fig. 127; for an n-p-n transistor the connections are reversed. If the stage being checked is not isolated from the rest of the circuit the other stages will appear as a resistance in parallel with that being measured. The measured value of resistance will therefore be lower than the actual resistance.

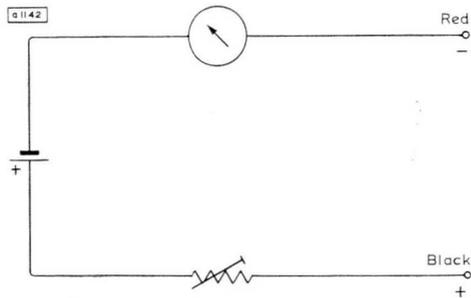


Fig. 126—Circuit of series-connected ohmmeter

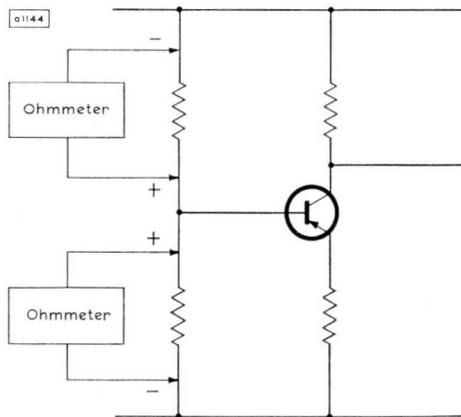


Fig. 127—Method of checking base bias resistors with ohmmeter

## MILLIAMMETER

A milliammeter with a full-scale deflection of 100mA may be used to measure the currents in the pre-amplifier and driver stages of the amplifiers described, but the output transistors in some of the circuits draw currents in excess of 1A.

## OUTPUT-POWER METER

An output-power meter can be used for checking a.f. output power. The loudspeaker should be replaced by the output-power meter which is switched to the loudspeaker impedance. The meter then indicates the output power directly.

A voltmeter can also be used conveniently for this measurement if an output-power meter is not available. The loudspeaker should be replaced by a resistor corresponding to the loudspeaker impedance and the power level calculated as the voltage drop across the resistor.

## AUDIO-FREQUENCY SIGNAL GENERATOR

The signal generator shown in Fig. 128 is a Wien-bridge oscillator which will supply an output voltage of 1V r.m.s. over a frequency range 15Hz to 200kHz.

### Circuit Description

The circuit uses a thermistor  $R_5$  as an amplitude control device, and the output is essentially independent of small changes in supply voltage and ambient temperature. The oscillator uses only three transistors and, apart from the frequency-determining capacitors, only one capacitor. The circuit operates from a 9V supply, although little difference in performance is obtained with supply voltages from 6 to 10V. The current consumption is:

6V supply	6.3mA
9V supply	11.5mA
10V supply	13mA

### Performance

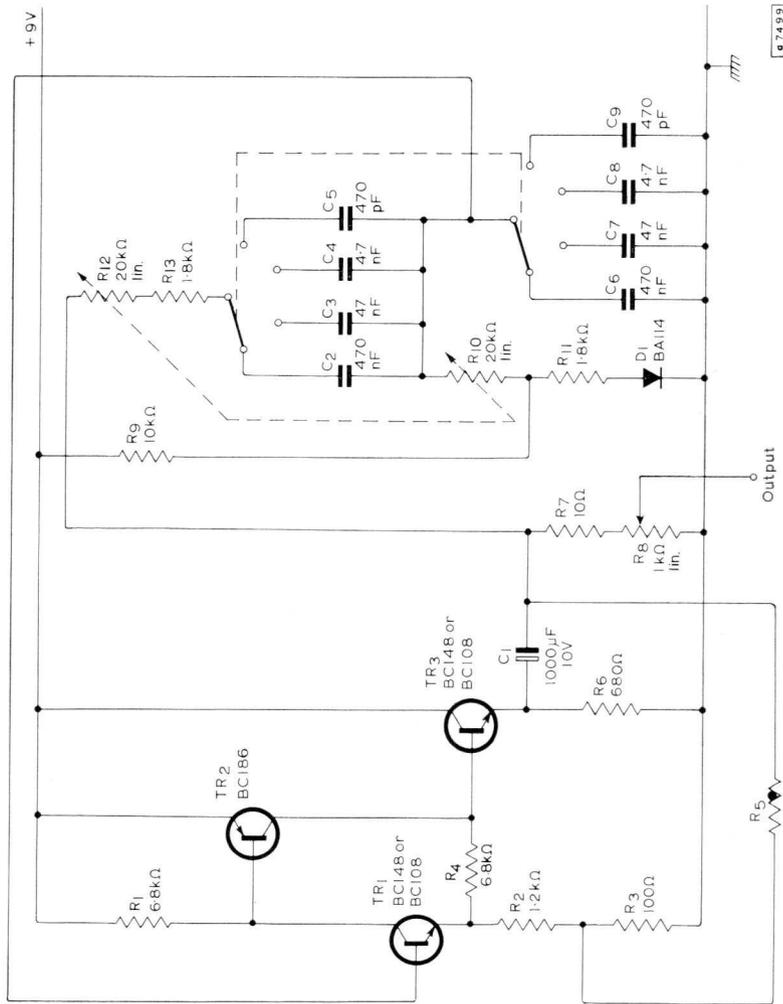
The frequency coverage is 15Hz to 200kHz in four ranges:

Range 1	15Hz to 200Hz
Range 2	150Hz to 2kHz
Range 3	1.5kHz to 20kHz
Range 4	15kHz to 200kHz

The approximate harmonic distortion at 1kHz is:

second harmonic	0.1%
third harmonic	0.05%

At frequencies above 100kHz the frequency calibration does not



[ 67499 ]

Fig. 128—A.F. signal generator circuit

coincide with that for lower ranges, because of stray capacitances, and the output voltage is slightly higher.

## Components

### Transistors and Diode

Circuit reference	Mullard type
TR <sub>1</sub>	BC148 or BC108
TR <sub>2</sub>	BC186
TR <sub>3</sub>	BC148 or BC108
D <sub>1</sub>	BA114

### Resistors

Tolerance:  $\pm 5\%$

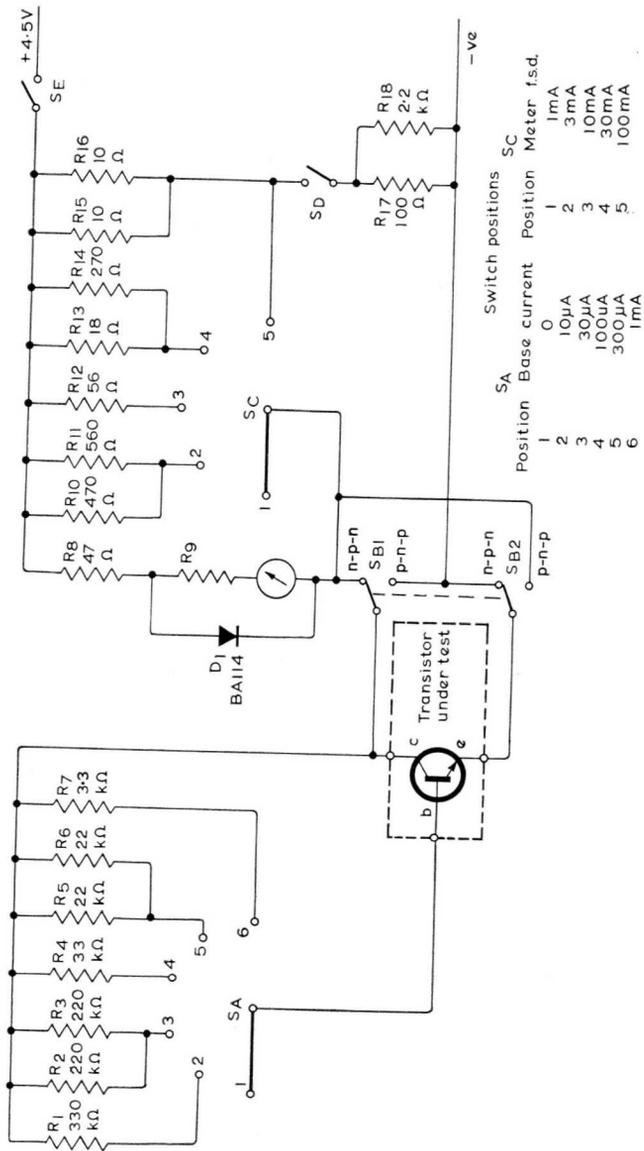
Power rating:  $\frac{1}{8}$ W

Circuit reference	Value
R <sub>1</sub>	6.8k $\Omega$
R <sub>2</sub>	1.2k $\Omega$
R <sub>3</sub>	100 $\Omega$
R <sub>4</sub>	6.8k $\Omega$
R <sub>5</sub> thermistor	
STC type R53	
R <sub>6</sub>	680 $\Omega$
R <sub>7</sub>	10 $\Omega$
R <sub>8</sub> linear potentiometer	1k $\Omega$
R <sub>9</sub>	10k $\Omega$
R <sub>10</sub> linear potentiometer	20k $\Omega$
R <sub>12</sub> linear potentiometer	20k $\Omega$
R <sub>11</sub>	1.8k $\Omega$
R <sub>13</sub>	1.8k $\Omega$

} matched to within 2dB  
(standard stereo matching)

### Capacitors

Circuit reference	Value	Description	Mullard type
C <sub>1</sub>	1000 $\mu$ F	electrolytic 10V	C437AR/D1000
C <sub>2</sub>	470nF	metallised foil	C280AE/A470K
C <sub>3</sub>	47nF	metallised foil	C280AE/P47K
C <sub>4</sub>	4.7nF	metallised foil	
C <sub>5</sub>	470pF	metallised foil	
C <sub>6</sub>	470nF	metallised foil	C280AE/A470K
C <sub>7</sub>	47nF	metallised foil	C280AE/P47K
C <sub>8</sub>	4.7nF	metallised foil	
C <sub>9</sub>	470pF	metallised foil	



07500

Fig. 129—Transistor tester circuit

## TRANSISTOR TESTER

The transistor tester shown in Fig. 129 uses a 1mA meter with suitable shunts to measure the collector current of the transistor under test. The base current of the transistor may be switched to zero for measurement of collector-emitter reverse leakage current,  $I_{CEO}$ , or to  $10\mu\text{A}$ ,  $30\mu\text{A}$ ,  $100\mu\text{A}$ ,  $300\mu\text{A}$  or 1mA for measurement of static forward current transfer ratio,  $h_{FE}$ .

### Circuit Description

A meter with 1mA f.s.d. is used and  $R_9$  is chosen to give a total resistance of  $450\Omega$ . Switch  $S_A$  selects base resistors  $R_1$  to  $R_7$ , whose common connection is taken to the collector to avoid the necessity for an additional pole on n-p-n/p-n-p selector switch  $S_B$ . Shunt resistors  $R_{10}$  to  $R_{16}$  are switched in by  $S_C$  to give collector current ranges 0 to 1mA, 0 to 3mA, 0 to 10mA, 0 to 30mA and 0 to 100mA. Switch  $S_D$  and resistors  $R_{17}$  and  $R_{18}$  provide a battery check facility. Diode  $D_1$  provides meter protection, limiting the current through the meter to 2mA.

Switches  $S_D$  and  $S_E$  should be spring-loaded to the 'off' position to prevent current drain from the battery when no measurement is being made. Switches  $S_A$  and  $S_B$  should be break-before-make, and switch  $S_C$  should be make-before-break.

### Measurement of $I_{CEO}$ and $h_{FE}$

Switch  $S_A$  is set to position 1,  $S_B$  to the correct polarity and  $S_C$  to a high range. The transistor is inserted into the socket and with  $S_E$  depressed to the 'on' position,  $S_C$  is turned until a reading is obtained. For germanium transistors this current,  $I_{CEO}$ , should be about 0.5 to 2mA, although for large transistors it may be higher. For silicon types,  $I_{CEO}$  should be negligible. If a high reading is obtained the device is probably faulty (short-circuited collector to emitter).

To measure gain, switch  $S_A$  is turned to the position corresponding to the required base current,  $S_C$  is set to a high range and  $S_E$  is again depressed. If the collector current obtained is  $I_C$  and the base current is  $I_B$ , the gain of the transistor is given by:

$$h_{FE} = \frac{I_C - I_{CEO}}{I_B}$$

If  $I_{CEO}$  is small enough to be neglected,  $h_{FE}$  can be read directly on the meter, but only for base currents of  $10\mu\text{A}$ ,  $100\mu\text{A}$  and 1mA. For other values of base current the gain must be computed using the formula given above.

If no increase in collector current is obtained when the base current is switched in, it may be assumed that the transistor is open-circuit.

## Battery Check

The internal battery should be checked periodically. With no transistor in the socket,  $S_C$  is switched to the 100mA position and  $S_D$  and  $S_E$  are depressed. A current of 45mA is drawn from a 4.5V battery, so the check is made on full load.

## Accuracy

The accuracy of the circuit is determined by the resistor tolerance—5% components are recommended—and the battery voltage. Accuracy also depends on the type of transistor under test and its gain.

The base resistors are returned to the collector of the transistor, and with this arrangement the base current is dependent to a small degree on the voltage drop in the meter circuit. In addition, with germanium transistors the base current will be higher than the value selected, due to the low value of  $V_{BE}$ .

With switch  $S_A$  in the  $10\mu\text{A}$  position, for example, for a silicon transistor the base current will be  $10\mu\text{A}$  with the meter reading at full scale. With the meter reading at one-third of full scale the base current will be  $11\mu\text{A}$ . A similar error will occur on all ranges. For a germanium transistor the corresponding base current with meter reading at full scale will be  $11.5\mu\text{A}$ , and  $12.5\mu\text{A}$  at one-third of full scale.

For most purposes the error for silicon devices may be neglected. For germanium devices it should be remembered that the base current is approximately 20 percent higher than the selected value.

## Components

### Diode

Circuit Reference	Mullard type
$D_1$	BA114

### Resistors

Tolerance:  $\pm 5\%$

Power rating:  $\frac{1}{8}\text{W}$

Circuit reference	Value	Circuit reference	Value
$R_1$	330k $\Omega$	$R_{10}$	470 $\Omega$
$R_2$	220k $\Omega$	$R_{11}$	560 $\Omega$
$R_3$	220k $\Omega$	$R_{12}$	56 $\Omega$
$R_4$	33k $\Omega$	$R_{13}$	18 $\Omega$
$R_5$	22k $\Omega$	$R_{14}$	270 $\Omega$
$R_6$	22k $\Omega$	$R_{15}$	10 $\Omega$
$R_7$	3.3k $\Omega$	$R_{16}$	10 $\Omega$
$R_8$	47 $\Omega$	$R_{17}$	100 $\Omega$
$R_9$	see text	$R_{18}$	2.2k $\Omega$

Suitable meters are manufactured by:  
Sifam Electrical Instrument Company Limited,  
Woodland Road, Torquay, Devon.  
Taylor Electrical Instruments Limited,  
Montrose Avenue, Slough, Bucks.

### BALANCE METER

A simple meter circuit which may be used to balance the two outputs in a stereo system is shown in Fig. 130.

Components  $C_1$  and  $C_2$  damp the meter movement. Resistor  $R_3$  is selected to suit the current rating of the centre-zero meter and the amplifier output (typically  $10k\Omega$  for a 1mA movement). The voltage rating of the electrolytic capacitors should be half the supply voltage of the system with which the meter is used.

Suitable meters are manufactured by:  
Sifam Electrical Instrument Company Limited,  
Woodland Road, Torquay, Devon.  
Taylor Electrical Instruments Limited,  
Montrose Avenue, Slough, Bucks.

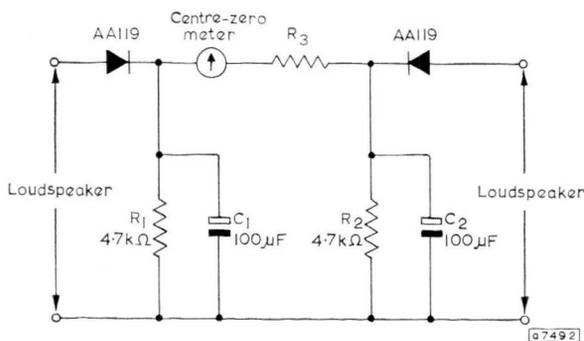


Fig. 130—Balance meter circuit

## PREVENTION OF EARTH-LOOP CURRENTS

Transistors may be destroyed by earth-loop currents if the chassis of test equipment is not earthed. The chassis may attain an a.c. potential of 50 to 100V through electrostatic coupling between the primary winding and the core of the mains transformer, as illustrated in Fig. 131. If, for example, the equipment under test is connected to the output terminals of an unearthed signal generator, this electrostatic potential is transferred to the chassis of the equipment, as shown in Fig. 131b. An isolating capacitor in the test leads will not prevent the transfer of the potential because this is an electrostatic effect. If an earthed soldering iron were now applied to the base of a transistor in the circuit, a relatively large current would flow to earth through the transistor and so destroy it.

The formation of this electrostatic potential can be prevented by earthing the chassis of the equipment and test instrument. An isolating capacitor, usually  $1\mu\text{F}$ , should be connected in the lead between a signal generator and the equipment to prevent the flow of direct circulating currents.

Transistors can also be damaged by the use of an unearthed soldering iron. It is possible for the bit, through a breakdown of the insulation between element and bit, to attain a potential of a few volts. When the iron is used on a circuit the potential of the bit may drive a relatively large current through the transistors. Damage due to the defect can be prevented by ensuring that the soldering iron is earthed. However, it should be remembered that when an earthed soldering iron is used the power supply to the circuit should be switched off during soldering.

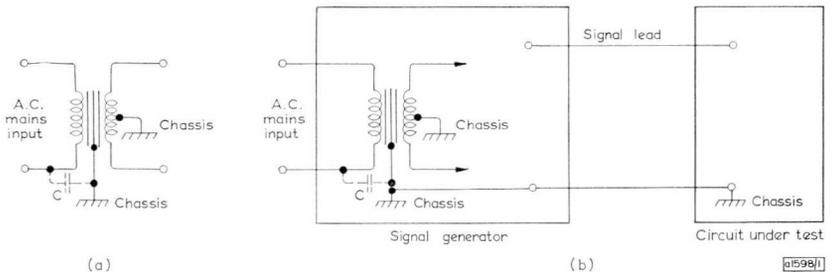


Fig. 131—Diagram showing (a) how the potential of an unearthed chassis is raised and (b) how the potential is transferred to other unearthed chassis

## APPENDIX 1

# BIASING ARRANGEMENTS FOR H.F. CIRCUITS

Three biasing arrangements used in h.f. circuits—voltage biasing with emitter feedback, current biasing with collector feedback and simple current biasing—were briefly considered in Chapter 2. The three arrangements are now described in detail, and for each of them an example is worked so that their effectiveness can be compared. In the examples, a transistor with a nominal value of  $h_{FE}$  of 100 ( $h_{FE}$  spread, 50 to 150) and a nominal  $V_{BE}$  of 0.7V ( $V_{BE}$  spread, 0.65 to 0.75V) is operating from a supply voltage  $V_S$  of 7V; the required emitter current is 1mA.

## VOLTAGE BIASING WITH EMITTER FEEDBACK

The circuit of a voltage biasing arrangement is given in Fig. 132. In this circuit the voltage  $V_B$  is given by

$$V_B = \frac{R_2 V_S}{R_1 + R_2}$$

provided that the voltage developed across  $R_2$  by the flow of base current is neglected.

The voltage  $V_E$  is given by

$$V_E = V_B - V_{BE}$$

and therefore

$$V_E = \frac{R_2 V_S}{R_1 + R_2} - V_{BE}$$

The operating current,  $I_E$ , is therefore given by

$$I_E = \frac{R_2 V_S}{R_E (R_1 + R_2)} - \frac{V_{BE}}{R_E} \quad \dots (1)$$

For the effects of spreads and temperature variations of  $V_{BE}$  to be negligible, the voltage  $V_E$  must be large compared with the changes in  $V_{BE}$ . Furthermore,  $R_E$  must also be large if changes in  $I_E$  caused by variation of  $V_S$  are to be small. In practice, a voltage drop,  $V_E$ , up to 3V is required with silicon transistors to prevent disproportionately large changes in operating current with changes in supply voltage, when large variations in  $V_S$  have to be accommodated. The corresponding value of  $V_E$  for germanium transistors is about 1V.

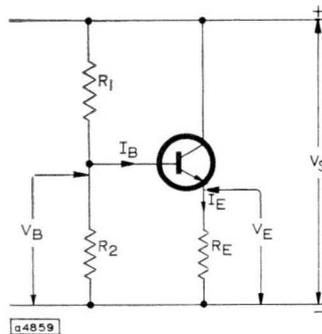


Fig. 132—Voltage biasing with emitter feedback

It has been assumed that the voltage developed across resistor  $R_2$  by the base current  $I_B$  is negligible and, if this is true, the operating current  $I_E$  is independent of  $h_{FE}$ , and therefore of spreads in  $h_{FE}$ . If this voltage is significant, however, the operating current is given by

$$I_E = \frac{\frac{V_S R_2}{R_1 + R_2} - V_{BE}}{\frac{R_1 R_2}{(R_1 + R_2)(1 + h_{FE})} + R_E} \quad \dots(2)$$

and the current is then dependent upon  $h_{FE}$ .

In the example considered the values of  $R_1$  and  $R_2$  are both  $15k\Omega$  and the value of  $R_E$  is  $2.7k\Omega$ . The nominal collector-emitter voltage is  $4.3V$ , and the actual nominal emitter current is  $1.01mA$ .

Substitution of these values in Eq. 2 gives maximum and minimum values of  $I_E$ , resulting from the spread of  $h_{FE}$ , of  $1.02mA$  and  $0.985mA$ . Thus, the spread in  $I_E$  resulting from the  $h_{FE}$  spread is  $+1\%$ ,  $-1.6\%$ .

The maximum and minimum values of  $I_E$ , resulting from the spread in  $V_{BE}$ , are  $1.025mA$  and  $0.99mA$ . Thus, the spread in  $I_E$  resulting from the spread in  $V_{BE}$  is  $\pm 1.7\%$ .

If  $V_S$  falls from  $7V$  to  $3.5V$ , the nominal emitter current falls from  $1.01mA$  to  $0.38mA$ ; that is,  $I_E$  falls by  $62\%$ .

Eq. 2 reverts to the simple equation (Eq. 1) if the following condition is fulfilled

$$R_E \gg \frac{R_1 R_2}{(R_1 + R_2)(1 + h_{FE})}$$

This equation can be written

$$I_E R_E \gg \frac{R_1 R_2}{(R_1 + R_2)} \times \frac{I_E}{(1 + h_{FE})}$$

or

$$V_E \gg \frac{R_1 R_2 I_B}{(R_1 + R_2)}$$

Therefore, for the operating current of the circuit shown in Fig. 132 to be substantially independent of  $h_{FE}$ , the voltage developed across the emitter resistor must be very much greater than the voltage developed, by the flow of base current, across the d.c. source resistance at the base of the transistor. The d.c. source resistance at the base of the transistor is formed by the parallel combination of  $R_1$  and  $R_2$ .

### CURRENT BIASING WITH COLLECTOR FEEDBACK

In the current-biased circuit shown in Fig. 133 the voltage  $V_C$  is given by

$$V_C = V_S - R_1 I_E .$$

Since

$$I_E = (1 + h_{FE}) I_B$$

then

$$V_C = V_S - I_B R_1 (1 + h_{FE}).$$

The base current  $I_B$  is also given by

$$I_B = \frac{V_C - V_{BE}}{R_2} .$$

Hence, if  $V_C$  is eliminated, the base current is given by

$$I_B = \frac{V_S - V_{BE}}{R_2 + R_1 (1 + h_{FE})} .$$

Consequently, the operating current is given by

$$I_E = \frac{(V_S - V_{BE}) (1 + h_{FE})}{R_2 + R_1 (1 + h_{FE})} . \quad \dots(3)$$

In the example considered, the value of  $R_1$  is  $2.7\text{k}\Omega$  and the value of  $R_2$  is  $330\text{k}\Omega$ . The nominal value of  $V_{CE}$  is  $4.28\text{V}$ , and the actual nominal emitter current is  $1.05\text{mA}$ .

Substitution of these values in Eq.3 gives maximum and minimum values of emitter current, caused by the spread in  $h_{FE}$ , of  $1.29\text{mA}$  and  $0.635\text{mA}$ . Thus the spread in  $I_E$  caused by the spread in  $h_{FE}$  is  $+23\%$ ,  $-35\%$ .

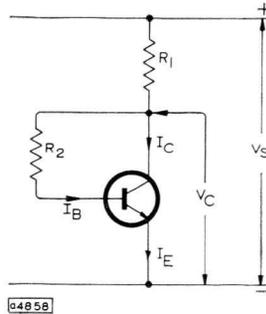


Fig. 133—Current biasing with collector feedback

The variation in  $I_E$  with spreads and temperature variations in  $h_{FE}$  can be reduced only by applying the following condition:

$$R_1 (1 + h_{FE}) \gg R_2.$$

This lowers the available collector voltage swing and is possible only with large supply voltages.

The maximum and minimum values of emitter current, caused by the spread in  $V_{BE}$ , are  $1.04\text{mA}$  and  $1.06\text{mA}$ . Thus, the spread in  $I_E$  caused by the spread in  $V_{BE}$  is  $\pm 0.95\%$ .

If  $V_S$  falls from  $7\text{V}$  to  $3.5\text{V}$ , the nominal emitter current falls from  $1.05\text{mA}$  to  $0.47\text{mA}$ , that is,  $I_E$  falls by  $55\%$ .

In this arrangement there is a spread in the collector voltage resulting from the spread in  $h_{FE}$ . In the extreme case, when most of the available supply voltage is developed across  $R_1$  (when the spread in operating current due to the spread in  $h_{FE}$  is very low) the spread in collector voltage is directly proportional to the spread in  $h_{FE}$ .

### SIMPLE CURRENT BIASING

The simplest method of biasing, using only one resistor, is shown in Fig. 134. The current  $I_B$  is given by

$$I_B = \frac{V_S - V_{BE}}{R_1}.$$

Thus, the emitter current is given by

$$I_E = \frac{V_S - V_{BE}}{R_1} (1 + h_{FE}). \quad \dots(4)$$

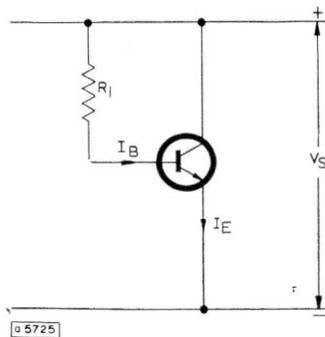


Fig. 134—Simple current biasing

In the example considered the value of  $R_1$  is  $680\text{k}\Omega$ . The nominal value of  $V_{CE}$  is  $7\text{V}$  (equal to  $V_S$ ), and the actual nominal value of  $I_E$  is  $0.935\text{mA}$ .

Substitution of these values in Eq. 4 gives maximum and minimum values of  $I_E$ , resulting from the spread in  $h_{FE}$ , of  $1.4\text{mA}$  and  $0.475\text{mA}$ . Thus the spread in  $I_E$  resulting from the spread in  $h_{FE}$  is  $\pm 49\%$ . Because the emitter current spread resulting from the spread in  $h_{FE}$  is high, simple current biasing is suitable only for transistors with narrow  $h_{FE}$  spreads.

The maximum and minimum values of  $I_E$  resulting from the spread in  $V_{BE}$  are  $0.944\text{mA}$  and  $0.928\text{mA}$ . Thus the spread in  $I_E$  resulting from the spread in  $V_{BE}$  is  $\pm 0.86\%$ .

If  $V_S$  falls from  $7\text{V}$  to  $3.5\text{V}$ , the nominal emitter current falls from  $0.935\text{mA}$  to  $0.415\text{mA}$ ; that is,  $I_E$  falls by  $56\%$ . However, because there are no resistors in either the collector or the emitter lead, the collector-emitter voltage is equal to the supply voltage. Thus, a higher-value series resistor can be used in the supply line (shared between the r.f. and i.f. stages), if the collector-emitter voltage in this method is to be the same as that in the other two biasing methods discussed. The higher the value of this series resistor the less dependent the emitter current will be on supply voltage.

## APPENDIX 2

# BBC TEST-TONE TRANSMISSIONS

Details of test-tone transmissions are reproduced in Table 21 from a BBC publication\*. The BBC reserves the right to change all or any part of the schedule.

The tones shown in the table are transmitted on Wednesdays and Saturdays. On other days, a 250Hz tone is transmitted in the left channel only from about four minutes after the end of the last programme on Radio Three until 23.55. This test may be interrupted from time to time.

The schedule given in the table is subject to variation in accordance with programme requirements and essential transmission tests. The zero level reference corresponds to 40% of the maximum level of modulation applied to either stereophonic channel before pre-emphasis. All tests are transmitted with pre-emphasis.

Periods of tone lasting several minutes are interrupted momentarily at one minute intervals.

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\*The British Broadcasting Corporation, Information Sheet No. 1605 (1), September, 1968.

**TABLE 21****BBC Test-tone Transmissions**

Time	Left Channel (A)	Right Channel (B)
23.30	250Hz at zero level	440Hz at zero level
23.32	440Hz at zero level	440Hz at zero level, antiphase to left channel
23.35	440Hz at +8dB	440Hz at +8dB, antiphase to left channel
23.37	440Hz at +8dB	440Hz at +8dB, in phase with left channel
23.39	250Hz at +8dB	440Hz at +8dB
23.40	250Hz at zero level	Nothing
23.44	Nothing	440Hz at zero level
23.47.20 approx.	Tone sequence at -4dB: 60Hz, 900Hz, 5kHz, 10kHz. This sequence is repeated.	Nothing
23.48.20 approx.	Nothing	Tone sequences as for left channel at 23.47.20
23.49.20	250Hz at zero level	Nothing
23.51	Nothing	Nothing
23.53	Reversion to monophonic transmission	

### APPENDIX 3

## CHARTS AND NOMOGRAMS

This appendix contains miscellaneous charts and nomograms relevant to radio and audio system design:

- Chart 1 Fletcher-Munson curves
- Chart 2 Every-day noise levels
- Chart 3 Frequency range of musical instruments
- Chart 4 Radio frequency and wavelength
- Chart 5 Decibel charts
- Chart 6 Reactance chart

### **CHARTS 1, 2 and 3**

These three charts are of interest in that they give some indication of the performance required of an audio reproduction system in terms of the characteristics of the human ear and the frequency ranges of musical instruments.

Chart 1 shows equal-loudness contours for the ear, the sound intensity required to produce a sensation of equal loudness at varying frequencies being plotted for various levels of loudness from just audible to the point where the sound is "felt" rather than heard. It will be seen that the ear can respond to all frequencies in the range 15Hz to 20kHz, and to an intensity range of about 120 to 130dB in the region of 3kHz. However, the ear is relatively insensitive to both high and low frequencies in the audio band, especially at low intensity levels. The sensitivity of the ear remains constant with varying intensity above a level of about 80dB and between about 70Hz and 6kHz, but is bass-deficient at lower intensity levels.

Chart 2 relates loudness levels expressed in phons to some every-day noises.

Chart 3 shows the frequency range of a selection of musical instruments, male and female speech. The solid line indicates the actual tone range of the instrument and the dotted line accompanying overtone and action noises.

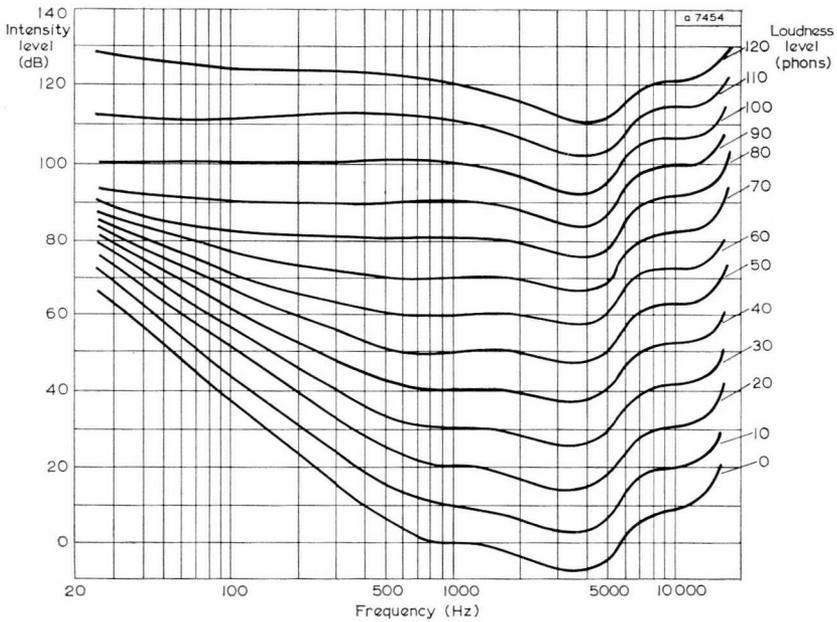


CHART 1. FLETCHER-MUNSON CURVES

Noise	Loudness level in phons
Pneumatic drill	110
Underground train	100
Very loud radio	90
Suburban train	80
Average factory	70
Quiet car	60
Average office	50
Public library	40
Audience noise during concert	30
Whisper	20
Night time in country	10
Soundproof room	approximate zero reference level

CHART 2. EVERY-DAY NOISE LEVELS

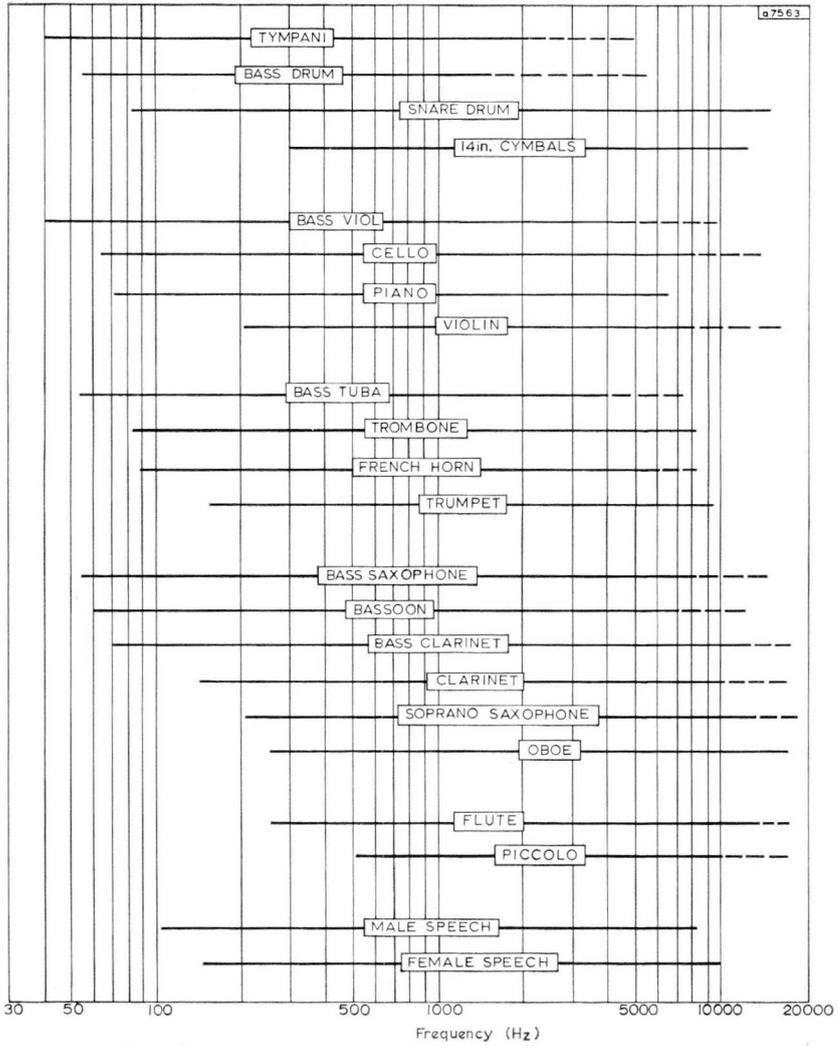


CHART 3. FREQUENCY RANGES OF MUSICAL INSTRUMENTS

#### **CHART 4 RADIO FREQUENCY AND WAVELENGTH**

The chart is self-explanatory, values of frequency being tabulated against corresponding values of wavelength. The example will illustrate the use of the chart.

Example: What is the wavelength corresponding to a frequency of 70MHz?

Opposite a figure of 7MHz on the scale a wavelength of 42.9 metres is shown. Multiplication by the correct factors for Band 5 gives a wavelength of 4.29 metres for a frequency of 70MHz.

Multiples of wavelength scale  
for different bands

Band 2 (1000 to 10000 metres)	$10^2$
Band 3 (100 to 1000 metres)	10
Band 4 (10 to 100 metres)	1
Band 5 (1 to 10 metres)	$10^{-1}$
Band 6 (10 to 100 centimetres)	$10^{-2}$

Multiples of frequency scale  
for different bands

Band 2 (30 to 300kHz)	$10^{-2}$
Band 3 (300kHz to 3MHz)	$10^{-1}$
Band 4 (3 to 30MHz)	1
Band 5 (30 to 300MHz)	10
Band 6 (300 to 3000MHz)	$10^2$

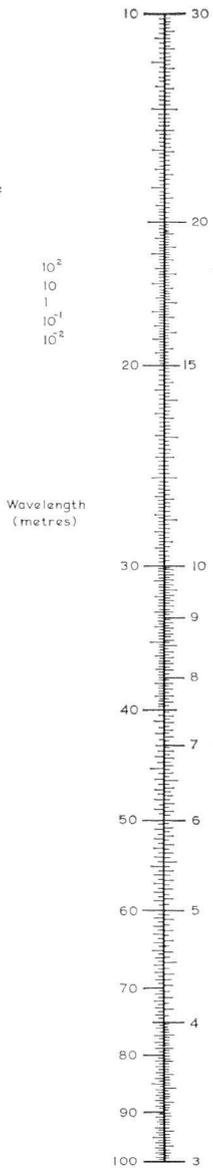


CHART 4. RADIO FREQUENCY AND WAVELENGTH

## CHART 5 DECIBELS UP (a) and DOWN (b)

The formula expressing the relationship between power ratio  $R$  and decibels dB is:

$$\text{dB} = 10 \log_{10} R$$

The formula expressing the relationship between voltage or current ratio,  $R_e$  or  $R_i$  respectively, and decibels dB, is:

$$\begin{aligned} \text{dB} &= 20 \log_{10} R_e \\ \text{or } \text{dB} &= 20 \log_{10} R_i \end{aligned}$$

Two points should be remembered when expressing gain in decibels. Firstly, a decibel is a ratio, so gain can only be expressed in decibels when a reference level is understood. Secondly, although voltage and current gains may be expressed in decibels, the decibel is essentially a measure of power ratio. The gain of an amplifier may be given in decibels only if the input and output impedances are equal or some allowance is made for the difference between them. The voltage or current gain of an amplifier is given by the expression:

$$\begin{aligned} \text{Gain (dB)} &= 20 \log_{10} R_e + 10 \log_{10} \frac{Z_1}{Z_2} \\ &\text{or } 20 \log_{10} R_i + 10 \log_{10} \frac{Z_1}{Z_2} \end{aligned}$$

where  $Z_1$  and  $Z_2$  are the input and output impedances of the amplifier.

The use of the charts is illustrated by two examples.

Example 1: What is the power ratio corresponding to 30dB up?

The power ratio is read directly from the 'power' scale (Chart 5a) and is 1000.

Example 2: What is the equivalent in decibels of a voltage ratio of 0.07?

The voltage ratio is located on the 'voltage and current' line (Chart 5b) and the equivalent in dB is read directly as -23dB

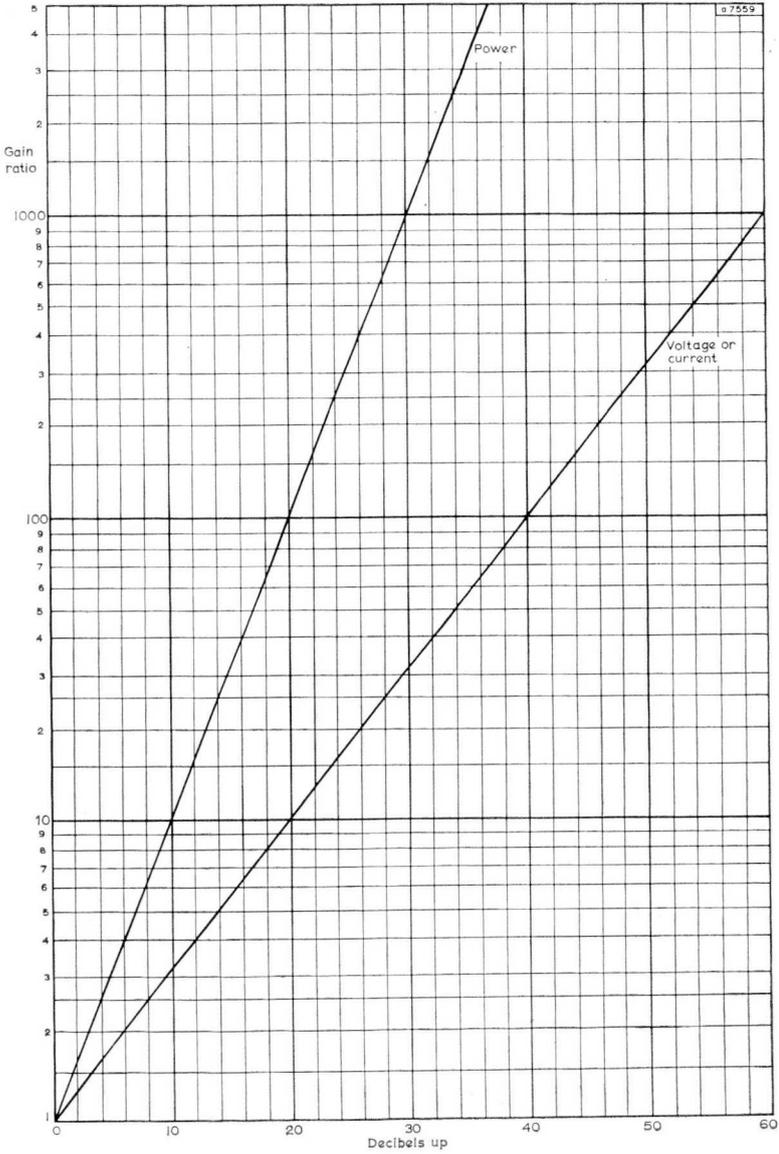


CHART 5a. DECIBELS UP

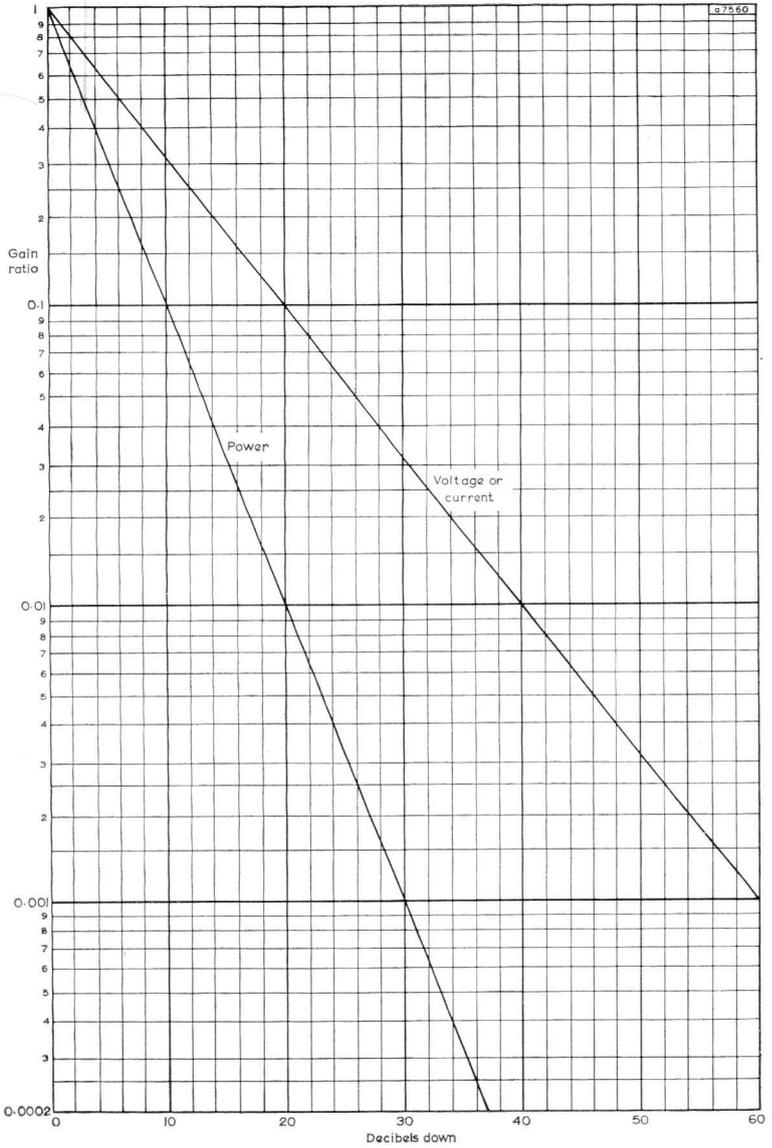


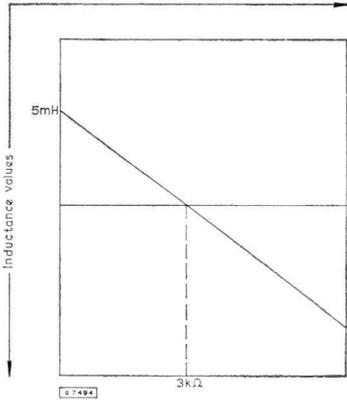
CHART 5b. DECIBELS DOWN

## CHART 6 REACTANCE CHART

This chart is used to find the reactance of inductors and capacitors.

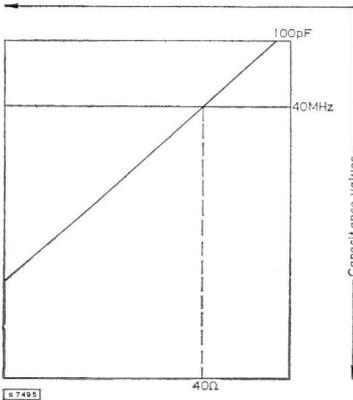
Values of inductance are represented by the lines with negative slope; the inductance scale is on the top and left of the chart. Values of capacitance are represented by the lines with positive slope; the capacitance scale is on the top and right of the chart. Values of frequency and reactance are represented by horizontal and vertical lines respectively. The following examples will illustrate the use of the chart.

Example 1: What is the reactance of a 5mH inductor at a frequency of 100kHz?



The intersection of the line representing 5mH with the 100kHz horizontal gives a reactance value of 3kΩ.

Example 2: What is the reactance of a 100pF capacitor at a frequency of 40MHz?



The intersection of the line representing 100pF with the 40MHz horizontal give a reactance value of 40Ω.



